

SPERRY-SUN DRILLING SERVICES
LOGGING SYSTEMS
Anchorage, Alaska



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FINAL
ADT WELL SUMMARY REPORT
ARCO Alaska, Inc.
OCS-Y-0865 No. 1 & OCS-Y-0866 No. 2
Kuvlum No. 2 & Kuvlum No. 3
Beaufort Sea, Alaska

OCS DISTRICT OFFICE

NOV 18 1993

MINERALS MANAGEMENT SERVICE
ANCHORAGE, ALASKA

Final Report Summary
October 1993

PREPARED FOR:
ARCO Alaska, Inc.

PREPARED BY:
John Patton & Don Walters
Sperry-Sun Drilling Services
Logging Systems
Anchorage, Alaska

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INTRODUCTION

Drilling operations for OCS-Y-0865 No. 1, the second well on the Kuvlum Prospect, were initiated 7-19-93 by ARCO Alaska, Inc. The well was drilled by Canmar's CDU Kulluk on a location in NR6-4 Block 672 of the Beaufort Sea, offshore Alaska. Kuvlum No. 2 was drilled to a total depth of 11125' on 8-20-93. The total number of operating days that were required to reach 11125' was 24 days from spud. After logging operations were completed, the well was plugged and abandoned on 8-27-93.

Drilling operations for OCS-Y-0866 No. 2, Kuvlum No. 3, were initiated on 9-9-93 after moving the Kulluk to a new location on NR6-4 block 673. This is the same block that the first Kuvlum well was completed during last years drilling season. Kuvlum No. 3 was drilled to a total depth of 8000' on 9-28-93, requiring a total of 20 operating days to complete. The well was plugged and abandoned on 10-4-93 after successfully evaluating the well with electric logs.

A Sperry-Sun Logging Systems MPT/2000 Unit was in operation from surface to TD providing full mud logging, applied drilling technology, and Mud Pulse-MWD services. The MPT/2000 Unit and crew provided essential assistance in the drilling of Kuvlum No. 2 & No. 3 by monitoring intrinsic drilling parameters and gas levels. Also provided were real-time Gamma Ray and EWR information, directional surveys, fluid hydraulics information, pore pressure vs. necessary mud weight evaluations, and a wide range of geological interpretations and sampling services.

The following pages of this report are designed to supply concise historical data of the events that occurred on both of these wells, along with some analysis and recommendations for specific problems that were experienced during different sections of the hole. All of the information compiled in this report was acquired and recorded by the MPT/2000 Unit at the well site.

The sensors incorporated in this unit are independent from the rig sensors and may differ slightly from those reported by the rig contractor. In addition, any evaluations in this report regarding formation evaluations, pore pressure estimates, or other geologic interpretations are made entirely by Sperry-Sun personnel from on site examination of drill cutting samples and pertinent data supplied solely by the MPT/2000 Unit.

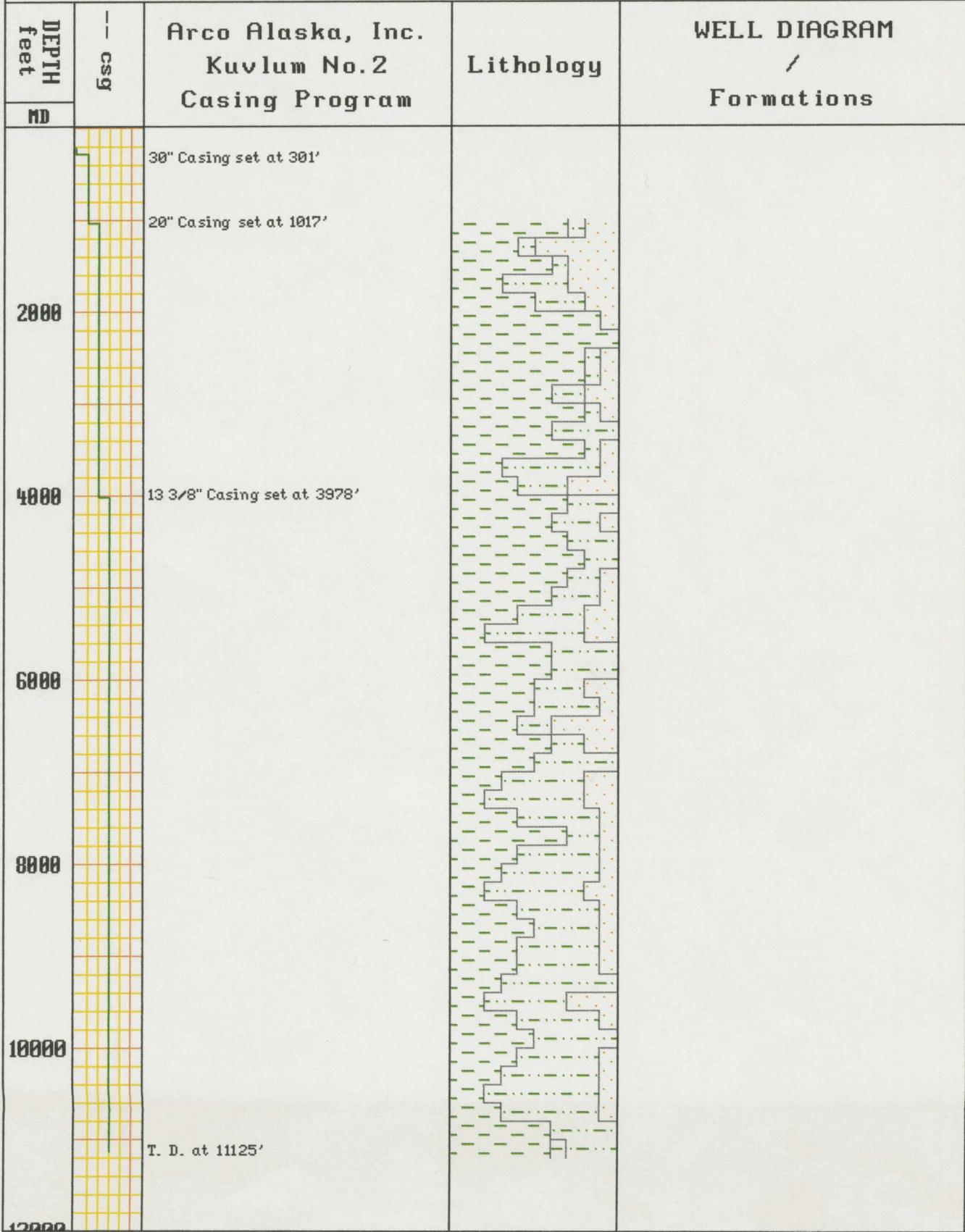
**SPERRY-SUN DRILLING SERVICES
ALASKA DISTRICT**

**SPERRY SUN
LOGGING
SYSTEMS**

WELL OCS-Y-0865 NO. 1
 COMPANY ARCO ALASKA, INC.
 LOCATION BLOCK 672, BEAUFORT SEA, AK.

