

# Experimental Investigation of Flow Models Applied to Worst-Case-Discharge Calculations



LSU

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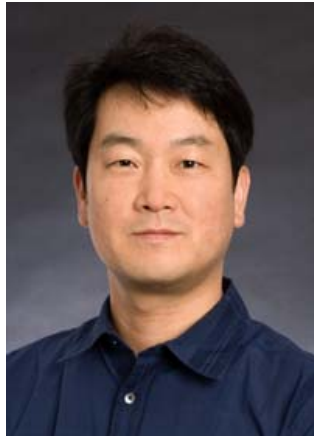
# LSU Team – Principal Investigators



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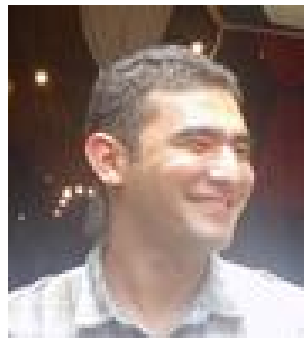


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MSc. in Petroleum Engineering



***Matheus Capovila, BS***

*PhD Graduate Student*



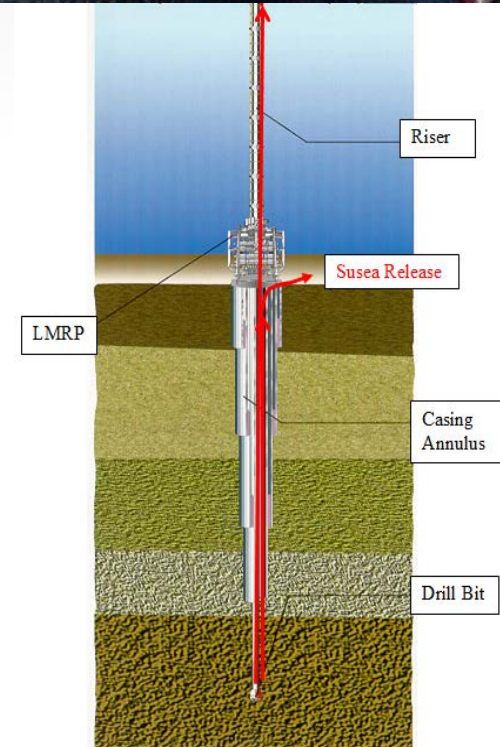
BS in Mechanical Engineering

# Outline

- ✓ Overview of Project Objectives and Deliverables
- ✓ Literature Review Findings and Conclusions
- ✓ Experimental Investigation
- ✓ Evaluation of Flow Models to Predict Experimental Data
- ✓ Comparison of Flow Models Applied to WCD Calculations
- ✓ Conclusions
- ✓ Future Projects

# Project Motivation [1]

- ❑ **Blowouts** Happen!
- ❑ For **effective contingency** plans, we need **accurate oil spill predictions!**
- ❑ For accurate predictions, **we need reliable models!**
- ❑ Industry and **regulatory agencies need guidance** from unbiased experts (**universities** and research institutions)
- ❑ **Improvement is needed** to avoid future **large environmental** and **economical impacts**



Source: TAMU – Pemex Offshore Drilling

# Project Motivation [2]



SPE Technical Report

Calculation of

Worst-Case Discharge (WCD)

March 2015

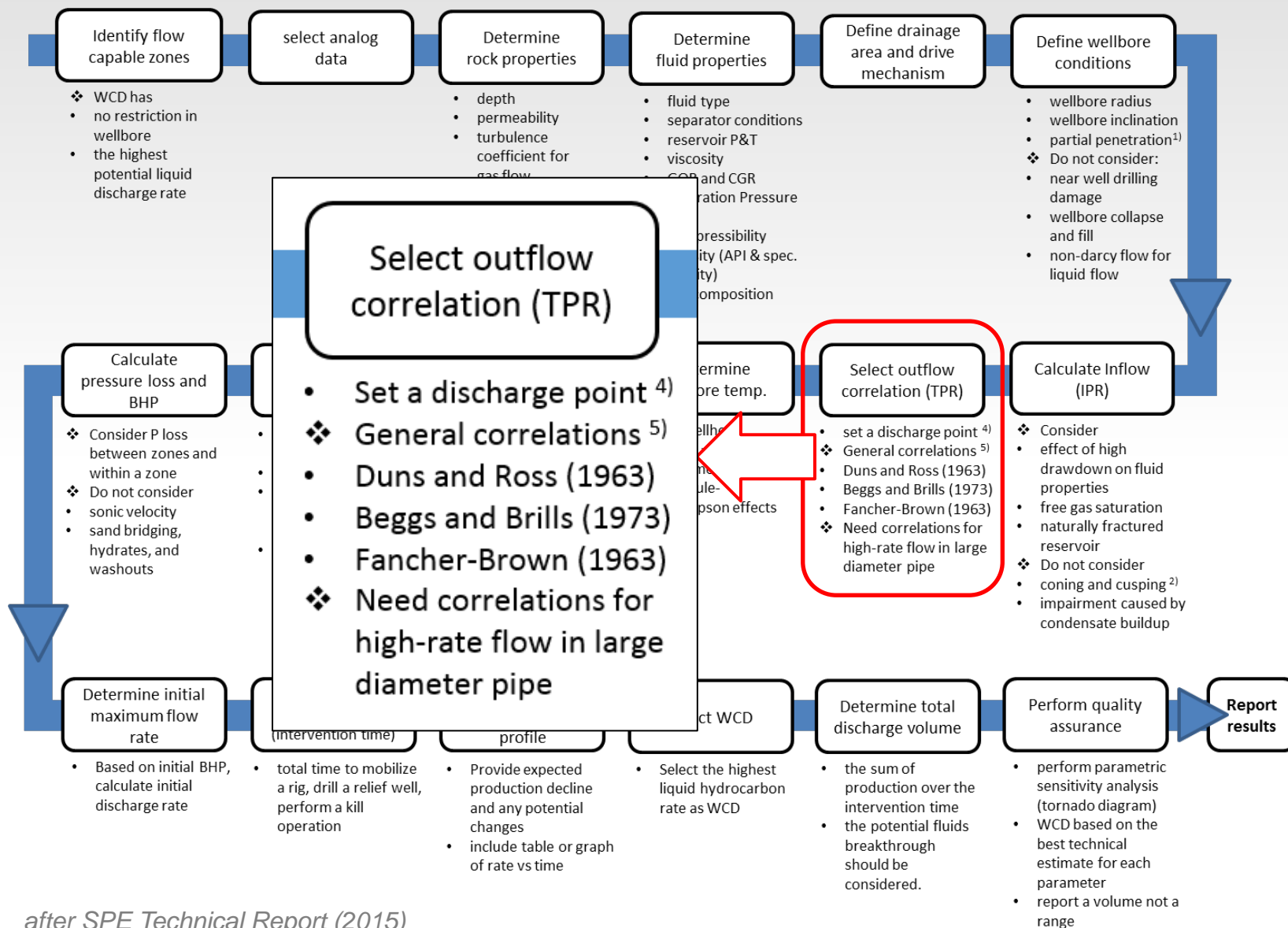
“Most flow correlations were developed for small diameter pipe, so their **applicability to larger-diameter pipe** and open hole **is uncertain.**”

“The committee proposes that **further research and development be conducted** on appropriate correlations **for high-rate flow in large diameter pipe.**”

This report represents the consensus viewpoints of subject matter experts and is intended to provide useful information to SPE members, the public, and the industry. It is not intended to take the place of advice on the application of technology to specific circumstances. Readers of this Technical Report are responsible for assessing its relevance and verifying its accuracy and their own choices, actions, and results. SPE and contributors to the Technical Report are not responsible for actions taken as a result of reading this document, nor the results of those actions.



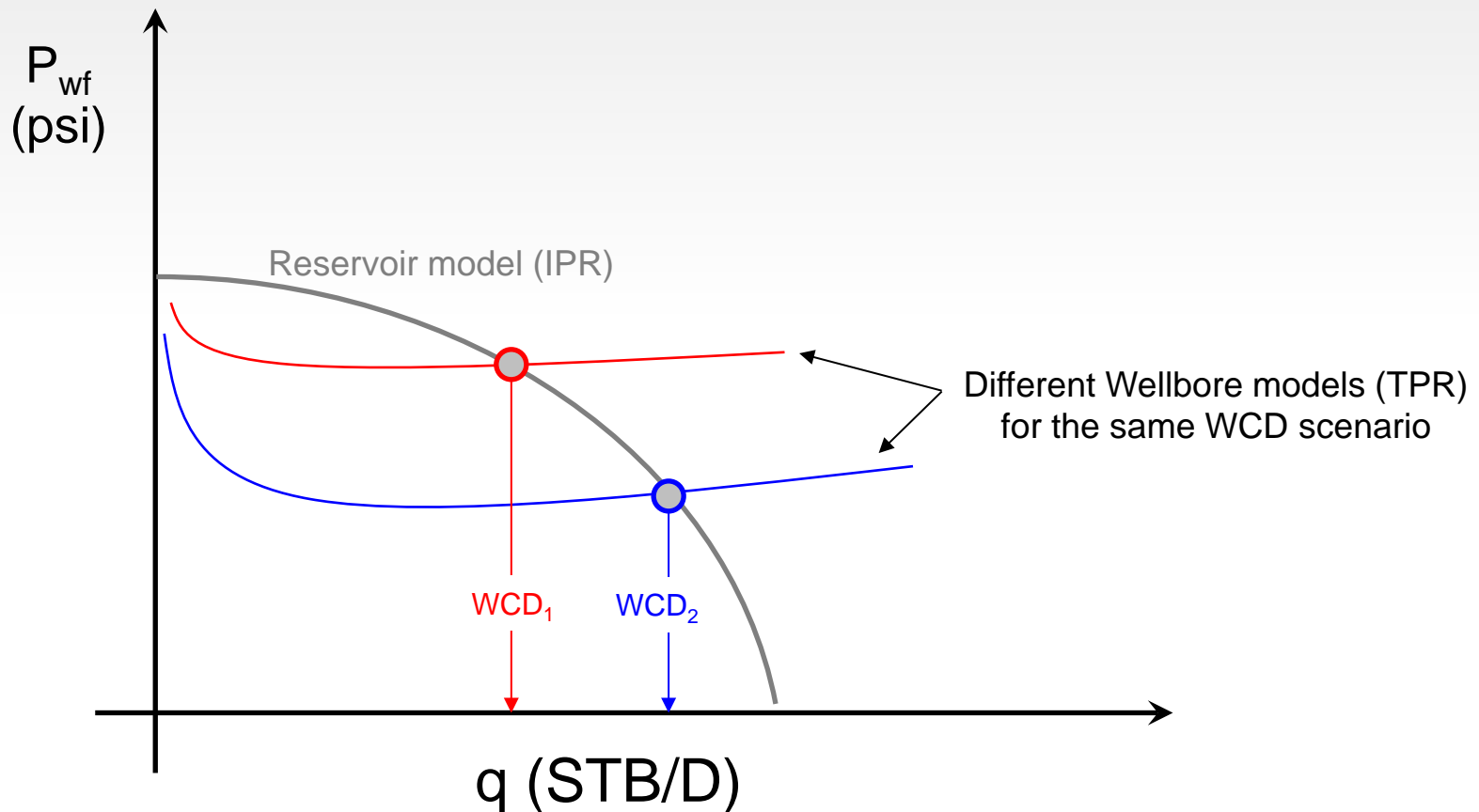
# Statement of the Problem [1]





# Statement of the Problem [2]

- **WCD predictions** are directly dependent to flowing bottomhole pressure of the well:



# Statement of the Problem [3]

- $q$  is calculated using reservoir and fluid properties, and  $p_{wf}$  :

$$q \propto \frac{kh(p_e - p_{wf})}{B_o \mu \ln\left(\frac{r_e}{r_w}\right)} \quad (\text{for } p_{wf} > p_{bp})$$

reservoir and fluid properties

- $p_{wf}$  is obtained from **wellbore flow correlations** and wellhead conditions:

$$p_{wf} = p_{wh} + \int_0^L \frac{dp}{dz} dz$$

generic pressure gradient equation

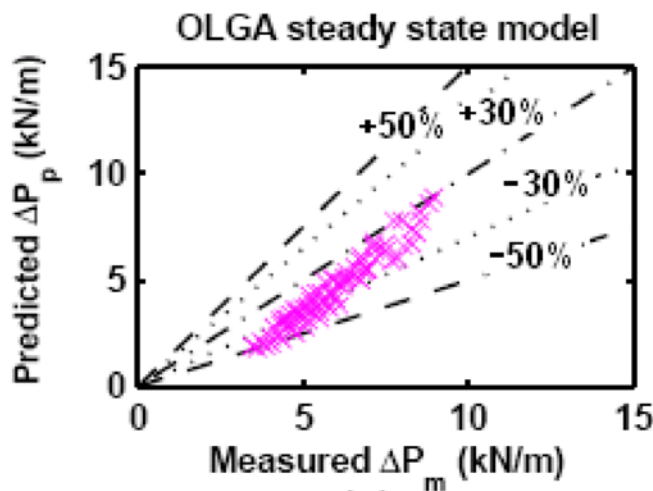
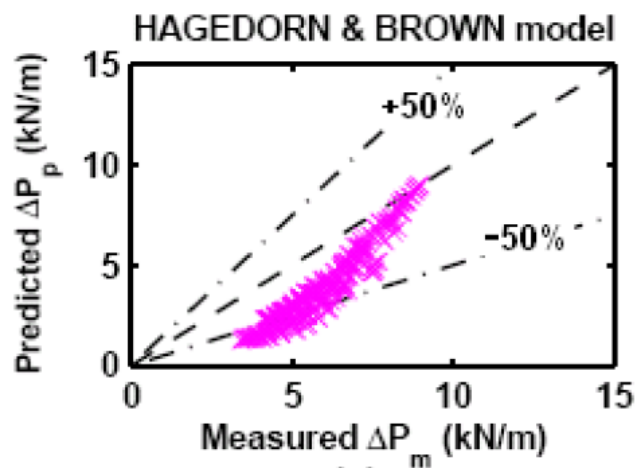
$$\frac{dp}{dz} = \frac{g}{g_c} \bar{\rho} + \frac{2f\bar{\rho}u_m^2}{g_c D} + \bar{\rho} \frac{\Delta(u_m^2/2g_c)}{\Delta z}$$

- Flow regimes
- Superficial velocities
- Pressure & temperature
- Fluid properties

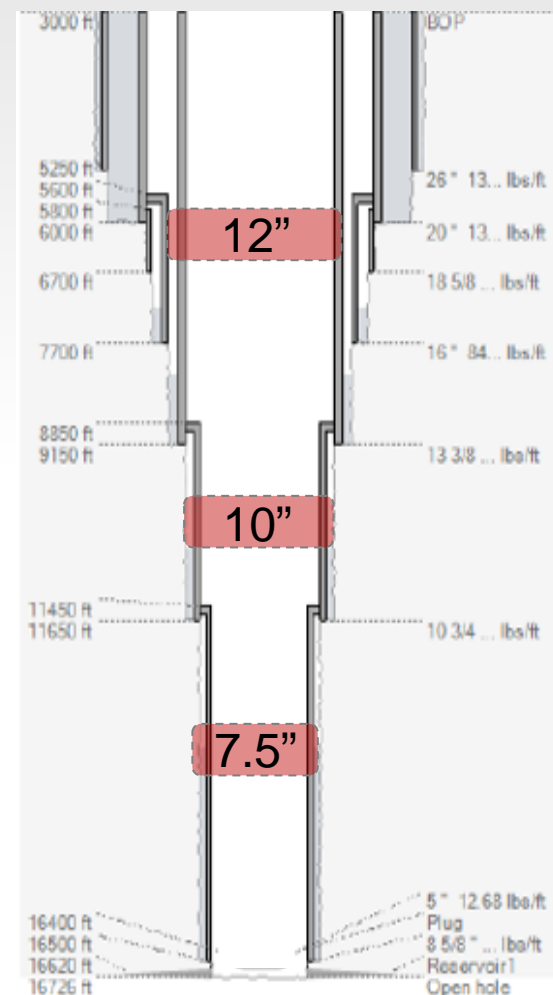
# Statement of the Problem [4]

- The use of flow correlations for **large diameter** pipes is **NOT well understood**:

Two-Phase flow in a vertical pipe (ID = 10 in)



Well configuration for typical WCD calculation scenario



# Objective

The goal of this project is to **examine the validity of current industry standard flow correlations** used in WCD calculations

## Scope of Work:

- Task 1 - A complete literature review
- Task 2 - A comparison between the different flow models applied to WCD
- Task 3&4 – Build apparatus & Generate data for large-diameters pipes and high-velocity flows
- Task 5&6 – Analyze experimental data & Compare with flow models results

# ***Literature Review (Task 1)***

# Worst-Case-Discharge Vastly Under Studied

## Wellbore and Near-Surface Hydraulics of a Blown-Out Oil Well

A.R. Clark, ARCO Oil and Gas Co.  
T.K. Perkins, SPE, ARCO Oil and Gas Co.