**WELL
DIAGRAM**

3



SPERRY-SUN DRILLING SERVICES
ALASKA DISTRICT

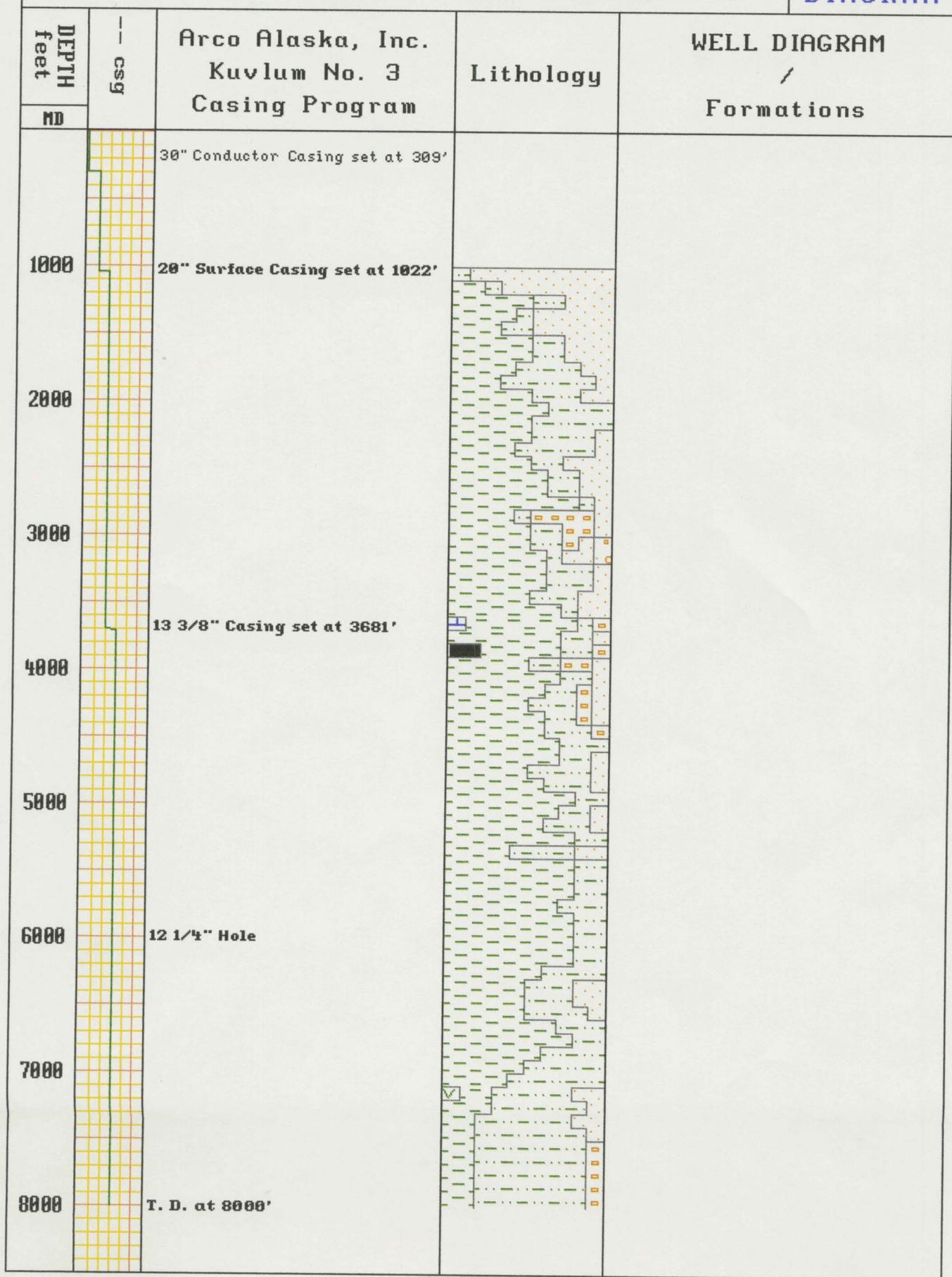
BAROID
LOGGING
SYSTEMS

WELL OCS-Y-0866-2 KUVLUM NO. 3

COMPANY ARCO ALASKA, INC.

LOCATION NR6-4 BLK 673, BEAUFORT SEA, AK.

WELL
DIAGRAM



WELL SUMMARY BY INTERVALS

4

KUVLUM NO. 2

Interval: 226' to 1030'

Days:	6	Average WOB:	21 klb
Hole Size:	26"	Average RPM:	83
No. Bits:	1	Average GPM:	1015
Rotating Hours:	33.7	Average SPP:	1875 psi
Deviation:	NA deg	Average ROP:	23 ft/hr
Mud Weight:	8.5 ppg	Mud Type:	Sea Water

Discussion:

The Canmar Kulluk was positioned on location prior to the spud in date of 7-28-93. Drilling operations were initiated by drilling a large diameter glory hole from the mud line at 167' to a depth of 211' to allow for the positioning of the blow out preventer stack below the ocean floor. A 24' diameter caisson was washed down with the glory hole bit to provide a barrier from sediments falling back into hole. Penetration rates for this large diameter hole were slow due to mechanical problems with the glory hole bit. Three additional trips were needed to repair this bit before completing the glory hole on 7-27-93.

After landing a temporary guide base, 30" - 310 lb/ft casing was jet drilled to 296' in conjunction with Bit No. 1. With the 30" casing landed on the guide base, drilling was continued with Bit No. 1 using a mud motor and without returns to surface as the riser system had not been connected. An air lift system was then installed at the glory hole to help remove cuttings from this area with some of the returns passed through the shaker box. Formation gasses were monitored during this interval with this system. A maximum gas of 8 units was recorded during this process while the background gas averaged 5 units. The 26" hole was drilled to a depth of 1030' on 7-31-93 occasionally pumping high viscosity sweeps to clean the hole. 20" - 133 lb/ft casing was then run and cemented to a depth of 1017'. No hole problems were encountered while drilling this section of the well.

Interval: 1,030' to 4005'

Days:	8	Average WOB:	14 klb
Hole Size:	12.25/17.5"	Average RPM:	122
No. Bits:	2	Average GPM:	720
Rotating Hours:	37.3	Average SPP:	2400 psi
Deviation:	.39 deg	Average ROP:	88 ft/hr
Mud Weight:	9.8 ppg	Mud Type:	PHPA

Discussion:

The blow out preventer stack was run on the riser assembly and landed on the well head housing allowing for mud returns to surface. The BOP Stack and the 20" casing were pressure tested to 2200 psi prior to drilling ahead with Bit No. 2.

The seawater mud system was replaced with 9.8 ppg seawater-PHPA mud prior to drilling the 20" casing shoe. Bit No. 2, a 17.5" bit, was used to drill out the 20" conductor casing along with 10' of new hole to 1,040' on 8-2-92. A leak off test was performed at this depth yielding a fracture pressure equivalent mud weight of 12.9 ppg.

Bit No. 2 was then pulled out of the hole and replaced with a 12.25" bit. Bit No. 3 was then used to drill ahead through clay and sand at a controlled drilling rate of 100± feet per hour to a depth of 2430' where a short trip was made to clean hole. On the way out, the hole pulled tight at 1766'. The hole was then washed and reamed from 1729' to 1761' and at 2380' on the trip back into the hole. The maximum gas recorded from circulating bottoms up on the trip was 61 units. Bit 3 drilled through clay, siltstone, and sand to 4005'. The estimated pore pressure during this interval was 8.5-8.7 ppg while maintaining the mud weight at 9.8 ppg.

Upon reaching the interval depth of 4005', the hole was conditioned with a short trip to the shoe that experienced drag on the way out that was probably due to swelling clays or possibly drill cuttings adhering to the borehole. Because of the excess drag, the hole was back reamed from 3561' to 1016'. The maximum gas from this short trip gas was 85 units. The hole was then circulated and conditioned in preparation for running electric logs.

Electric logs were successfully run and operations to open the hole were initiated on 8-7-93 with Bit No. 3 was run into the hole ahead of a 17.5" hole opener. Drilling rates were very good during the hole opening process. The hole was then conditioned with a short trip in preparation for running casing. On the trip out, the pipe was back reamed and pumped out of hole due to tight hole conditions and then washed and reamed back to bottom. The maximum short trip gas

was 60 units. 13³/₈" - 68 lbs/ft casing was landed at a total depth of 3978'. This casing was cemented in place without problems.