Journal of Natural Gas Science and Engineering 26 (2015) 438–445

### Summary

A method is presented for estimating flow velocity, pressure, and total discharge in a blown-out oil wellbore geometry. The method requires wellbore geometry, wellbore and near-surface hydraulic knowledge or correlations (PI) and gas/oil properties. The method is given for estimating the two-phase flow rate above the wellbore.



Contents lists available at ScienceDirect

## Journal of Natural Gas Science and Engineering

journal homepage: [www.elsevier.com/locate/jngse](http://www.elsevier.com/locate/jngse)

### Flow rate and total discharge estimations in gas-well blowouts

Ruo Chen Liu<sup>a</sup>, A. Rashid Hasan<sup>b</sup>, M. Sam Mannan<sup>a,\*</sup>

<sup>a</sup> Mary Kay O'Connor Process Safety Center, Department of Chemical Engineering, Texas A&M University, TX, USA

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#### ABSTRACT

Despite multitier safeguards in any drilling operation, blowouts do occur. In such cases, the total discharge of hydrocarbons becomes the focal point for a drilling operator, the service provider, and the regulatory body. Rate estimation based on scant information about the formation and fluids at the time of the accident requires guidelines that require such estimates for any offshore drilling, systematic investigations, and wellbore analysis.

This study presents an analytical model coupling the flow in a reservoir/wellbore system. The model considers flow in the tubing, annulus and riser, and the attendant wellbore system. To gauge safety concerns, a commercially

SPE 69530

## A Study on Blowouts in Ultra Deep Waters

O.L.A. Santos, SPE, Petrobras

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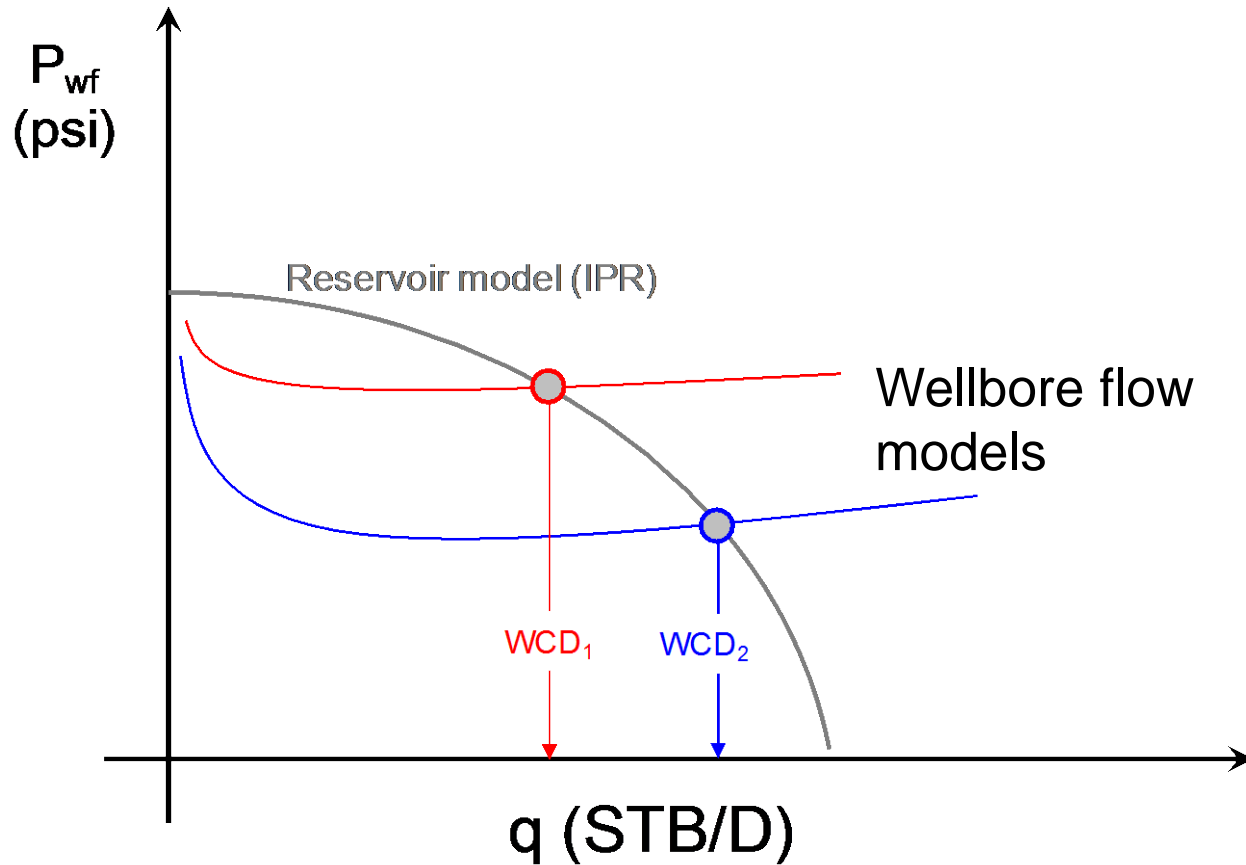
This paper was prepared for presentation at the SPE Latin American and Caribbean Petroleum Engineering Conference held in Buenos Aires, Argentina, 25–28 March 2001.

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### Abstract

This paper presents the preliminary results of a research project on ultra deepwater blowouts. This research is a part of a comprehensive study currently conducted by Petrobras, the Brazilian oil company, aiming at drilling and producing safely, in terms of well control, in water depths as deep as 10000 feet (approximately 3000 meters). Firstly, the paper presents a methodical procedure that predicts wellbore pressures and well properties during a gas blowout using an unsteady state model that considers the multiphase nature of the flow.

# BOEM'S ENGINEERING WORKFLOW



**Tubing Curve:**  
Directional Survey, Drilling Program, Casing Design, and Open Hole Configuration

Generate WCD Rate

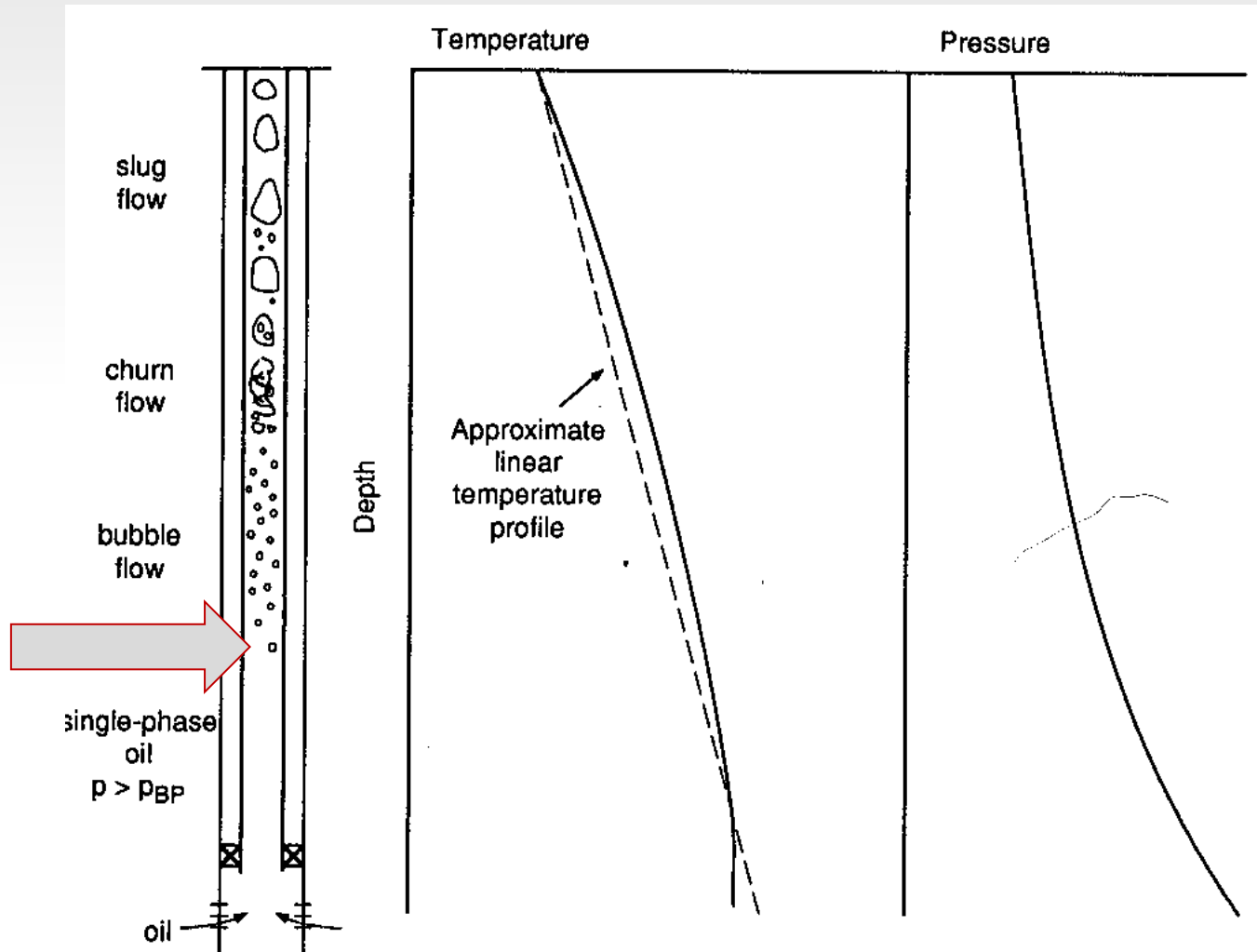


# PRESSURE DROP ( $\Delta P$ ) PREDICTION MODELS

- ❑ **Empirical Correlations** (strongly based on data)
- ❑ **Drift-Flux models** (additional physics but still based on data)
- ❑ **Mechanistic Models** (1D solution of conservation equations but also uses empirical correlations)
- ❑ **CFD Models** (3D-transient solution of conservation equations but needs calibration and computationally expensive)

# SOURCES OF ERRORS ON FLOW MODELS [1]

## ❑ ERRORS IN FLUID PROPERTIES & CALCULATION DIRECTION



# SOURCES OF ERRORS ON FLOW MODELS [2]

## Review of Conditions Used to Develop Flow Models

Correlation	Fluid	Pipe ID (in)	Pipe length (ft)	liquid rate (bbl/d)	Gas rate (Mscf/d)	Fluid properties	Degree From horizon
Poetmann and Carpenter (1952)	Oil/gas, gas/oil/water	2, 2 ½, 3	1,100-11,000	5 - 1,400 (oil)	18 -1,630	30°-54° API; 0.6-1.15 Gas SG 0.2<GOR<41 Mscf/bbl	90
Baxendell and Thomas (1961)	Gas/oil	2 7/8 , 3 ½	6,250	200-5,100 (oil)	N/A	Oil: 34° API, 2.58 cp at 160° F 120<GOR< 160 vol/vol Oil: 20°-40° API 1 - 300 cp	90

Duns and Ros (1963)	1, 5/8, 3 ½, 6 in ID Vertical Pipe
Asheim (1986) (Mona)	Tested with Forties field, Ekofisk field, and Prudhoe Bay flow line data
Ansari (1994)	Developed with data from TUFFP Databank
Gomez et al. (2000)	Validated against TUFFP Databank
OLGA-S 2000 S.S.	Used over 10000 data from SINTEF multiphase flow loop

Asheim (1986) (Mona)	Tested with Forties field, Ekofisk field, and Prudhoe Bay flow line data points	0 to 90
Yao and Sylvester (1987)	Gas/water, oil/gas compared with field data from Camacho (1970) and Reinicke and et al. (1984), Govier and Fogarasi (1975)	90
Ansari (1994)	Developed with data from TUFFP Databank	90
Petalas and Aziz (1996)	Verified against Stanford Multiphase Flow Database (SMFD)	any angle
Chokshi and et al.(1996)	Air/water 3 ½ 1333 79-4250 42-2800 16<GLR<12685	90
Gomez et al. (2000)	Validated against TUFFP	any angle
OLGA-S 2000 S.S.	Used over 10000 data from SINTEF multiphase flow loop	N/A
LedaFlow	Used over 10000 data from SINTEF multiphase flow loop	N/A

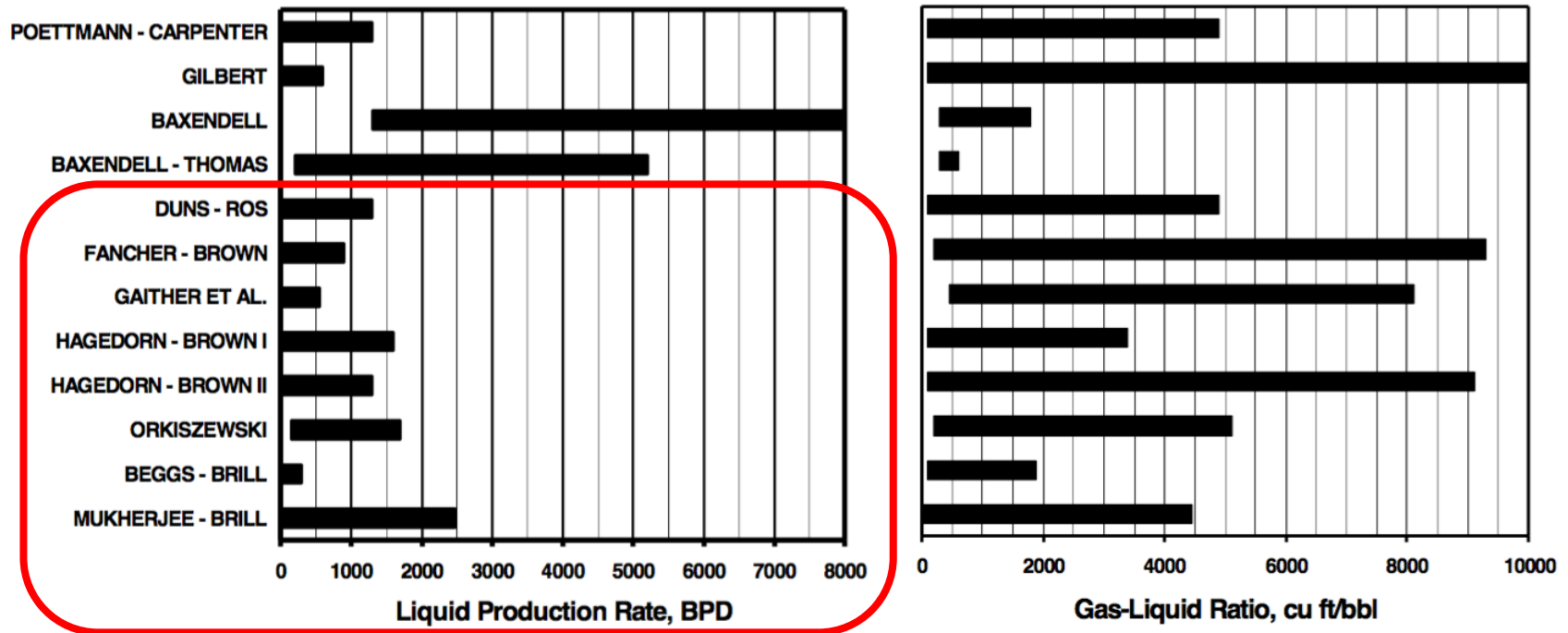
# SOURCES OF ERRORS ON FLOW MODELS [3]

## Review of Databases Used to Develop Flow Models

SINTEF multiphase flow loop (OLGA-S 2000 S.S.)	Nitrogen, Naphtha/diesel, lube oil	8 in ID
TUFFP databank	Oil/gas/water	1-8 in ID
Forties field	Oil/gas	3.958, 6.185 in ID

# SOURCES OF ERRORS ON FLOW MODELS [4]

## Review of Flow Rates Used to Develop Flow Models



$$Q_1 < 2,500 \text{ STB/D}$$

Takacs (2001)

# SOURCES OF ERRORS ON FLOW MODELS [5]

## Why Flow Regime Predictions are Important for WCD calculations?

### Correlations

Duns and Ros (1963)

Hagedorn and Brown (1964)

Hagedorn and Brown Modified (1965)

Orkiszewski (1967)

Beggs and Brill Revised (1973)

Gray (1974)

Govier and Foragasi (1975)

Mukherjee and Brill (1985)

Ansari (1994)