Lithologies of this section consisted of sand, clay, and siltstone with traces of limestone, gravel, and coal. No abnormal gas readings or any indication of gas hydrates were encountered. The pore pressure estimate for this section of the hole was 8.5-8.7 ppg, a normal gradient. Hole problems for the interval were attributed to swelling clays-siltstones and some bit balling.

Interval: 4,005' to 11,125'

Days:	10	Average WOB:	10-20 klb
Hole Size:	12.25"	Average RPM:	145
No. Bits:	5	Average GPM:	620/700
Rotating Hours:	99.4	Average SPP:	3000 psi
Deviation:	4.03 deg (max)	Average ROP:	80 ft/hr
Mud Weight:	9.8-10.7 ppg	Mud Type:	PHPA

Discussion:

The Blow Out Preventers were tested prior to running in the hole with Bit No. 4. The 13 3/8" casing was tested to 3500 psi. Bit No. 4 was then used to drill the cement, the float collar, and the shoe along with 10' of new formation to 4015'. A leak-off test was performed at this depth and realized a test of 14.9 ppg equivalent mud weight without breaking down. This value differs somewhat from a calculated value of 13.9 ppg at this depth using the Eaton Method for estimating the fracture gradient in shales.

After completing the leak-off test, Bit No. 4 was used to drill to 5525' where a short trip to the shoe was performed to condition the hole. The hole pulled tight and had to be back reamed and pumped out of hole. The trip gas reading from this short trip was 95 units. While drilling ahead, the mud weight was raised to 10.0 ppg to stabilize hole conditions on trips. Drilling continued with this bit to 6593' where Bit No. 4 was pulled out of the hole. Connection gas readings were consistently logged below 4300'. A slightly increasing pore pressure trend noted on pressure plots. The estimated pore pressure was raised to 9.0 ppg in reference to this data.

Bit No. 5, a PDC type bit, was run back in the hole on the same bottom hole assembly. Drilling continued with this bit to 6729'. The decision was made to core this interval due to a potential show indicated from information provided by the MWD tool in addition to previous shows of oil fluorescence in the drill cutting samples. The hole was then circulated out and conditioned for a coring run. Bit No. 5 was pulled without encountering excessive drag.

Core Bit No.1 was then run in the hole. The trip gas from bottom was 246 units. After getting on bottom with the core bit, penetration rates were very slow. Core bit No.1 was pulled at 6732' after attempting to core for only 3 feet. There was no core recovery. The core bit was apparently balling up due to clay.

Bit No. 5RR was run back in hole to continue drilling. The trip gas reading from bottom was 142 units. Penetration rates were good while drilling ahead through clay, siltstone, and sand to 7698' where a short trip to the shoe was made to condition hole. The hole again pulled tight and

was back reamed from 6842' to 6570'. The maximum trip gas was 625 units, a notable increase from the previous trip. Drilling continued with Bit No. 5RR to 9500' where it was pulled out of hole for BOP test. Tight hole conditions again required pumping out of hole from bottom to a depth of 7620'.

A pressure trend was estimated to develop below 7000' using information detailed on the D-Exponent plot and a slight increase in recorded connection gas readings. The estimated pore pressure was raised to 9.4 ppg at 7675'. Additional evidence for a pressure transition zone was indicated by the Condensed Resistivity Plot during this interval. The pore pressure estimate was steadily increased to 9.7 ppg by 9500'. The mud weight was raised in two stages to 10.4 ppg for additional overbalance.

Bit No. 6, also a PDC type bit, was ran back into hole. The maximum trip gas from bottom was 1543 units. Very good penetration rates were achieved with this new bit. Drilling continued to 10551' where a short trip was made to condition hole. The trip gas after short trip was 683 units. Bit No. 6 then drilled ahead through a predominant siltstone/clay formation to the total depth of this well at 11125'. Resistivity and D-exponent data indicated an increasing pore pressure gradient continuous to about 10000'. The estimated formation pressure was raised to 9.9/10.0 ppg by this depth. The mud weight was increased to 10.7 ppg to provide for additional overbalance. The increasing pressure trend appeared to stabilize while drilling below 10000' and required no additional changes in pore pressure estimates or mud weight.

The hole was circulate out prior to running a short trip to shoe. Excess drag was noted while pulling pipe between 10261'-10071' and 9057' - 8767'. The hole was then circulate and condition in preparation for running E-logs. No tight hole problems were experienced while pulling out of hole for logs. Electric logging operations commenced on 8-21-93.

Logging operations were completed on 8-27-93. Operations to plug and abandon Kuvlum No. 2 were initiated on this date.

Lithologies of this section consisted of clay, thin bedded sands, hydrated shale, and siltstone. Minor shows of oil fluorescence were logged in sands below 6000'. Hole problems for the interval were minor and largely included tight hole conditions experienced on trips.

WELL SUMMARY BY INTERVALS

KUVLUM NO. 3

Interval: 230' to 1040'

Days:	4	Average WOB:	2/10 klb
Hole Size:	26"	Average RPM:	160
No. Bits:	1	Average GPM:	967
Rotating Hours:	26.7	Average SPP:	1375 psi
Deviation:	NA deg	Average ROP:	30.7 ft/hr
Mud Weight:	8.8 ppg	Mud Type:	Sea Water

Discussion:

The Canmar Kulluk was positioned on location prior to the spud in date of 9-9-93. Drilling operations were initiated by drilling a large diameter glory hole from the mud line at 172' to a depth of 211' to allow for the positioning of the blow out preventer stack below the ocean floor. A 24' diameter caisson was positioned in the glory hole to provide a barrier from sediments falling back into hole. The 24' caisson was washed down with the glory hole bit to 216'. The glory hole was completed on 9-10-93.

After landing a temporary guide base, a string of 30"- 310 lb/ft casing was jet drilled to 309' in conjunction with Bit No. 1. With the 30" casing landed on the guide base, drilling was continued with Bit No. 1 using a mud motor. No mud was returned to surface as the riser system had not been connected. An air lift system was then installed at the moon pool area to help remove cuttings from the base of the glory hole with some returns of sea water coming back through the shaker box. Formation gasses were sometimes monitored during the interval with this system. A maximum gas of 3 units was recorded during this process.

The 26" hole was drilled to a depth of 1040' on 9-11-93 while occasionally pumping high viscosity sweeps to clean the hole and then displaced with 9.6 ppg mud. A string of 20" - 133 lb/ft casing was then run and cemented to a depth of 1022'. The BOP stack was landed and pressure tested; however, the 20" casing failed to test. The casing was then cleaned out with Bit No. 2. A stinger was run inside the casing and a squeeze was made with 83 bbls of cement. The casing then tested to 2200 psi for 30 minutes.

Interval: 1,040' to 3705'

Days:	10	Average WOB:	15 klb
Hole Size:	12.25/17.5"	Average RPM:	118
No. Bits:	2	Average GPM:	633
Rotating Hours:	28.2	Average SPP:	2667 psi
Deviation:	.22 deg	Average ROP:	98 ft/hr
Mud Weight:	9.8 ppg	Mud Type:	PHPA-POLY

Discussion:

The seawater mud system was replaced with 9.8 ppg PHPA-polymer mud prior to drilling the casing shoe. Bit No. 2, a 17.5" bit, was used to drill out the 20" surface casing along with 10' of new hole to 1050' on 9-14-93. A leak off test was performed at this depth yielding a fracture pressure equivalent mud weight of 14.3 ppg.