### Flow patterns

bubble, slug, and froth

no flow pattern consideration

bubble, slug

bubble, slug, annular slug transition, annular mist

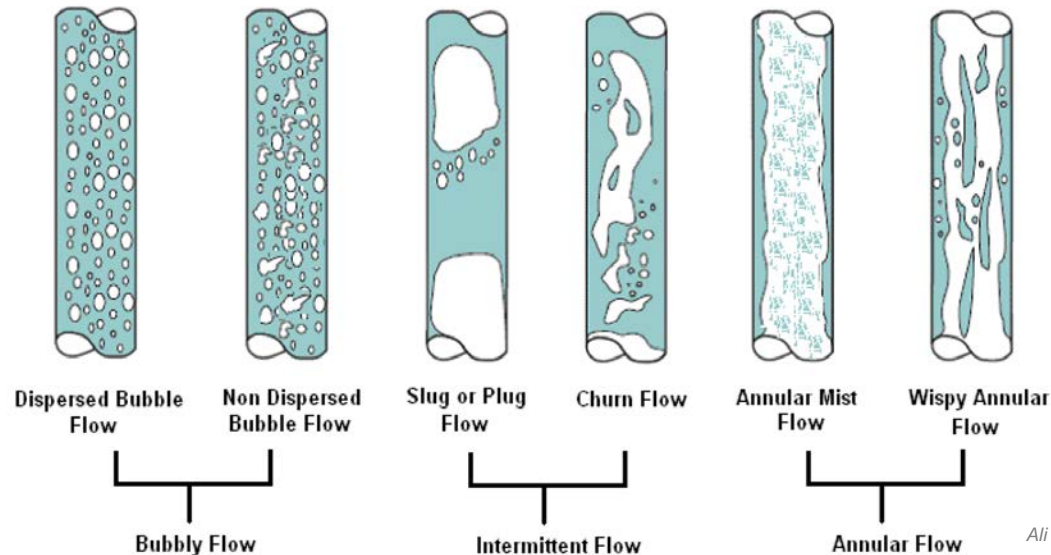
(horizontal pipe) segregated, intermitted, distributed, froth

no flow pattern consideration

slug, annular mist, froth

no flow pattern consideration

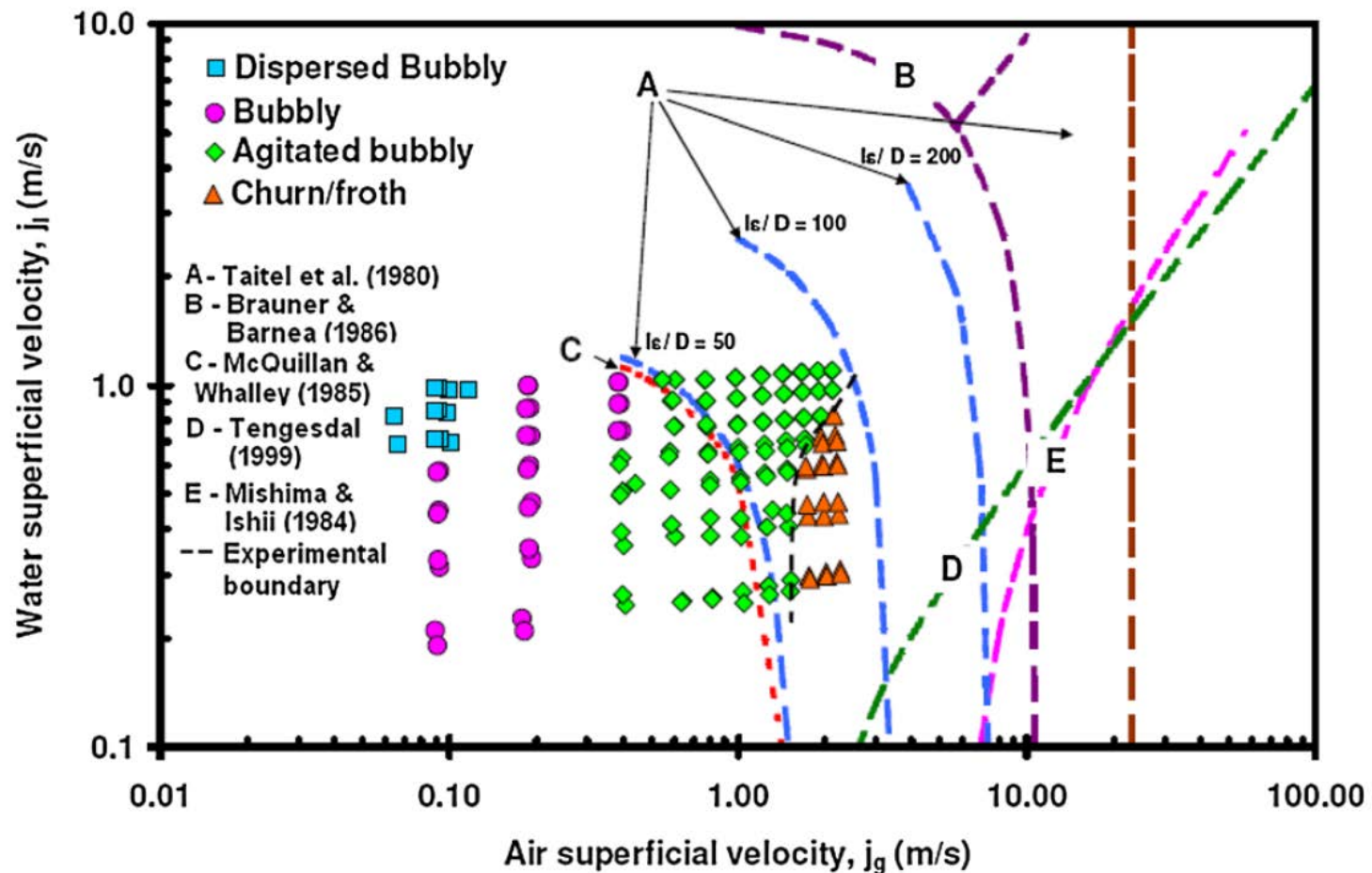
bubble, slug, and annular



# Flow Regime Maps for Large-Diameter Pipes

## Ali (2009) - Experimental conditions tested

Study	$Q_o$ , BBL/D	$Q_l$ , GPM	ID, in	$U_{sl}$ , m/s	GLR, SCF/STB	$Q_g$ , MMSCF/D	$Q_g$ , SCFM	$U_{sg}$ , m/s
Ali	30,300	883	10	1.1	41	0.350	243	2.3

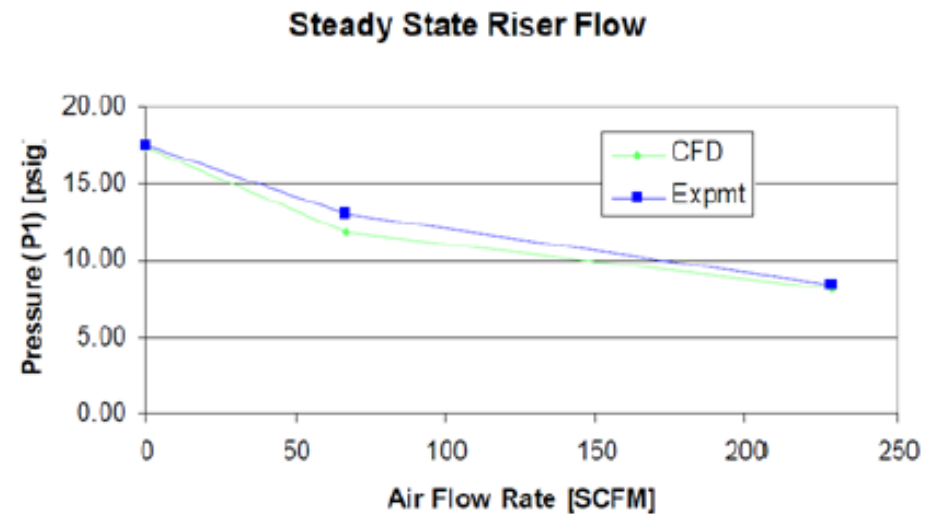
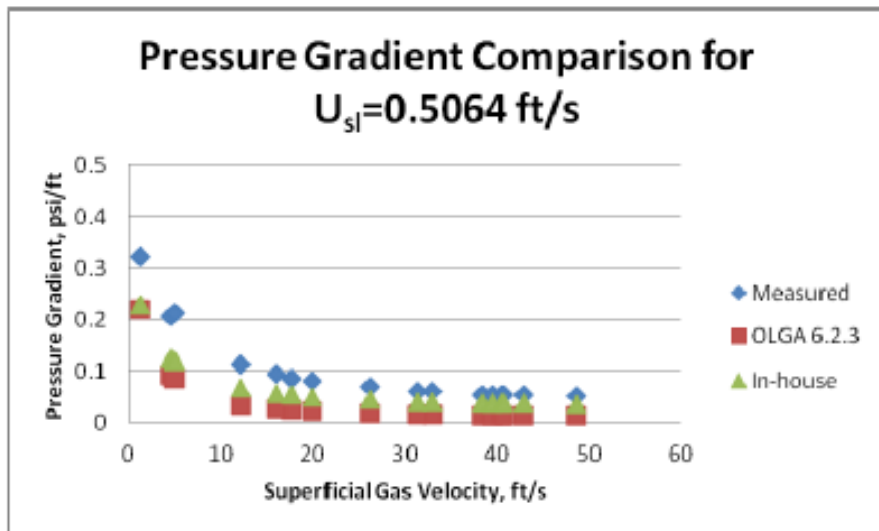




# Evaluation of Using CFD models for Multiphase flow in Large Pipe Diameters

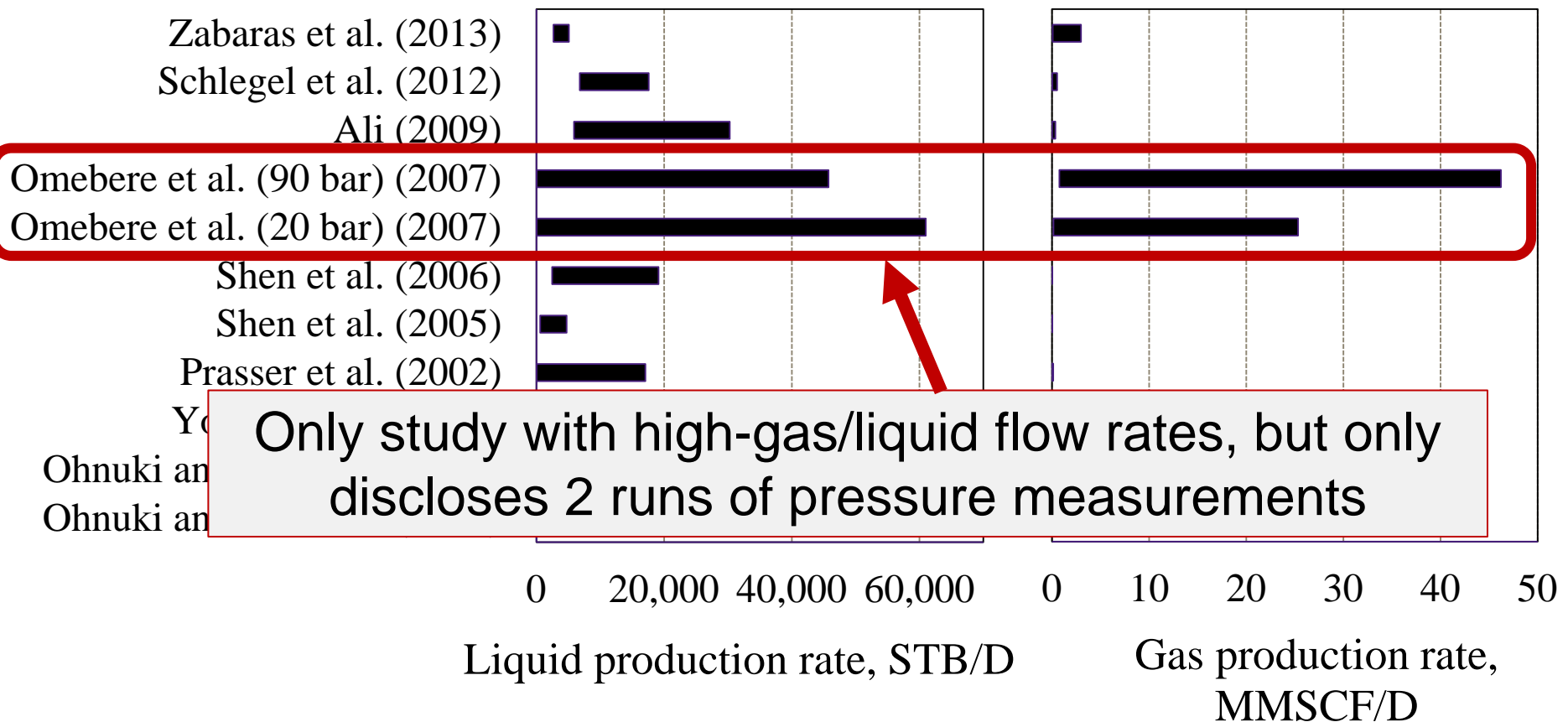
## Zabaras (2013) - Experimental conditions tested

Study	Qo, BBL/D	Ql, GPM	ID, in	Usl, m/s	GLR, SCF/STB	Qg, MMSCF/D	Qg, SCFM	Usg, m/s
Zabaras	5140	150	11	0.15	2640	2.97	2063	15.9

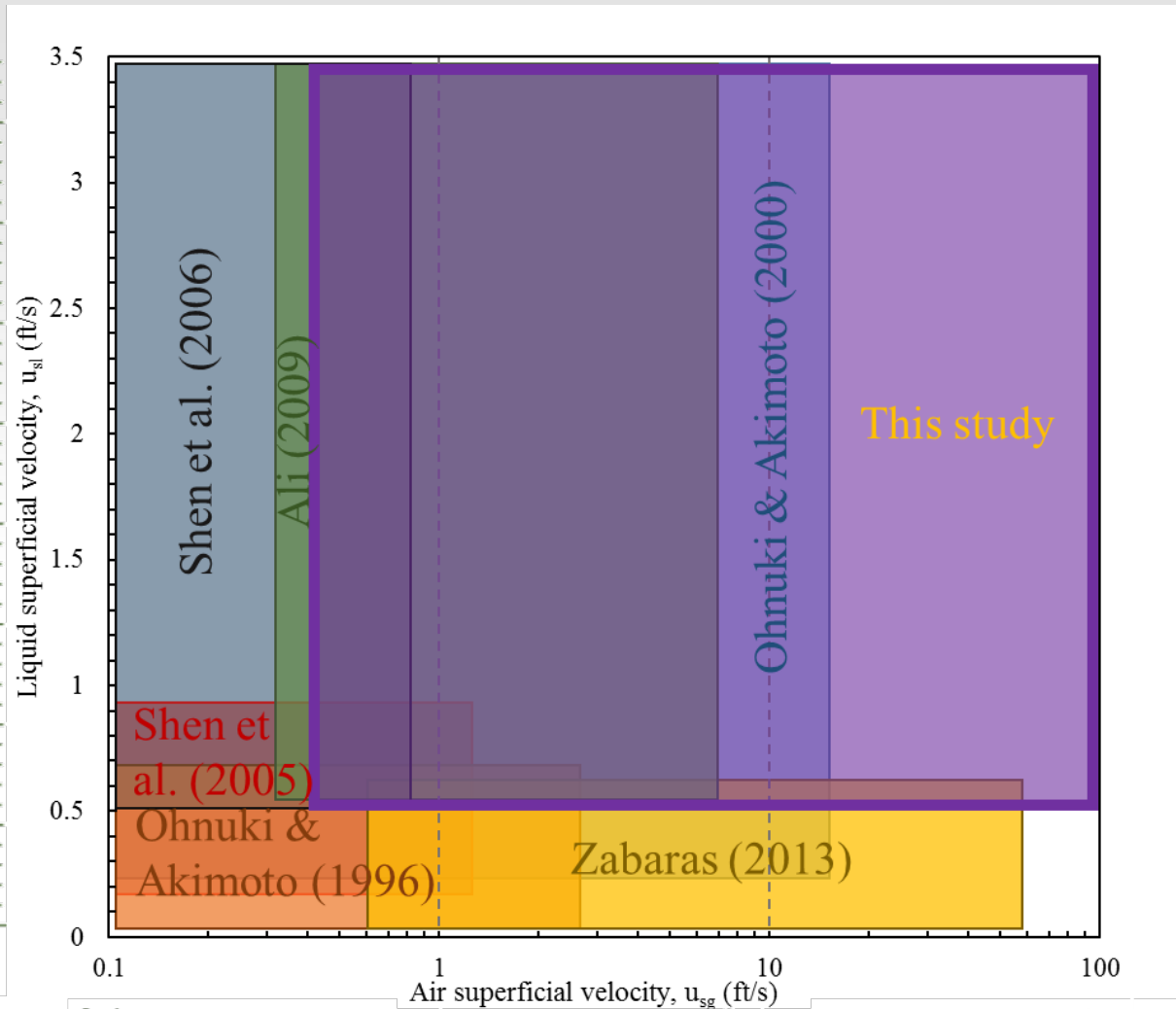
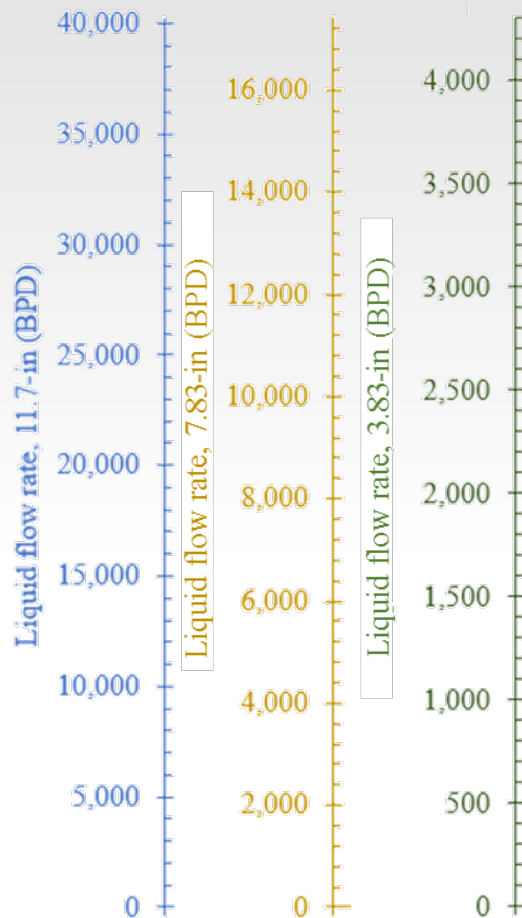