Bit No. 2 was then pulled out of the hole and replaced with a 12.25" bit. Bit No. 3 was then used to drill ahead through clay and sand at a controlled drilling rate of 100⁺/ feet per hour to a depth of 2336' where a short trip was made to clean the hole. On the way out, the hole pulled tight at 1866' and the drill string was pumped and back reamed to the shoe. The maximum gas recorded from bottoms up from this trip was 153 units. Bit 3 drilled through clay, siltstone, and sand to 3705'. The estimated pore pressure during this interval was 8.7 pp while maintaining the mud weight between 9.7 to 9.9 ppg.

Upon reaching the interval depth of 3705', the hole was conditioned with a short trip to the shoe that experienced drag on the way out that was probably due to swelling clays. The drill string was then pumped and back reamed from a depth of 3235' to the 20" shoe. The maximum gas from this short trip was 313 units. Additional circulating time was applied to the hole in preparation for running electric logs. On this trip out, the drill string pulled tight inside the 20" casing, an indication of clay cuttings balling on the BHA.

After electric logs failed to reach bottom, another clean out run was made. The maximum trip gas reading while circulating at bottom was 214 units. After successfully completing the electric logs, rig operations were then suspended for 12 hours because of weather. Preparations were then made to open the hole.

Bit No. RR 3 was run into the hole ahead of a 17.5" hole opener. Drilling rates were very good during the hole opening process. The hole was then conditioned with a short trip in preparation for running casing. The pipe was back reamed and pumped out of hole from 1304' to the 20"

casing shoe to condition the area around the shoe. After getting back to bottom and circulating, a maximum short trip gas of 114 units was recorded. No excess drag was noted on the trip out of the hole. A string of 13³/₈" - 68 lbs/ft casing was then landed at a total depth of 3681'. This casing was cemented in place without problems.

Lithologies of this section consisted of sand, clay, and siltstone with traces of limestone, gravel, and coal. No abnormal gas readings or any indication of gas hydrates were encountered. The pore pressure estimate for this section of the hole was 8.7 ppg, a normal gradient. Hole problems for the interval were attributed to swelling clays/siltstones and bit/BHA balling.

Interval: 3705' to 8000'

Days:	6	Average WOB:	8-10 klb
Hole Size:	12.25"	Average RPM:	160
No. Bits:	2	Average GPM:	700
Rotating Hours:	45.6	Average SPP:	2625 psi
Deviation:	2.18 deg	Average ROP:	90 ft/hr
Mud Weight:	9.8-10.7 ppg	Mud Type:	PHPA

Discussion:

The Blow Out Preventers were tested prior to running in the hole with Bit No. 5. The 13 3/8" casing was tested to 3000 psi. Bit No. 5, a PDC type, was run in hole but would not drill the float collar. Bit No. 5 was pulled out of the hole and Bit No. 6, an FDT, was run into the hole in its place. This bit drilled the float collar, the shoe, and 20' of new hole to 3725'. A leak-off test was performed at this depth and yielded a value of 14.8 ppg equivalent mud weight. This value differs somewhat from a calculated value of 13.9 ppg using the Eaton Method for estimating the fracture gradient in shales.

After completing the leak-off test, Bit No. 6 was used to drill to 4584'. The bit was pulled due to slow penetration rates. The hole pulled tight and the drill string had to be back reamed and pumped out of hole from 3937' to the 13 3/8" shoe.

Connection gas readings were consistently logged below 3800'. A slightly increasing pore pressure trend noted on pressure plots. The estimated pore pressure was raised to 8.9 ppg.

Bit No. 7, a PDC type bit, was run back in the hole on the same bottom hole assembly. While drilling ahead, the maximum trip gas reading was 520 units. Drilling continued with this bit to 6658' where a short trip was made to condition the hole. The hole pulled tight on the way out and was back reamed to shoe recording a maximum short trip gas of 365 units.

A pressure trend was estimated to develop below 4500' using information from the Condensed Resistivity Plot in conjunction with an increase in recorded connection gas readings. The estimated pore pressure was raised to 9.4 ppg by 6900'. The pore pressure estimate was steadily increased to 9.7 ppg by 7500' while the average mud weight was raised to 10.7 ppg for additional overbalance.

Bit No. 7 was used to drill to the total depth of this well to 8000'. The hole was circulated out prior to performing a short trip to shoe. Excess drag was noted while pulling pipe between bottom and 6120'. The hole was then circulated and conditioned in preparation for running

electric logs and recorded a short trip gas of 525 units. No tight hole problems were experienced while pulling out of hole for logs. Electric logging commenced on 9-29-93.

On the first logging attempt the logging tool would not penetrate beyond the casing shoe. A clean out run was made to further condition the hole. The maximum gas recorded from this trip was 181 units. Logging operations were completed on 10-4-93 and operations to plug and abandon Kuvlum No. 3 were initiated on this date.

Lithologies of this section consisted of clay, thin bedded sands, hydrated shale, and siltstone. Minor shows of oil fluorescence were logged in siltstones below 6000'. Hole problems for the interval were minor and largely due to tight hole conditions experienced on trips caused by swelling clays and siltstones.

CONCLUSIONS AND RECOMMENDATIONS

5

The drilling program for OCS-Y-0865 No. 1 - Kuvlum No. 2 was designed to penetrate to an estimated depth of 9500' and to evaluate the possible extension of the field discovered on Kuvlum No. 1 during the previous drilling season. After drilling through the targeted area, the decision was made to deepen this well for additional data. Kuvlum No. 2 was successfully drilled to a total depth of 11125' on 8-20-93 requiring 24 operating days after spudding in the well.

The drilling program for OCS-Y-0866 No. 2 - Kuvlum No. 3 was designed to penetrate to an estimated depth of 8000' and to evaluate the same potential zones discovered on Kuvlum No. 1 during the previous drilling season. Kuvlum No. 3 was successfully drilled to a total depth of 8000' on 9-28-93 requiring 20 operating days after spudding in the well.

Minor hole problems were experienced in the upper intervals of both wells in handling the nature and volume of cuttings at the shale shakers of which resulted in some additional mud losses when the shakers were overloaded. Minor fluid losses to the hole were also noted while logging and running casing.

In the bottom intervals of the Kuvlum No. 2 & No. 3, notable amounts of drag were experienced on trips causing swabbing conditions that lead to improper pipe displacement fill. The probable causes for this condition were swelling clays and some buildup of cuttings adhering to the bore hole. Short trips were employed while drilling this section to clean and condition the hole but required some additional rig time; especially when conditions warranted pumping and back reaming out of the hole. We would like to recommend additions of a hole stabilizing product, Resinex, which is often effective in controlling clay swelling problems experienced in other areas on the North Slope for this interval of the well.

Pore pressure estimates were very near a normal gradient for the majority of formations logged on. On Kuvlum No. 2, a modest pore pressure gradient was estimated to develop below 7000' and extend to a depth of 10000' before formation pressure increases appeared to stabilize at an estimated value of 9.9/10.0 ppg. This trend analysis is supported through interpretation of data supplied by the D-Exponent and Condensed Resistivity Plots provided in the Parameters vs Depth section of this report. A slightly less defined gradient was estimated to occur on Kuvlum No. 3 below 4200' and extending to a depth of 7800' where the pore pressure was estimated to reach a value of 9.6/9.7 ppg. No significant hole problems were experienced because of the gradients as the mud weight maintained throughout this section on both wells provided for ample overbalance to safely drill.

On Kuvlum No. 2, shows of fluorescence were noted on the mud logs in sands logged below 6000'. Five show evaluation reports were made while drilling this well beginning at 6470' and extending to a depth of 7115'. Analysis of the reports provide evidence of the presence of hydrocarbons over this zone of interest; however, ratio analysis of the gas readings indicate that this zone is predominantly gas bearing or possibly tight. No porosity estimates could be effectively made from the drill cutting samples as the sand came back unconsolidated. A more detailed description of the individual zones can be found in the Show Report section of this report.