# Gaps in Studies for Large-Diameter Pipes [1]

## Review of Studies on Two-Phase Flows for ID > 6 in



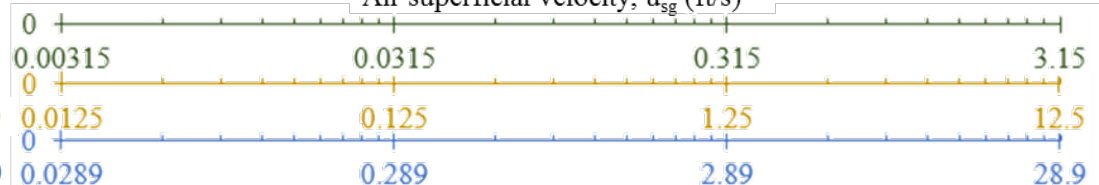
# Gap in Studies for Large-Diameter Pipes [2]



Gas flow rate at 5,000 psi, 3.83-in (MMSCF/Day)

Gas flow rate at 5,000 psi, 7.83-in (MMSCF/Day)

Gas flow rate at 5,000 psi, 11.7-in (MMSCF/Day)



# Conclusions from Literature Review







- ❑ **Flow correlations** were originally developed and are still **NOT** verified for **LARGE-diameters (ID < 8 in)**
- ❑ **Lack of studies** on Two-Phase Flows in **large-diameters (ID > 6)** and **high liquid/gas flow rates ( $Q_l > 30,000$  bbl/d)**
- ❑ **“Non-standard” flow correlations** should be evaluated **to be used** in **WCD models**
- ❑ **WCD models** vastly under studied
- ❑ **Models specifically developed for WCD scenarios ARE NEEDED!**

# **Experimental Investigation**

## ***(Task 3-5)***

# Experimental Apparatus



-  Pressure transducer
-  Thermocouple
-  Ball valve
-  Gate valve
-  Control valve
-  Check valve





Ex



Pressure  
Gauges



d





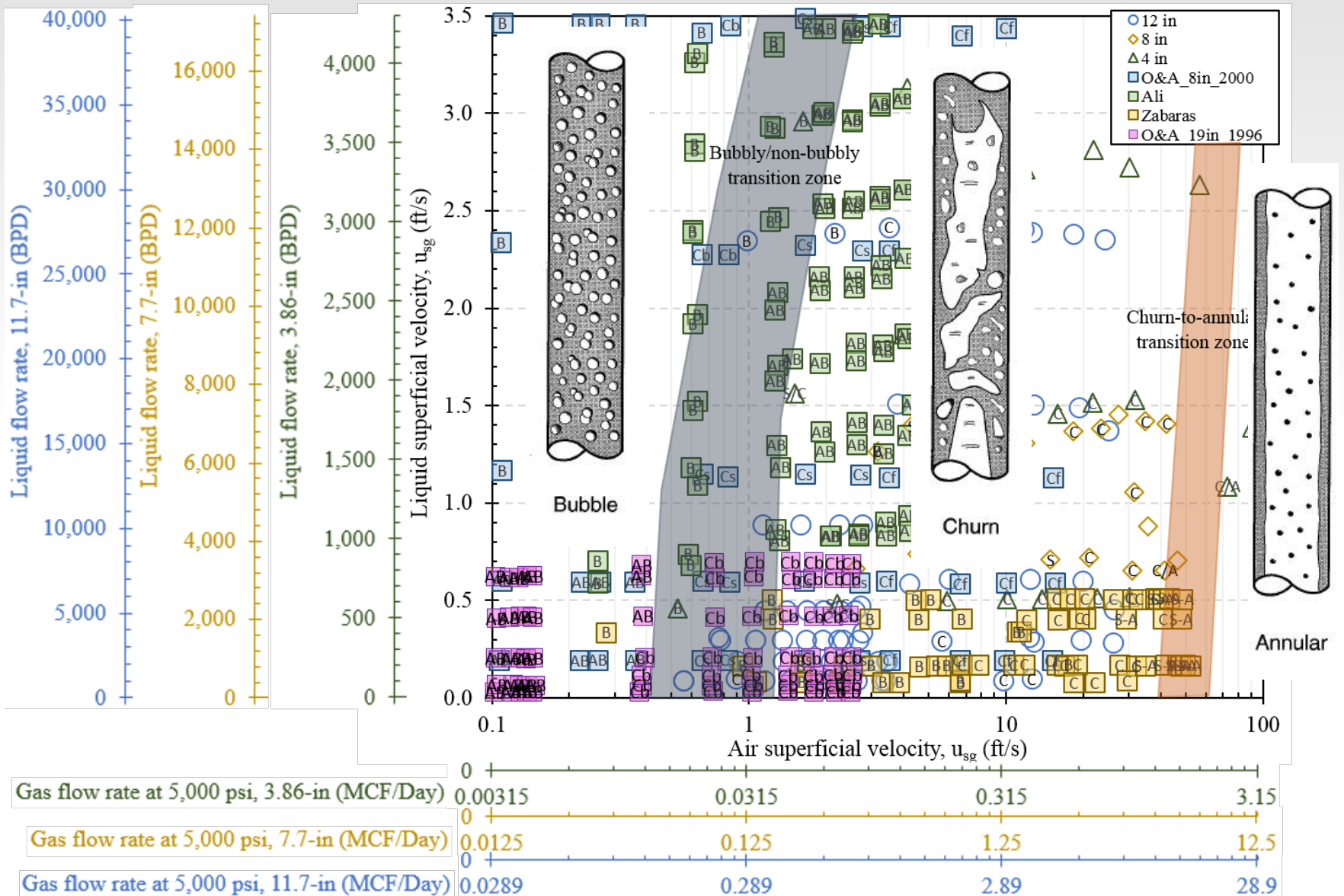
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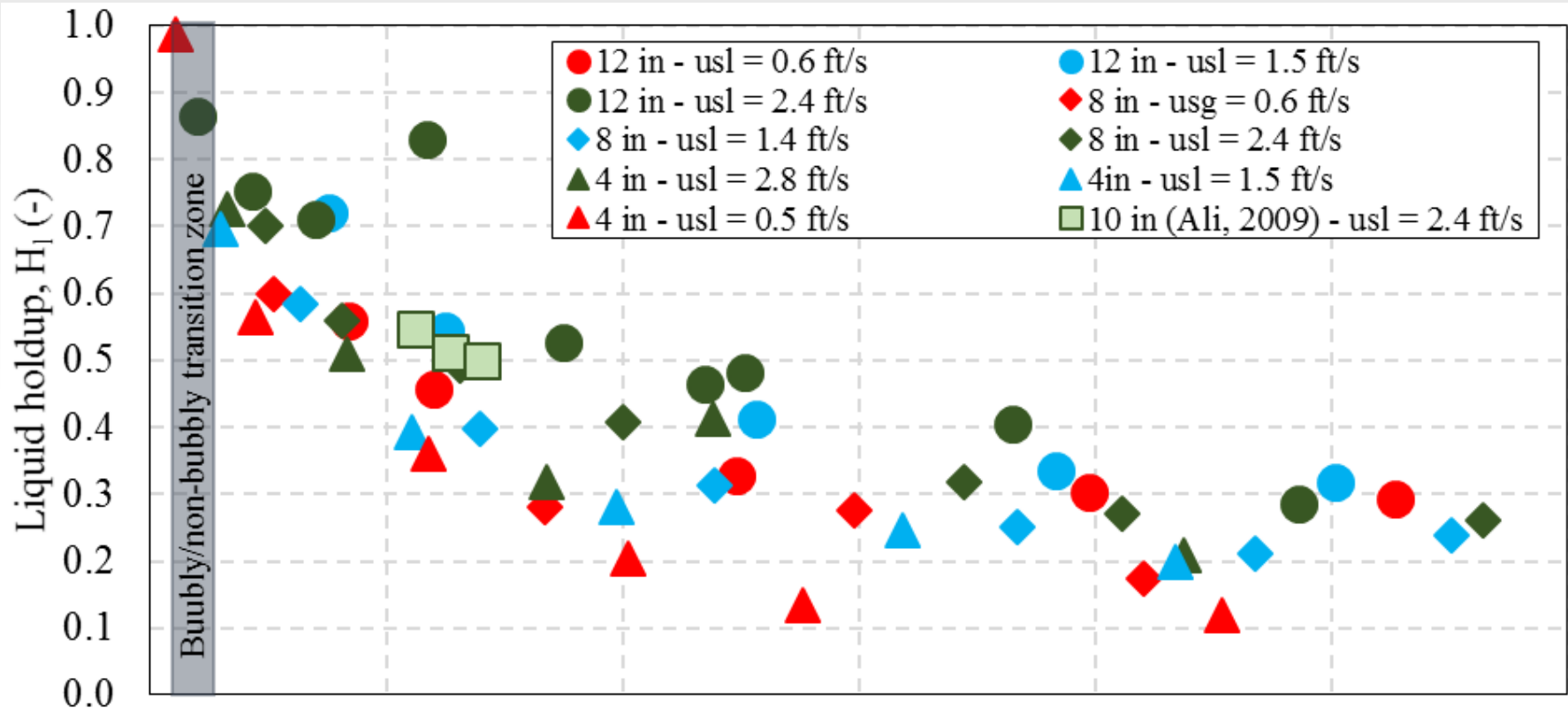
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# Flow Regime Observations [2]

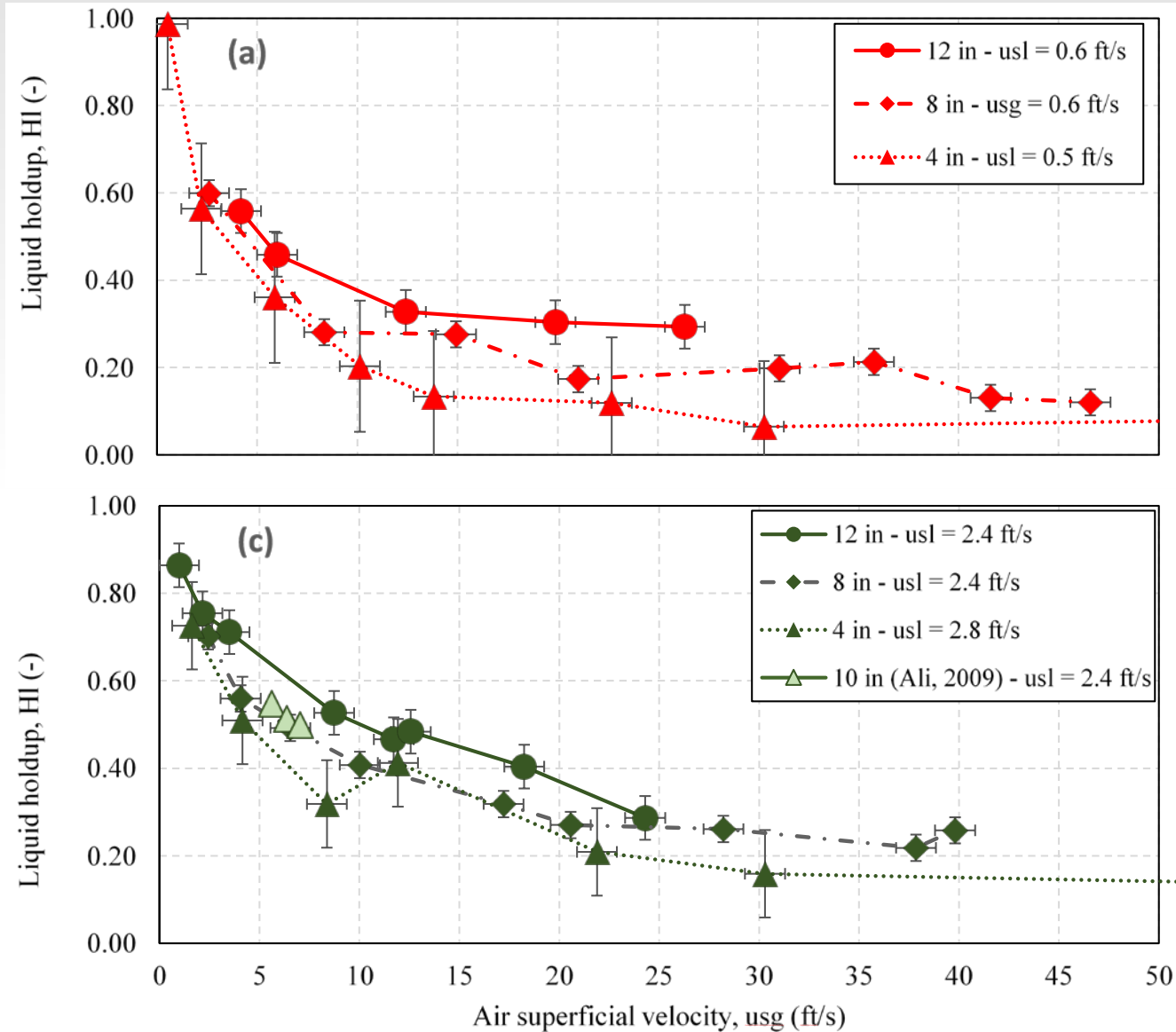


# Liquid Holdup Measurements [1]



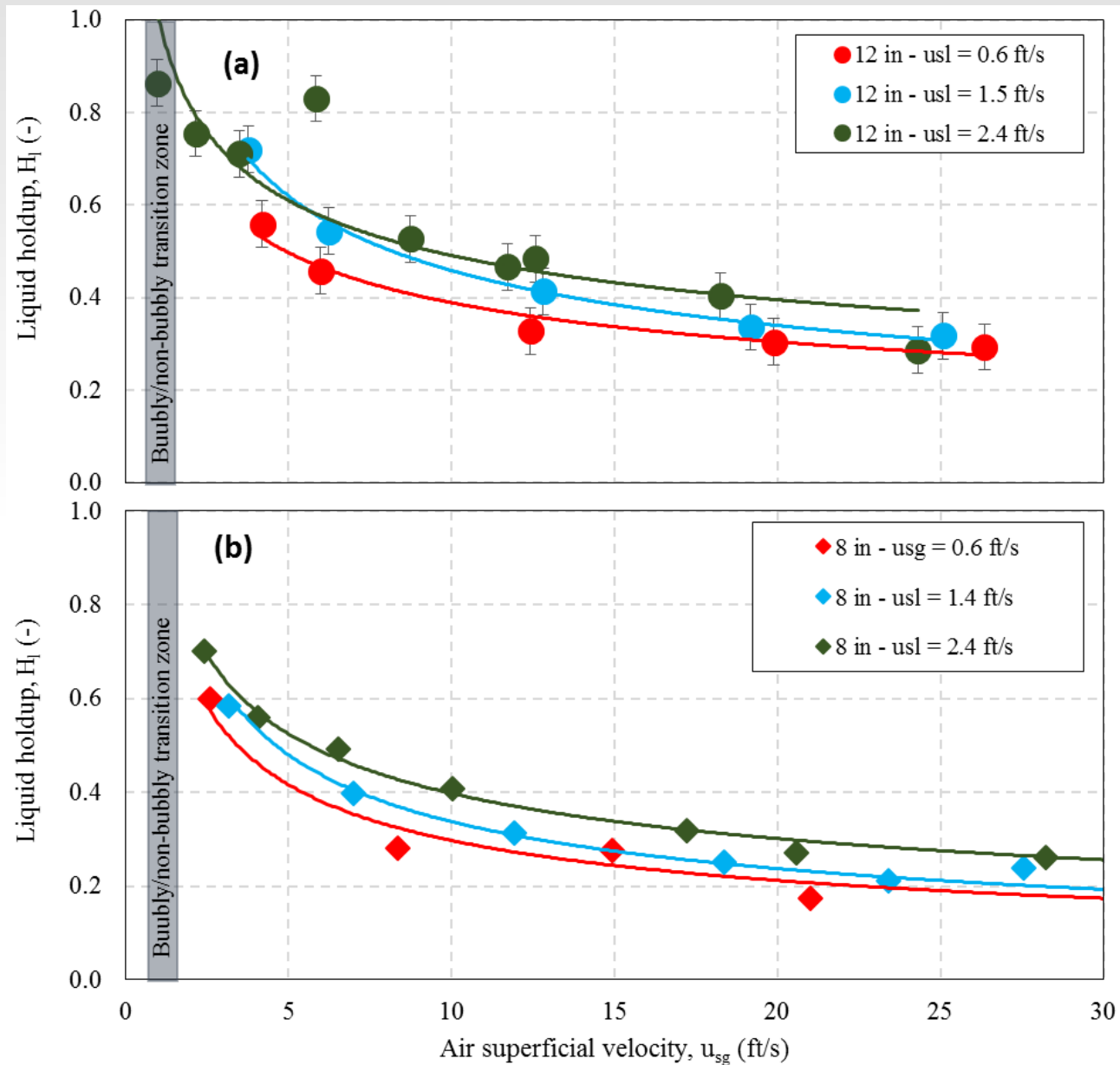
$$1.53 \left[ \frac{g(\rho_L - \rho_g)\sigma}{\rho_L^2} \right]^{0.25} (1 - \alpha)^{0.5} \sin(\theta) = \frac{u_{sg}}{\alpha} - 1.2(u_{sl} + u_{sg})$$