On Kuvlum No. 3, shows of fluorescence were noted on the mud logs in the sand logged at 3785' and the siltstones below 7000'. Porosity estimates for the sand were poor and ranged from 0% - 5%. There were no heavy hydrocarbons (C2-C5) associated with the sand interval although consistent readings of C2-C5 were logged below 4900'. No show reports were completed for this interval on this well.

The following hydraulics and mud property recommendations are based on the drilling program used on Kuvlum No. 2 and No. 3. The recommendations are made using a similar casing design and differ very little from the mud weights observed on each well.

RECOMMENDED MUD PROPERTIES

Depth	Csg Seat	Mud Weight	Yield Point	Water Loss
0-1000	20"	Sea Water	Sweeps	N/A
-3900	13 ³ / ₈ "	9.6	20-30	<10
-7000	8 ¹ / ₂ " Hole	9.8	20-30	< 6
-TD	8 ¹ / ₂ " Hole	10.0/10.7	20-30	< 5

RECOMMENDED HYDRAULICS

Hole Size:	26"	17.5"	12.25"	12.25"
Depth:	800	2500	6000	9000
Gallons Per Min:	1100	925	650	650
Nozzles:	4-20's	4-16's	4-12's	4-14's
Pump Pressure:	2200	3000	3000	3000

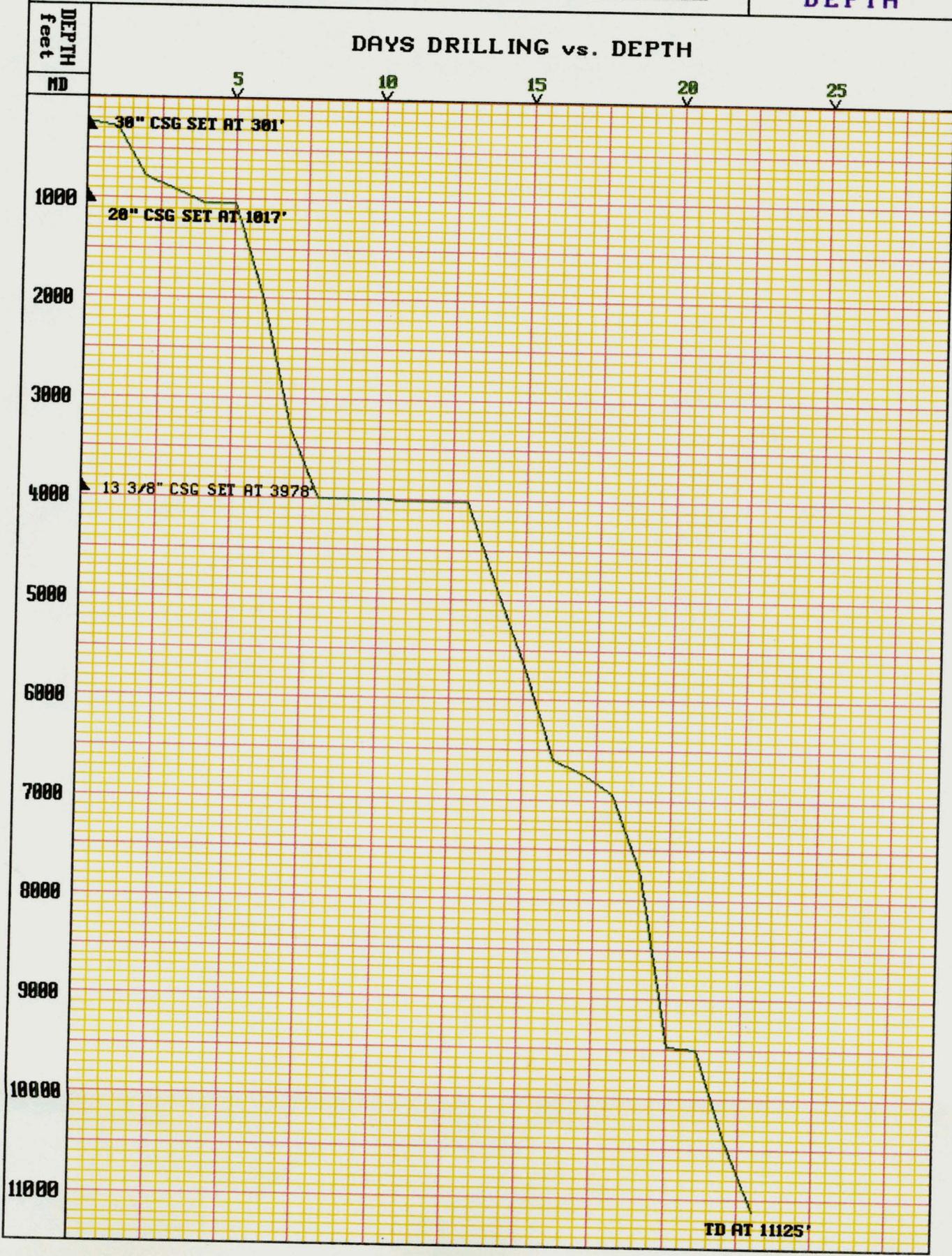
SPERRY SUN DRILLING SERVICES
A BAROID COMPANY

SPERRY SUN
LOGGING
SYSTEMS

WELL OCS-Y-0866 NO. 1
COMPANY ARCO ALASKA, INC.
LOCATION BLOCK 672 BEAUFORT SEA, AK.