# Liquid Holdup Measurements [2]





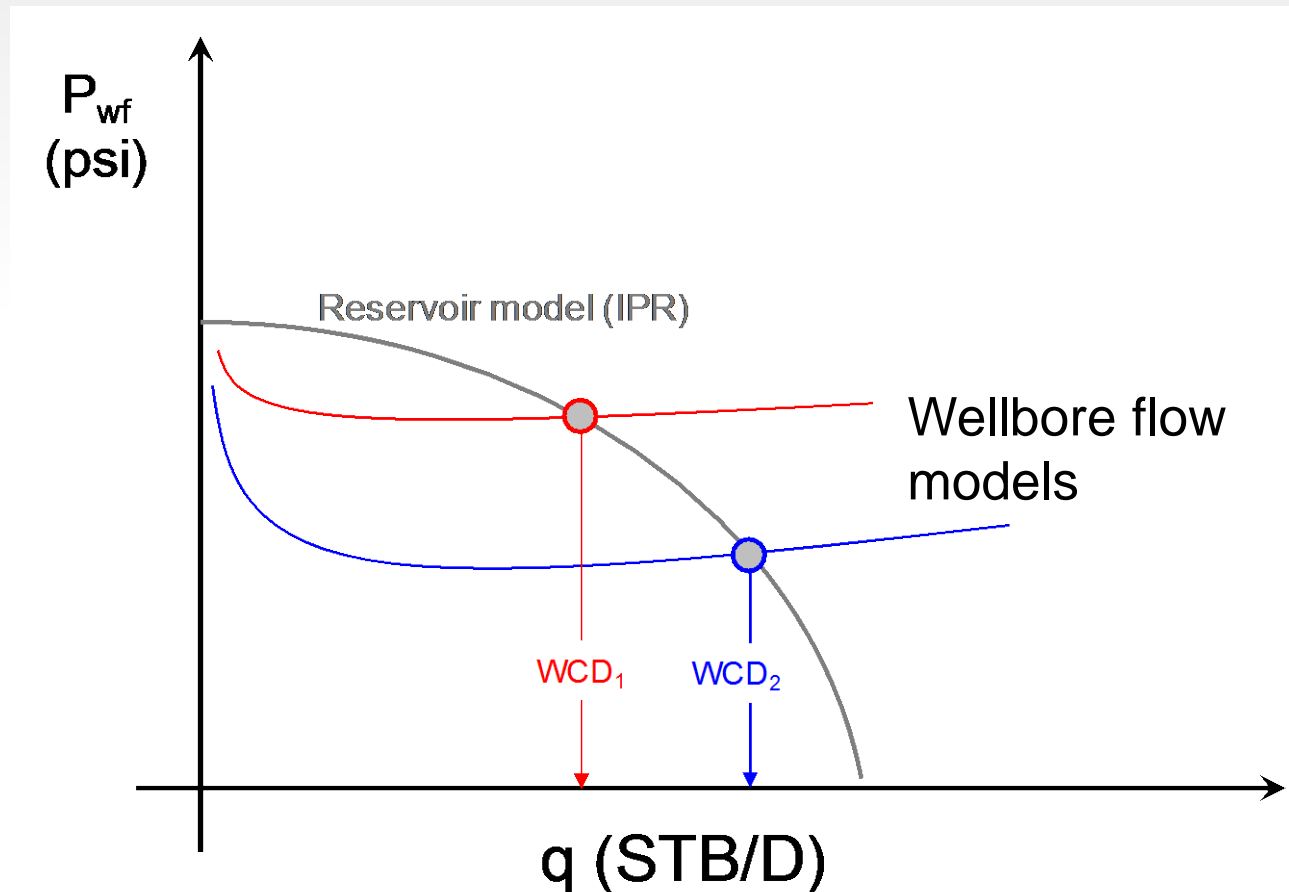
# Liquid Holdup Measurements [3]



$$\bar{\rho} = H_l \rho_l + (1 - H_l) \rho_g$$

# $\Delta p / \Delta z$ Measurements [1]

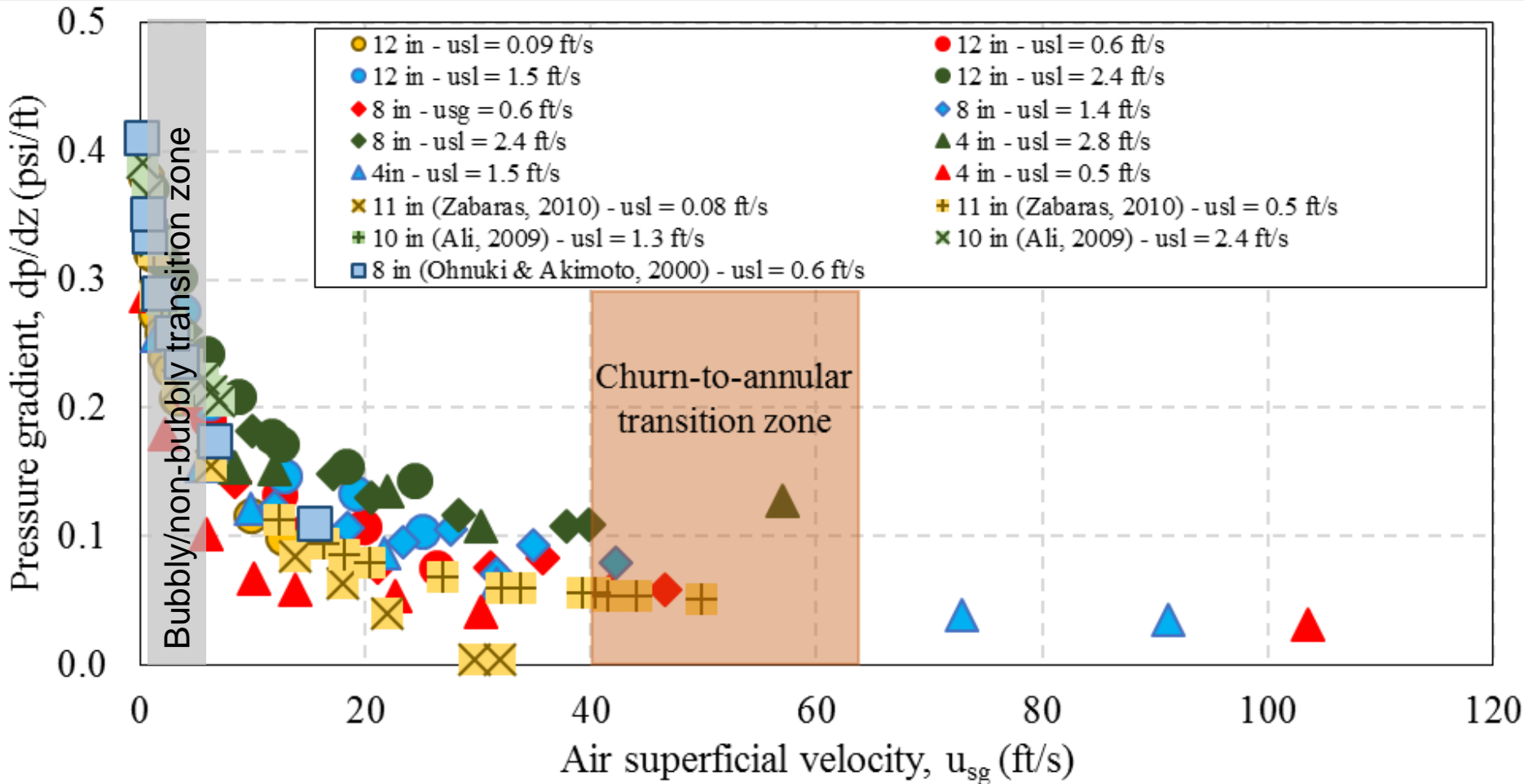
$$\frac{dp}{dz} = \underbrace{\frac{g}{g_c} \bar{\rho}}_{\text{gravitational}} + \underbrace{\frac{2 f \bar{\rho} u_m^2}{14.22 D}}_{\text{friction}} + \underbrace{\bar{\rho} \frac{\Delta(u_m^2 / 2 g_c)}{1.44 \Delta z}}_{\text{acceleration}}$$



$$\bar{\rho} = H_l \rho_l + (1 - H_l) \rho_g$$

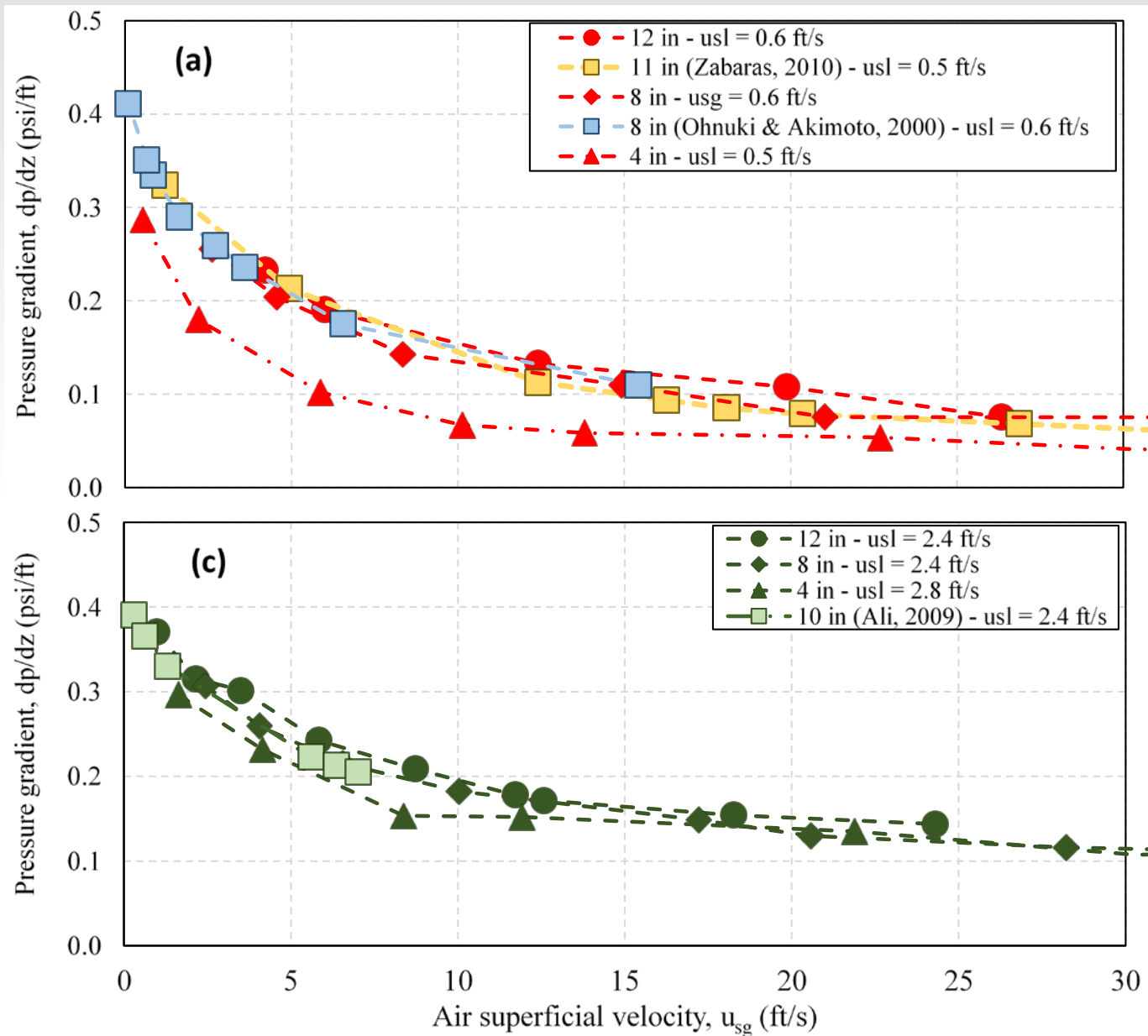
# $\Delta p/\Delta z$ Measurements [2]

$$\frac{dp}{dz} = \underbrace{\frac{g}{g_c} \bar{\rho}}_{\text{gravitational}} + \underbrace{\frac{2f\bar{v}_m^2}{4.8D}}_{\text{friction}} + \underbrace{\bar{\rho} \frac{\Delta(u_m^2/2g_c)}{1442443}}_{\text{acceleration}}$$





# $\Delta p/\Delta z$ Measurements [3]



# Conclusions from Experimental Investigation

- ❑ As previously observed by other investigators, **slug flow was not observed** for pipe **diameter larger than 4 inches**
- ❑ **Good match** between the flow regimes,  $H_l$  and  $dp/dz$  measured in this study and reported by **other authors**
- ❑ Surprisingly, the **pipe diameter has negligible effect** on the  **$dp/dz$**  for pipe **diameters over 4 inches**
- ❑ **Liquid flow rate** has **small effects on  $dp/dz$**  for  $ID > 4$  in, particularly for **high-liquid velocities**
- ❑ **Axial flow development** does **not seem to impact** significantly the  $dp/dz$  in large-diameter pipes ( **$ID > 4$  in**)

# **Evaluation of Flow Models with Experimental Data (*Task 6*)**

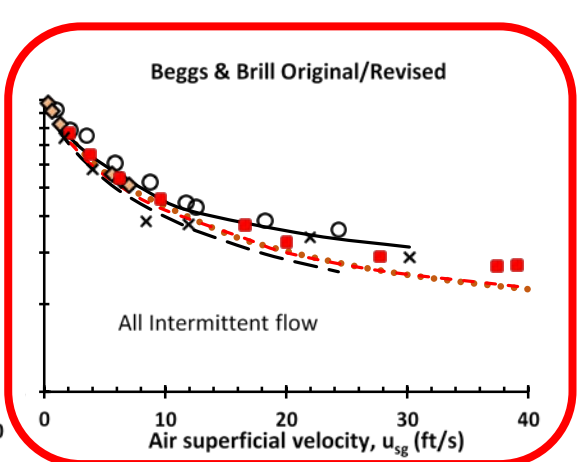
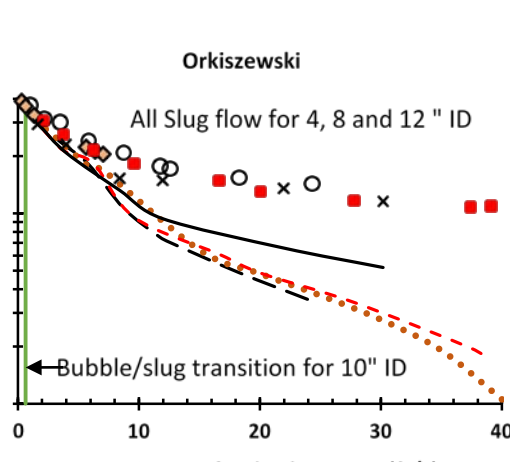
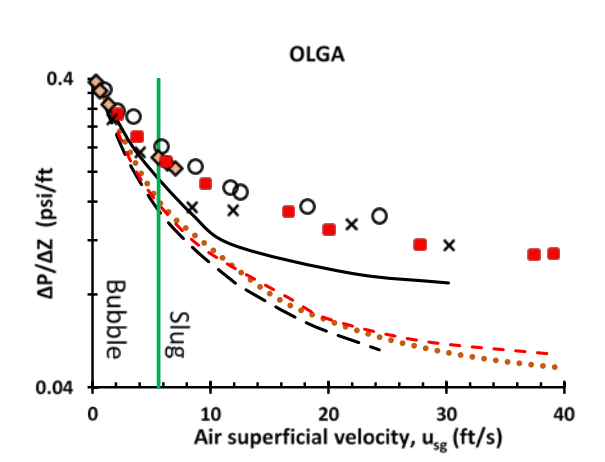
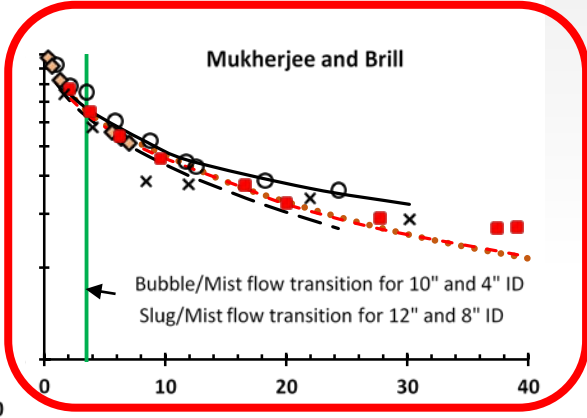
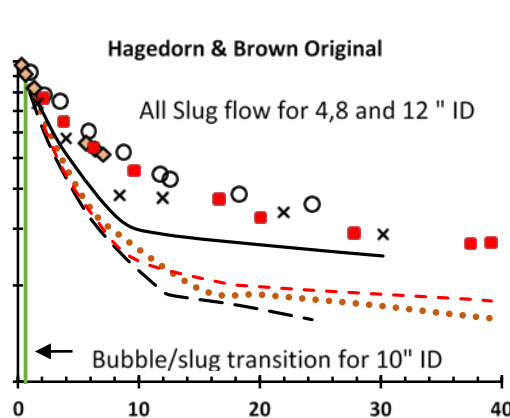
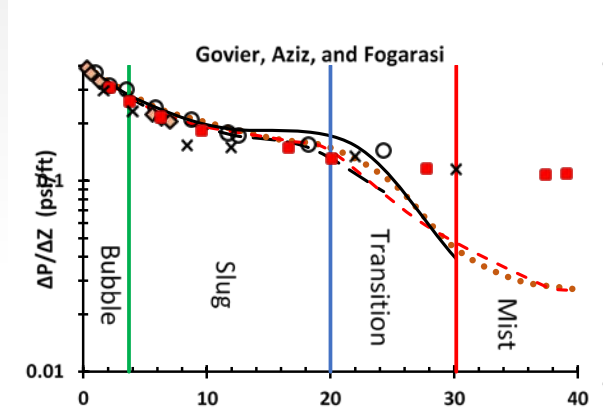
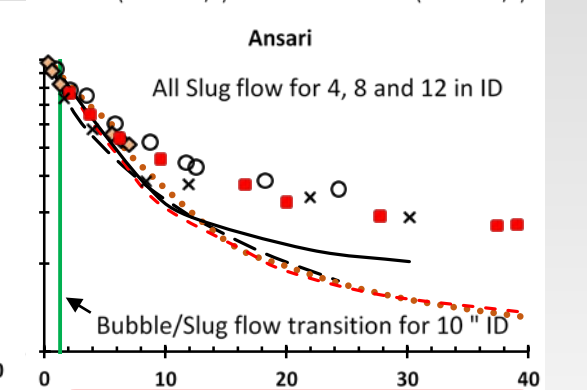
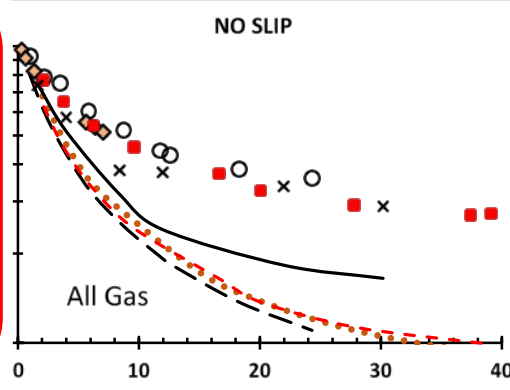
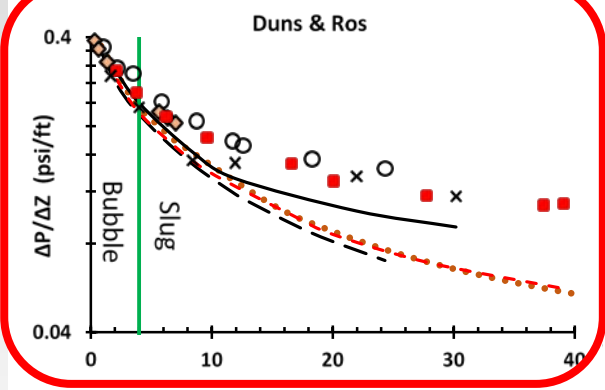
# Methodology for Comparison of Flow Models

Wellbore flow model	Nomenclature
Ansari (1994)	ANS
Beggs and Brill (1973)	BB
Beggs and Brill Revised (1979)	BBR
Duns and Ross (1963)	DR
Govier, Aziz, and Fogarasi (1972)	GA
Gray Original (1974)	GO
Gray modified (PipeSim 2011)	GM
Hagedorn and Brown (1964)	HB
Hagedorn and Brown with Duns and Ross map (PipeSim 2011)	HBDR
Mukherjee and Brill (1985)	MB
No Slip (PipeSim 2011)	NS
Orkiszewski (1967)	OR
OLGA-S 2000 V.6.7.2	OLGA
Computational Fluid Dynamics (Fluent)	CFD

- Common models available in commercial packages
- Models available in PIPESIM at LSU
- Include different model approaches (empirical, mechanistic, CFD)

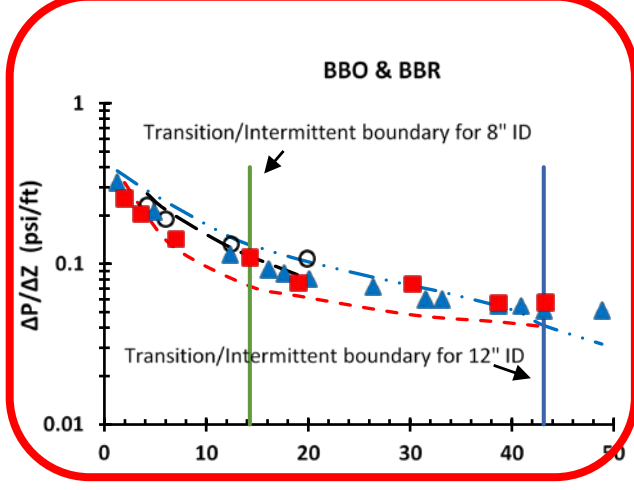
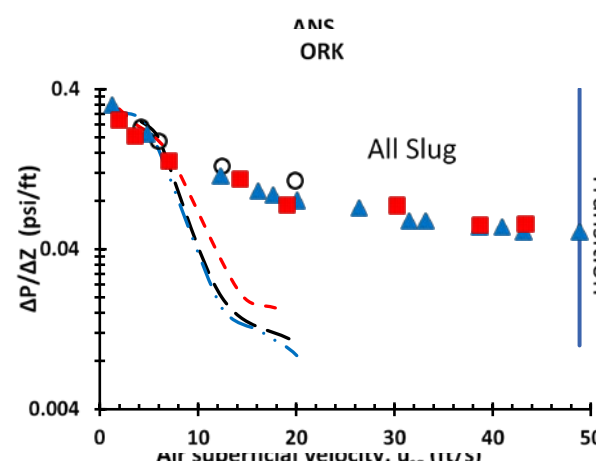
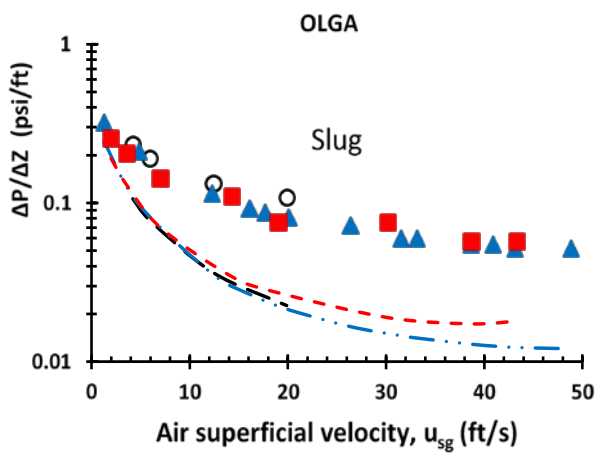
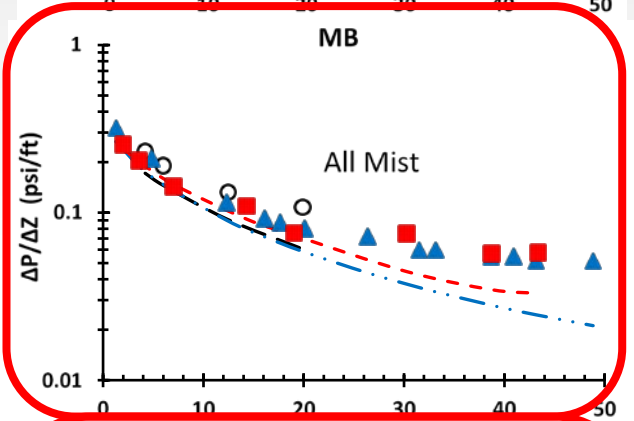
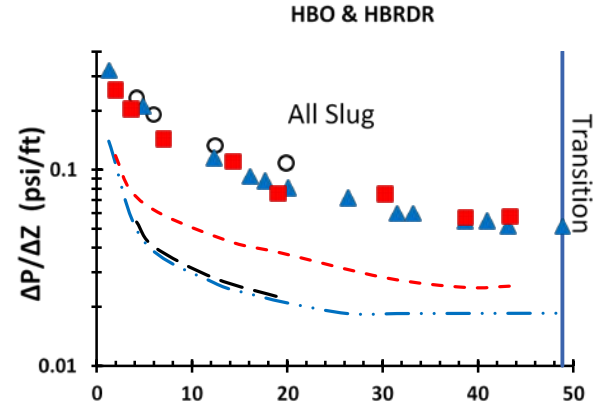
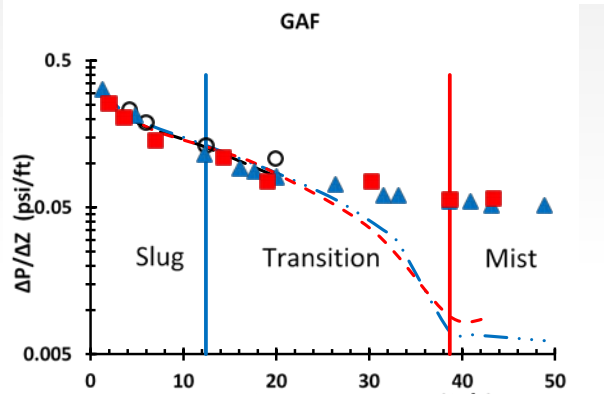
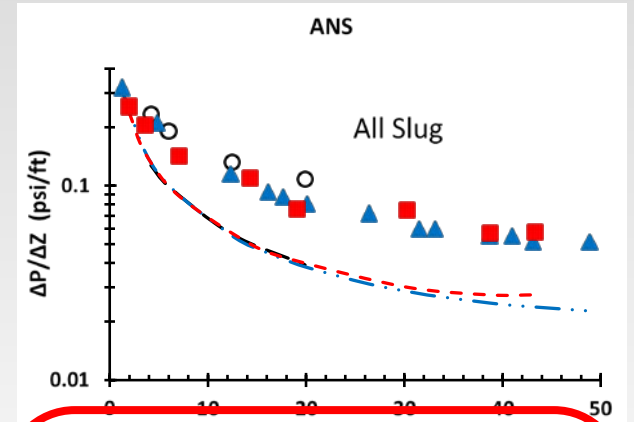
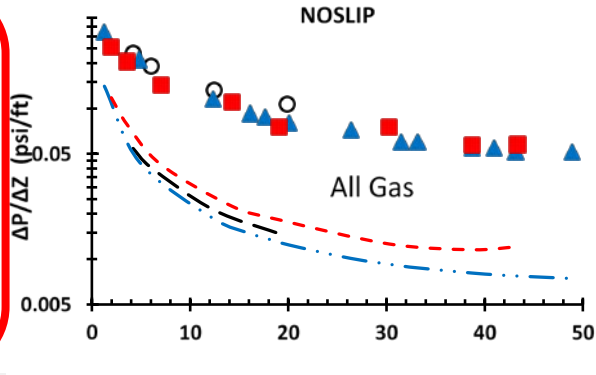
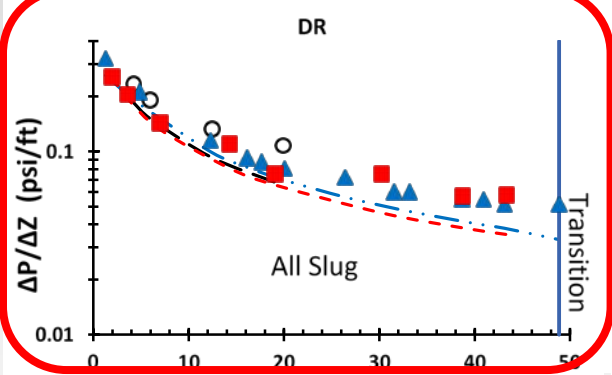
# p. Data and Flow Model Results

- 12 in (usl=2.4 ft/s)    ●●●● 10 in (usl=2.4 ft/s)
- - - 8 in (usl=2.4 ft/s)    — 4 in (usl=2.9 ft/s)
- 12 in (usl=2.4 ft/s)    ◆ 10 in (usl=2.4 ft/s)
- 8 in (usl=2.4 ft/s)    × 4 in (usl=2.9 ft/s)