DAYS
VS
DEPTH

6

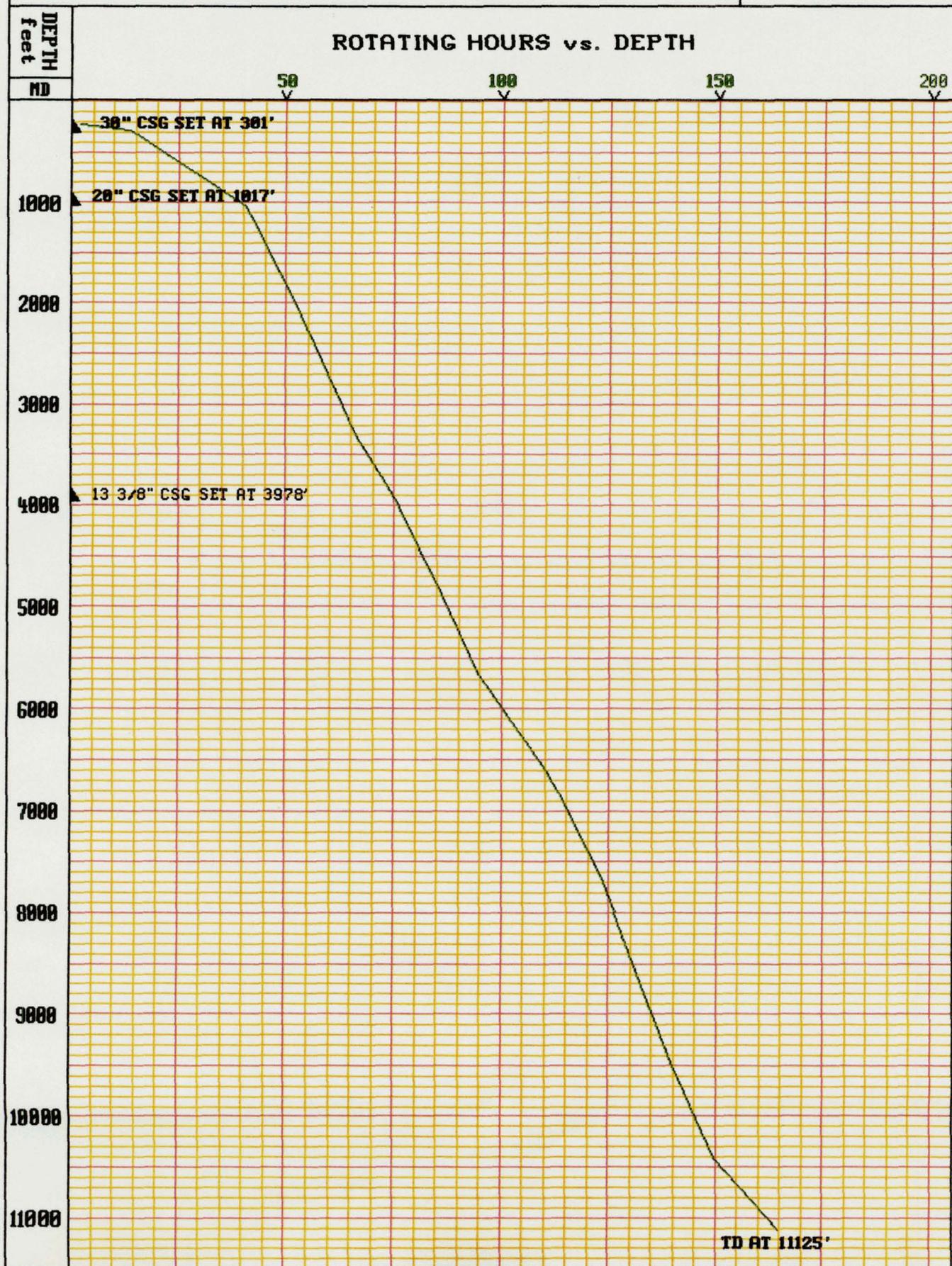


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**SPERRY SUN
LOGGING
SYSTEMS**

WELL DCS-Y-0865 NO. 1
COMPANY ARCO ALASKA INC.
LOCATION BLOCK 672 BEAUFORT SEA, AK.

**ROTATING HRS
VS
DEPTH**



SPERRY-SUN DRILLING SERVICES

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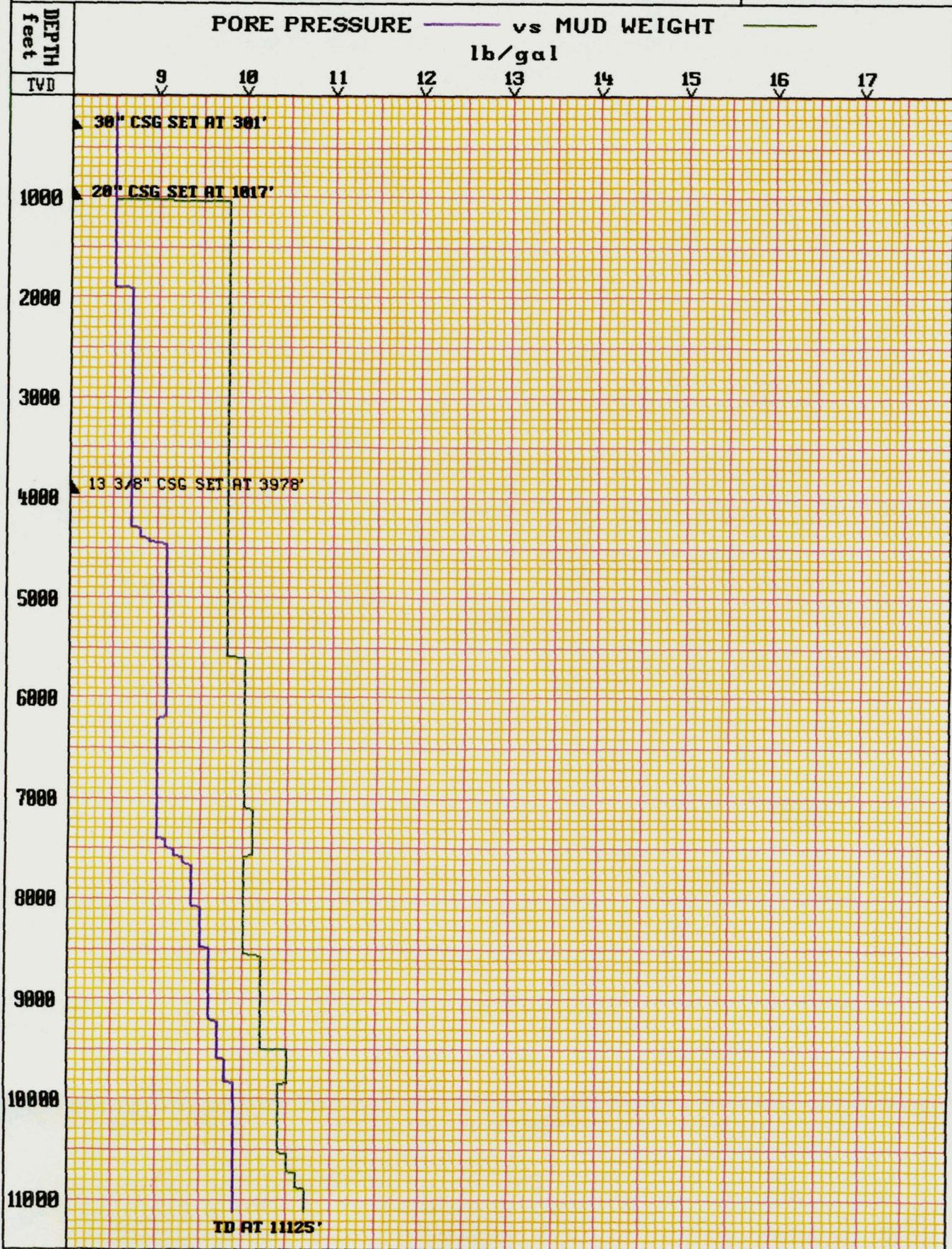
**SPERRY SUN
LOGGING
SYSTEMS**

WELL OCS-Y-0865 NO. 1

COMPANY ARCO ALASKA, INC.

LOCATION BLOCK 672 BEAUFORT SEA, AK.

**PORE
PRESSURE vs
MUD WEIGHT**

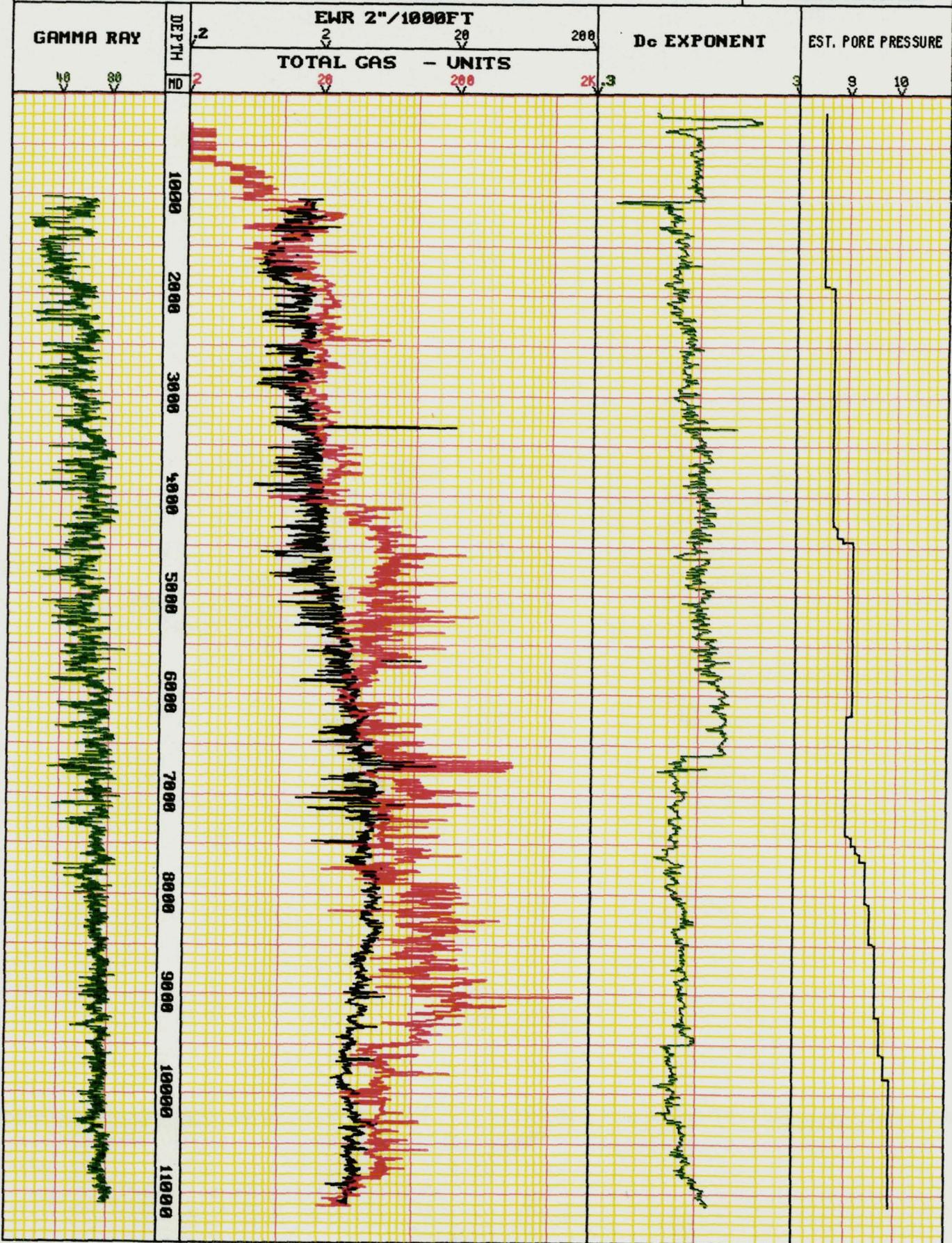


**SPERRY-SUN DRILLING SERVICES
LOGGING SYSTEMS**

WELL OCS-Y-0865 NO. 1 KUVLUM # 2
 COMPANY ARCO ALASKA, INC.
 LOCATION NR6-4 BLK 672, BEAUFORT SEA, AK.

**BAROID
LOGGING
SYSTEMS**

**PRESSURE
PARAMETERS**

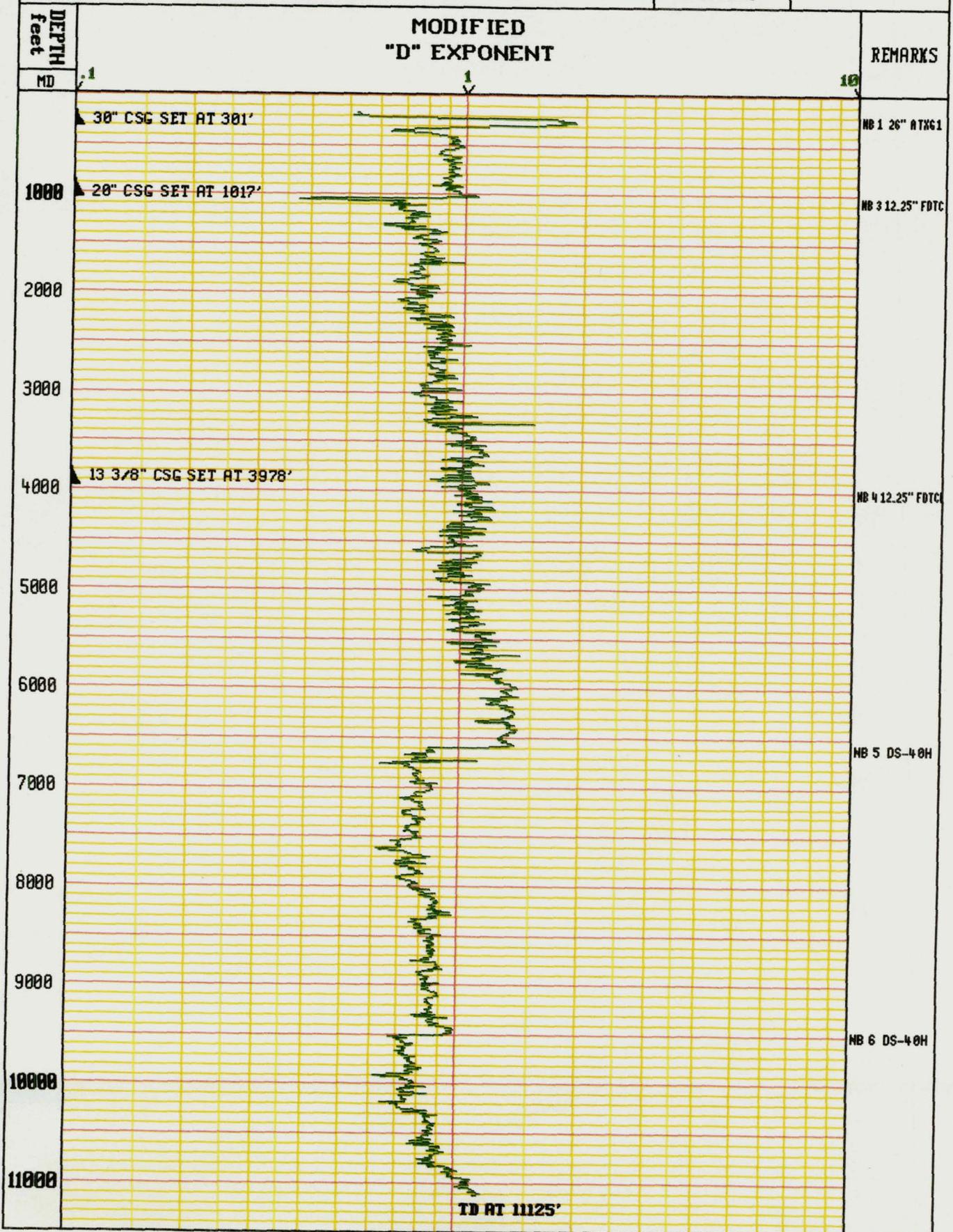


**SPERRY-SUN LOGGING SYSTEMS
ALASKA DISTRICT**

WELL OCS-Y-0865 NO. 1
 COMPANY ARCO ALASKA INC.
 LOCATION BLOCK 672 BEAUFORT SEA, AK.

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SPERRY SUN
LOGGING
SYSTEMS

WELL DCS-Y-0866-2 KUVLUM NO. 3

COMPANY ARCO ALASKA, INC.

LOCATION NR6-4 BLK 673, BEAUFORT SEA, AK.