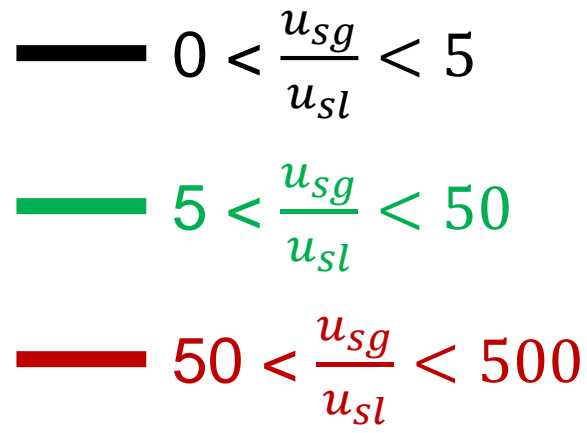
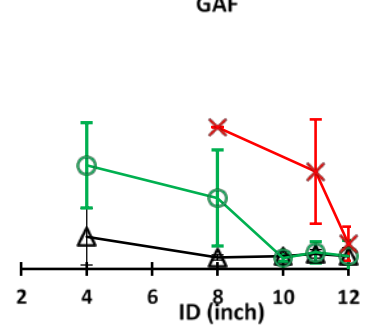
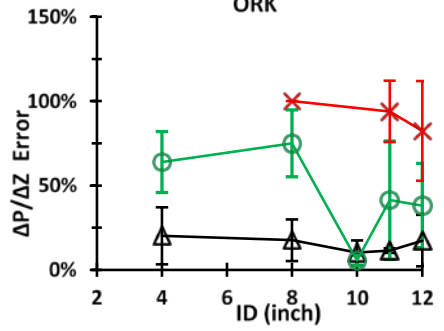
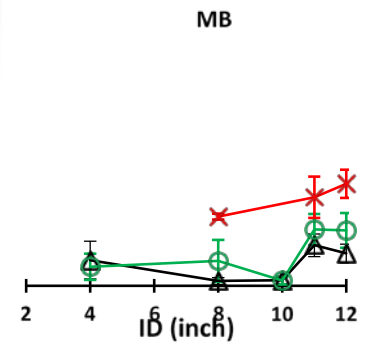
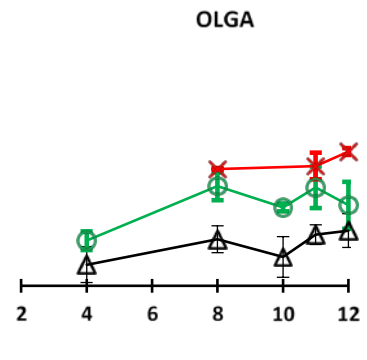
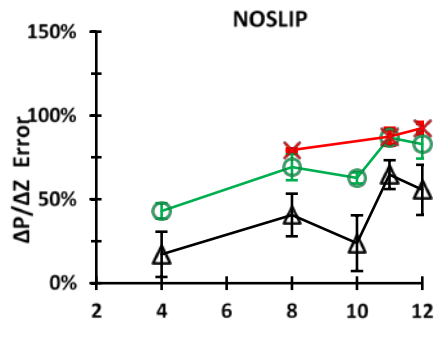
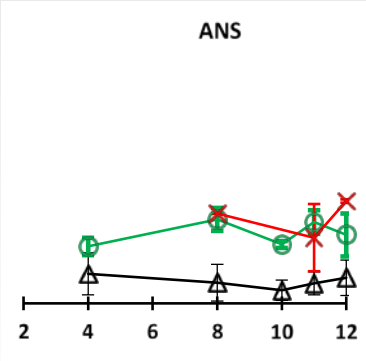
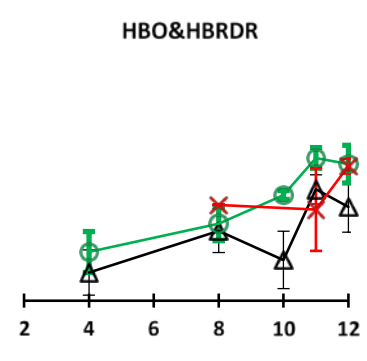
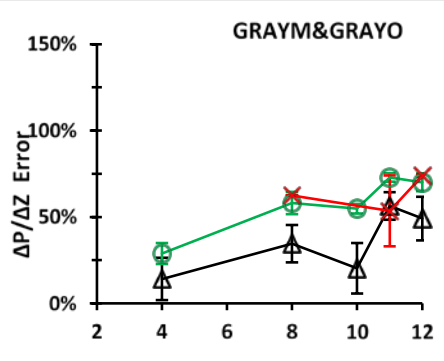
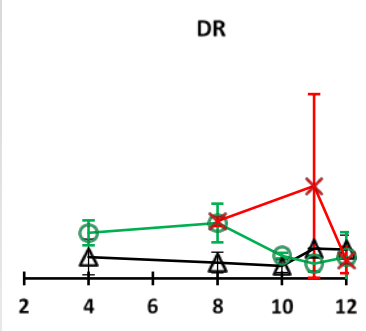
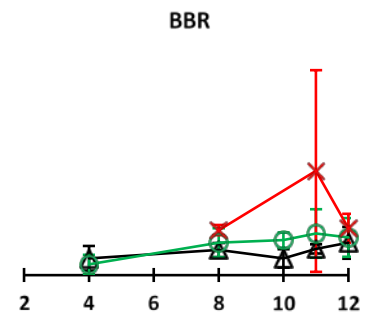
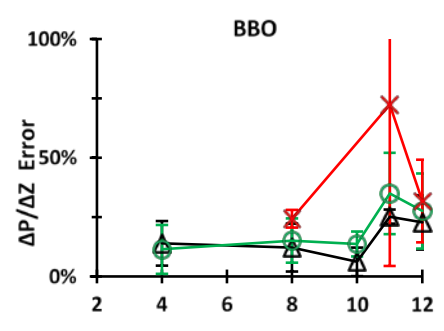


# Exp. Data and Flow Model Results for

- 12 in (usl=0.6 ft/s)
- - - 11 in (usl=0.5 ft/s)
- - - 8 in (usl=0.7 ft/s)
- 12 in (usl=0.6 ft/s)
- ▲ 11 in (usl=0.5 ft/s)
- 8 in (usl=0.7 ft/s)



Data points from:  
 LSU (2016), Ali (2009),  
 Zabararas et al. (2013)





# Oh My God

I NEED A BREAK ....

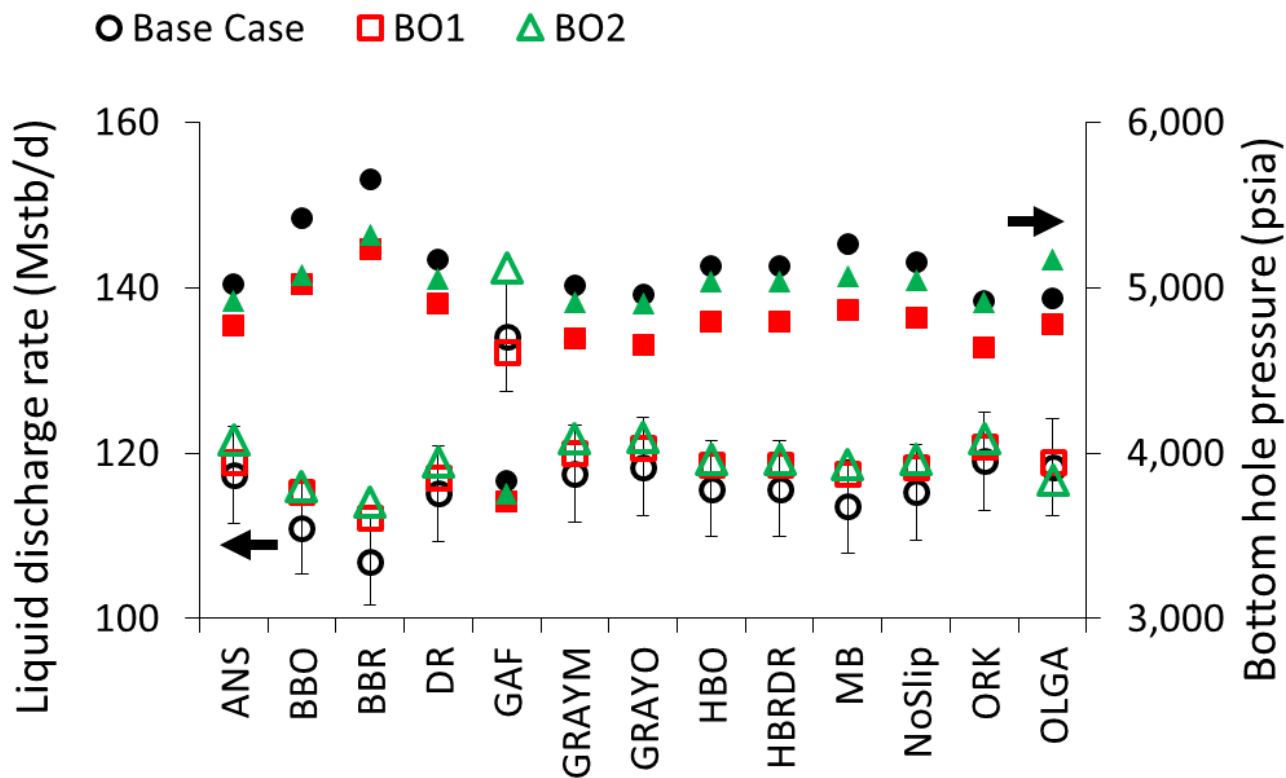


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# **Comparison of Flow Models Applied to WCD (*Task 2*)**

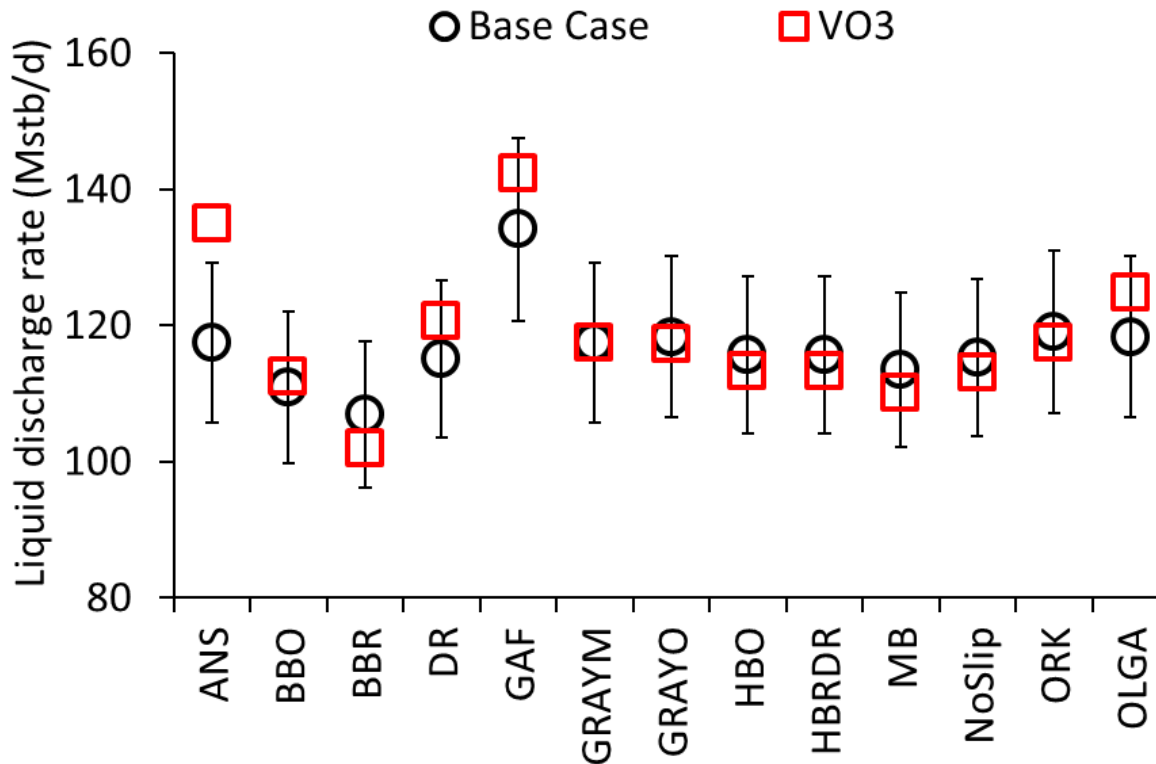
# Results for WCD Calculations for Different Wellbore Flow Models

Fluid Sample	Reservoir depth (ft)	Reservoir pressure (psi)	Reservoir Temp. (°F)	GOR (scf/stb)	$p_{bp}$ (psi)	$\rho_o$ (API)	$\mu_o$ (cp)	PI (STB/D/psi)
Base Case	16,726	11,305	210	1,700	6,306	28	0.8	19.05
BO1	19,426	10,391	166	1,190	7,693	25.3	1.49	19.05
BO2	19,553	12,523	251	1,562	5,192	34.5	0.173	19.05

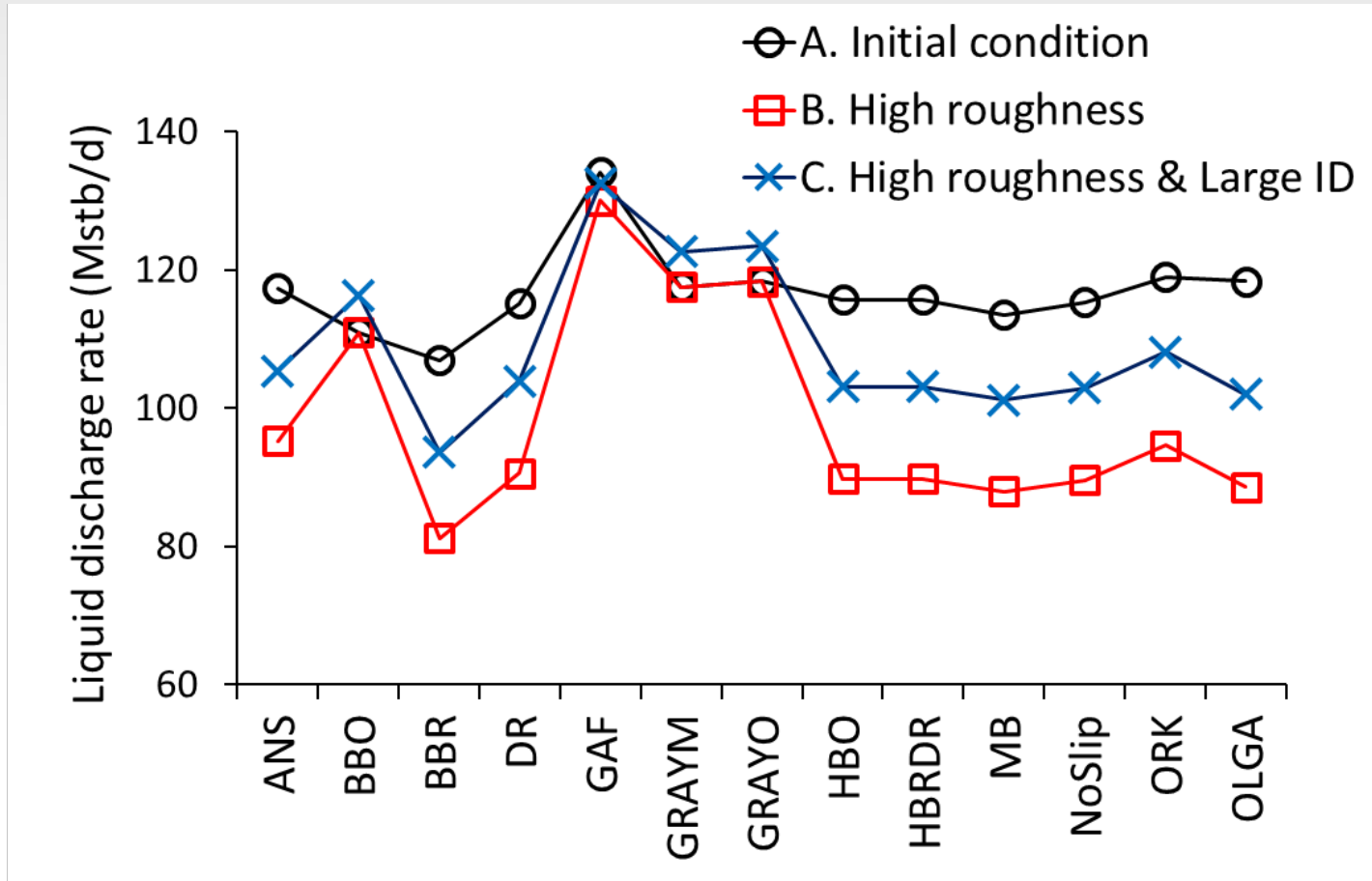


# Effect of Fluid Type

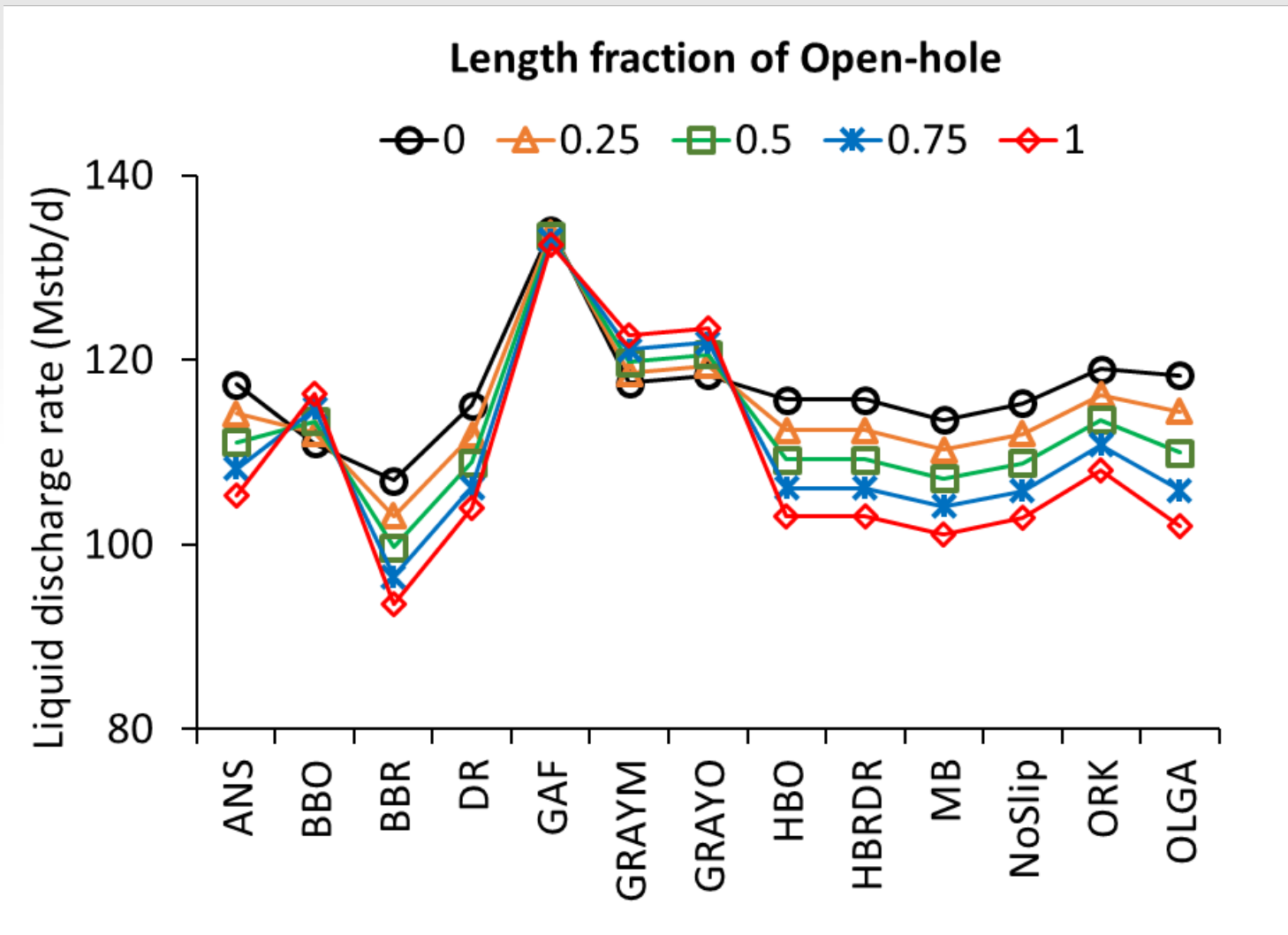
Fluid Sample	Reservoir measured depth (ft)	Reservoir pressure (psi)	Reservoir Temperature (°F)	GOR (scf/stb)	Oil gravity (API)	PI (STB/D/psi)
Base Case	16,726	11,305	210	1,700	28	19.05
VO3	14,374	11,009	261	3,803	42.1	19.05



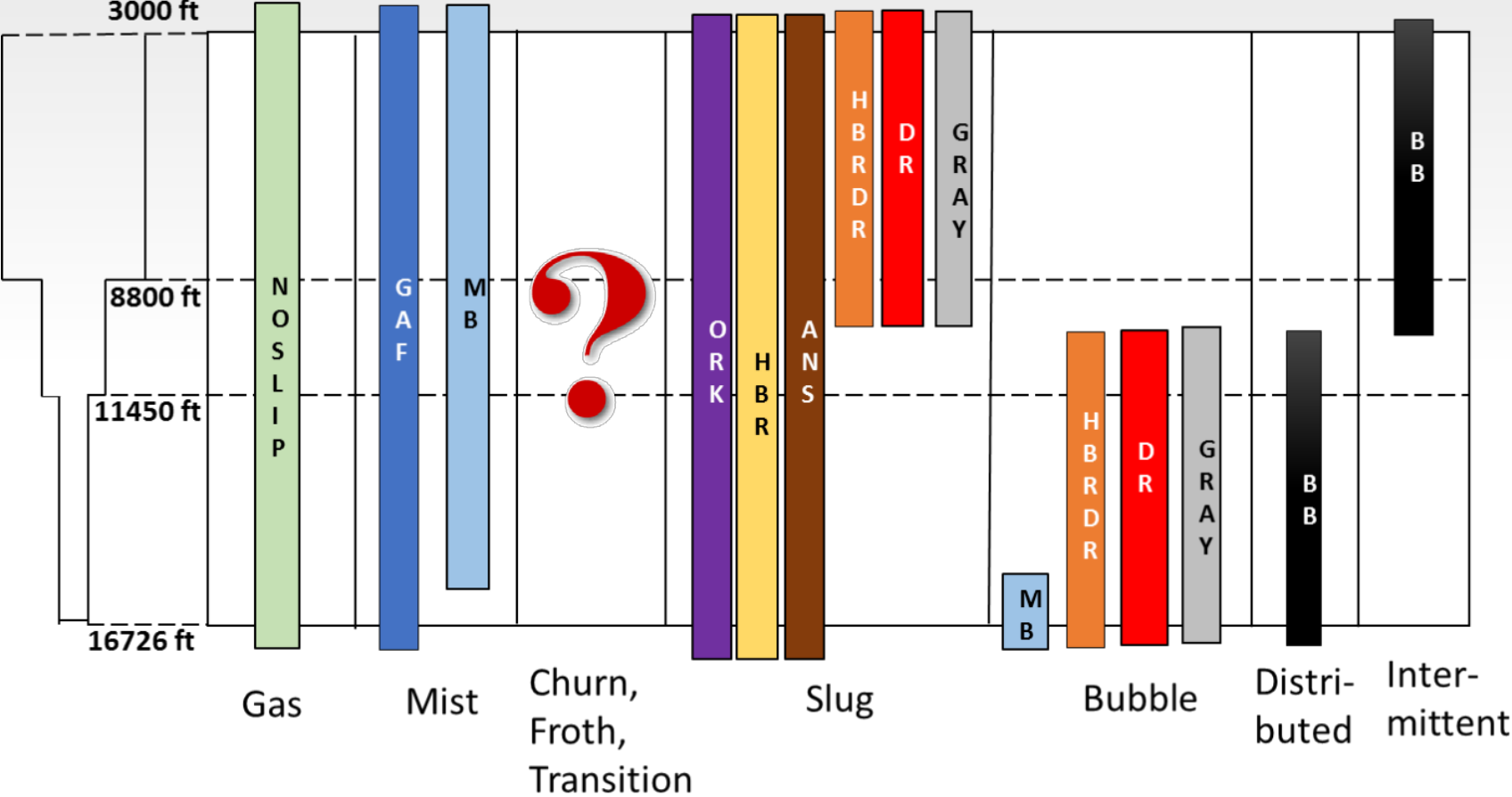
# Effect of Roughness [1]



# Effect of Roughness [2]




# Results for Flow Regime Prediction for Base Case





# Final Remarks

- ✓ We have done a **significant amount of work in 12 months.** 
- ✓ **Pipe diameter** has a significantly **smaller effect** on the **pressure gradient** for ID **over 4 inches** than in pipe diameter smaller than 4 inches.
- ✓ Most **flow models** show **better results for the 4-inch diameter** pipe than for larger diameters.
- ✓ **Flow models** and **laboratory experiments discrepancy** is likely caused by the **use of the slug flow regime, instead of churn flow** (which is observed experimentally)

# Final Remarks

- ✓ **Different methods** may be suggested for **different fluid and flow conditions**, making the **recommended practice field specific** depending on reservoir and fluid properties
- ✓ Variation of **reservoir fluid properties** ( $p_{bp}$ , GOR,  $\rho_o$ ,  $\mu_o$ ) has a relatively **small effect (up to 10%)** on **WCD rate estimates** for black oil and volatile oil reservoirs, **for the well conditions examined**
- ✓ **Further investigations** of benchmarking and **calibration** of existing WCD models against representative **field and fluid WCD conditions is needed!**
- ✓ Based on preliminary comparisons, **significant improvement** can be achieved on **wellbore flow models for WCD calculations**

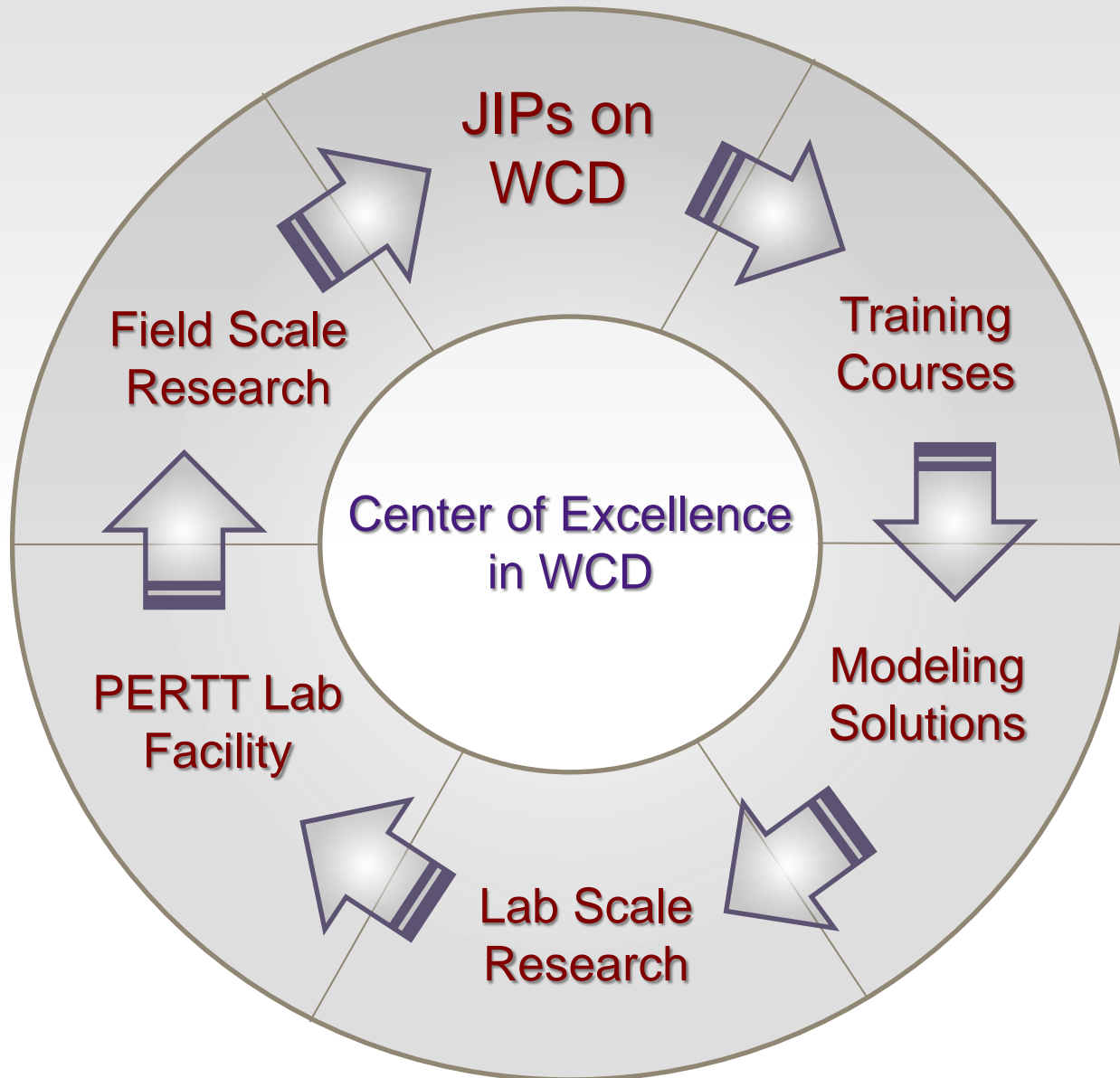
# Suggestion for Future Projects

## □ Five-year Research Plan (LSU WCD Group)

*“ To foster **safety on the development of new oil and gas reserves in the Gulf-of-Mexico**”*

- ✓ Establish a WCD Research Center at LSU
- ✓ Organize a Industry Advisory Committee (IAC) for the WCD group
- ✓ Create a Priority List for topics to address challenges on WCD
- ✓ Organize a Joint-Industry-Project (JIP) on the validation and development of a Open-Source model for WCD calculations
- ✓ Create a Handbook/Manual/Standard and Training Courses for WCD calculations (standardization)
- ✓ Disseminate information from LSU WCD group among industry and regulatory agencies

# LSU WCD Research Center

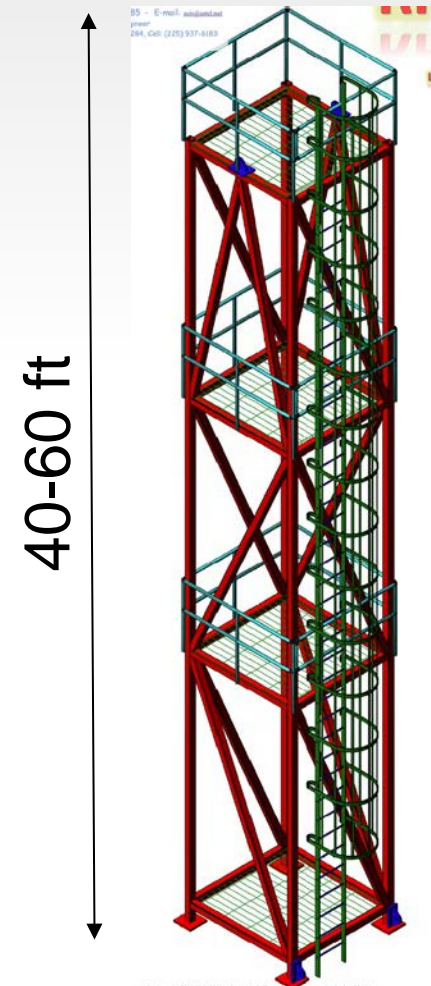


# Preliminary Priority List of Topics [1]

- ❑ Experimental work for large pipe diameters **and inclined pipe!** (No well is **truly vertical!!!**)

New design under development  
(Investment of ~\$150,000)

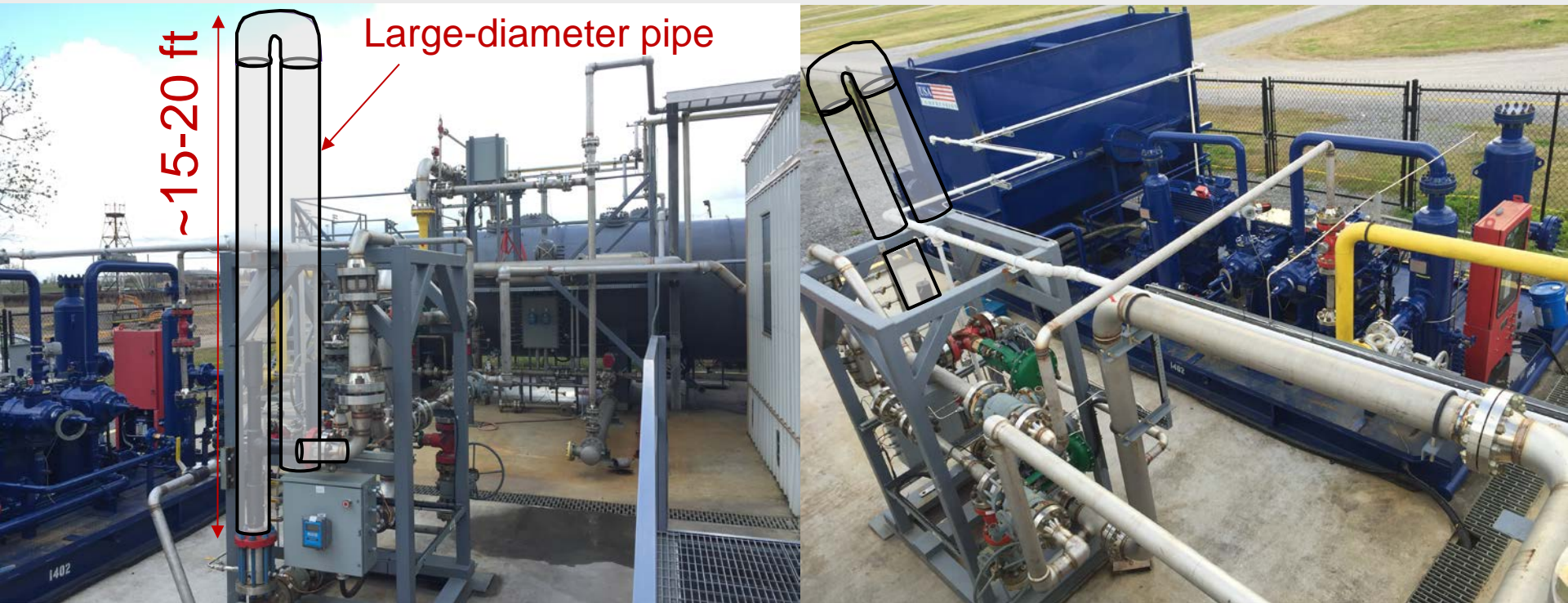
Old Inclinable flow loop





# Preliminary Priority List of Topics [2]

- ❑ Flow tests for different **pressures and fluid types** (fluids other than water and air)



- ✓ Industry investment already made of about ~\$ 2,000,000
- ✓ Closed-loop that allow use of different fluid types (oil, gas, water, nitrogen...)
- ✓ Allow use of pressures up to 1,200 psi
- ✓ Allow tests with high-liquid rates (15,000 BBL/D) and high-gas rates (4 MMSCFD)

# Preliminary Priority List of Topics [3]

- ❑ Development of a **Flow Models dedicated to WCD calculations**
- ❑ Development of a **web tool to provide unbiased and accurate WCD calculations**

Validation with 24 wells – Reinicke et al. (1987)

Validation with 12 wells – Facher and Brown (1963)