DAYS
VS
DEPTH



SPERRY SUN DRILLING SERVICES
A BAROID COMPANY

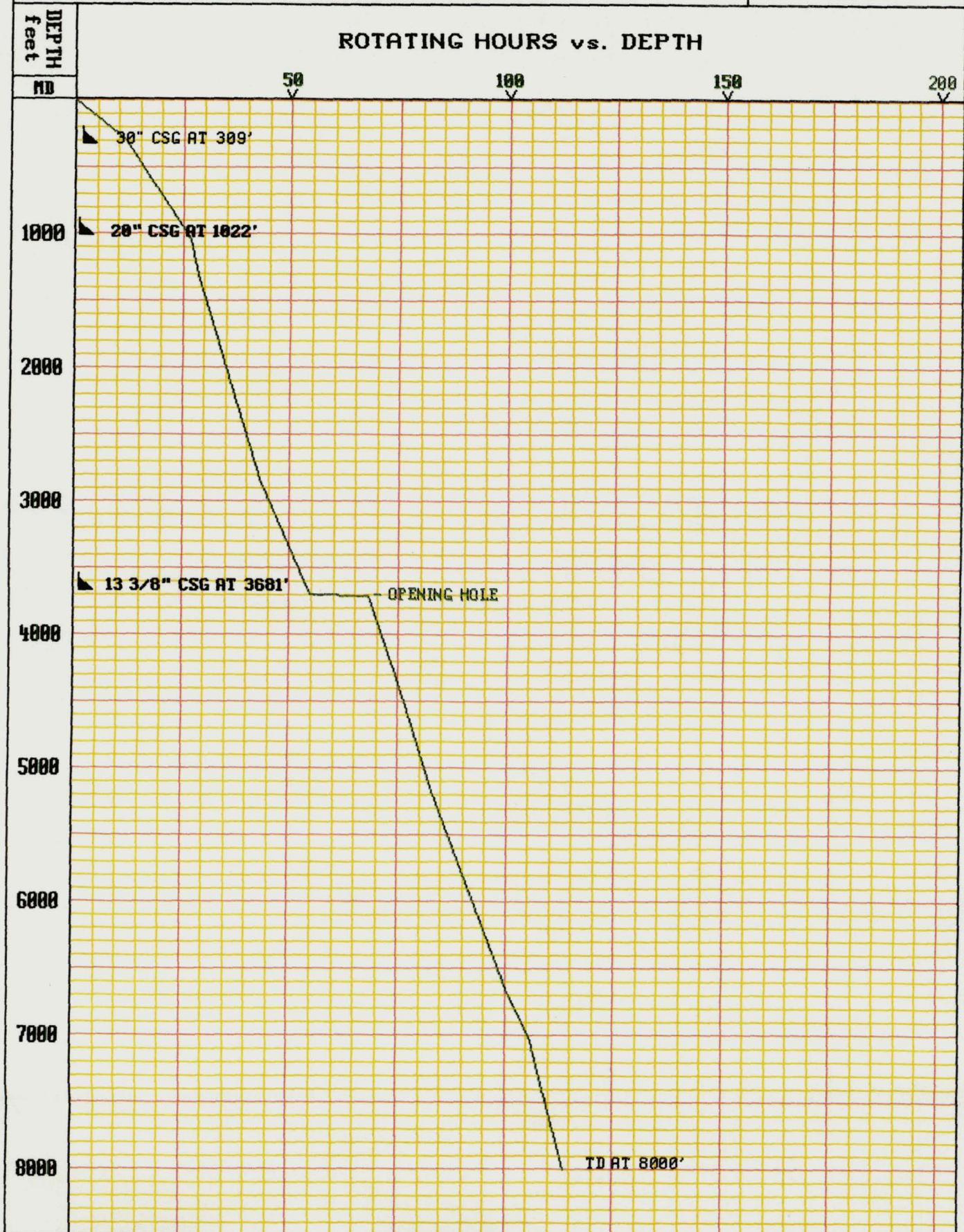
SPERRY SUN
LOGGING
SYSTEMS

WELL OCS-Y-0866-2 KUVLUM NO. 3

COMPANY ARCO ALASKA INC.

LOCATION NR6-4 BLK 673, BEAUFORT SEA, AK.

ROTATING HRS
VS
DEPTH

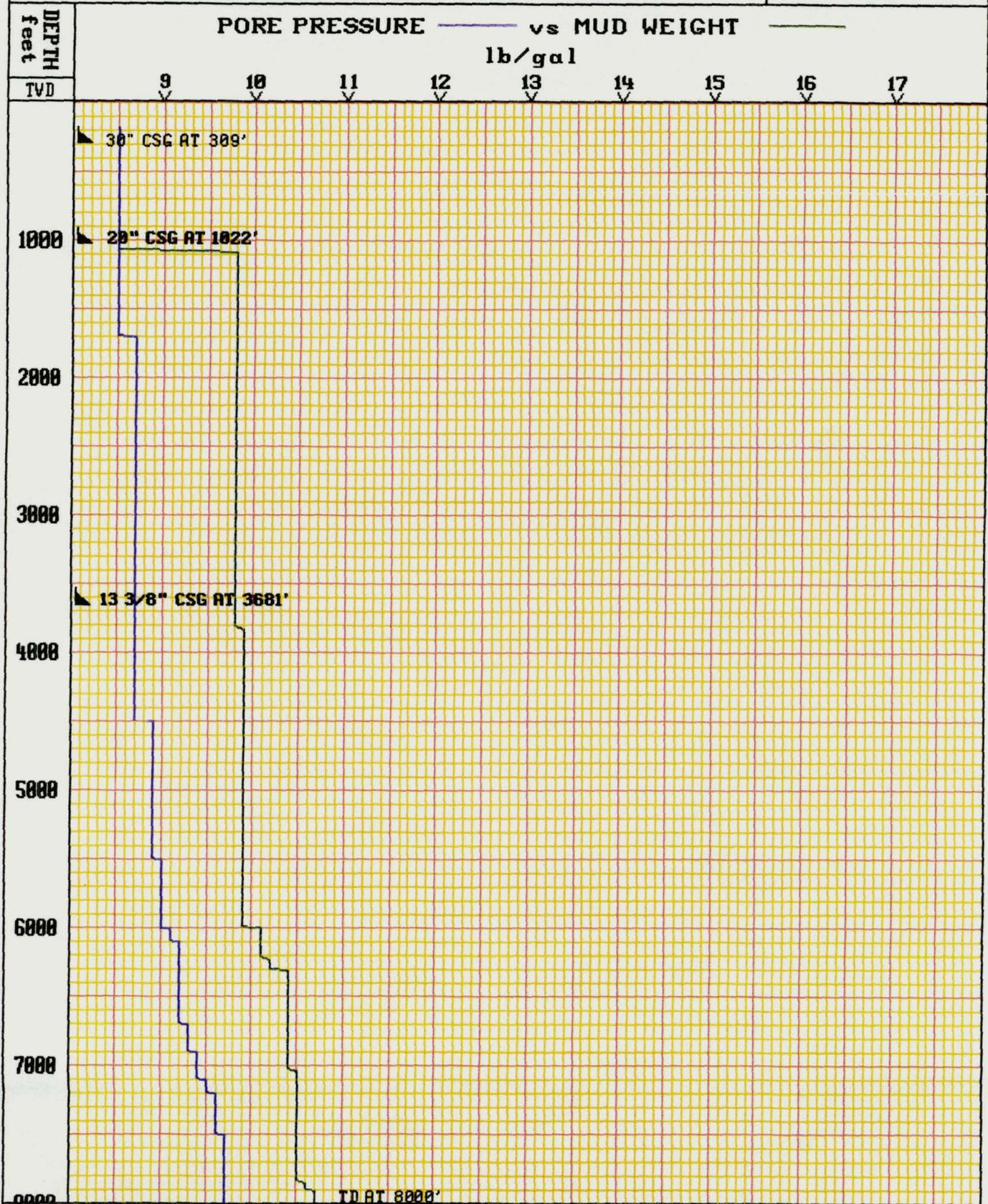


SPERRY-SUN DRILLING SERVICES
ALASKA DIVISION

LOGGING
SYSTEMS

WELL OCS-Y-0866-2 KUVLUM NO. 3
COMPANY ARCO ALASKA, INC.
LOCATION NR6-4 BLK 673, BEAUFORT SEA, AK.

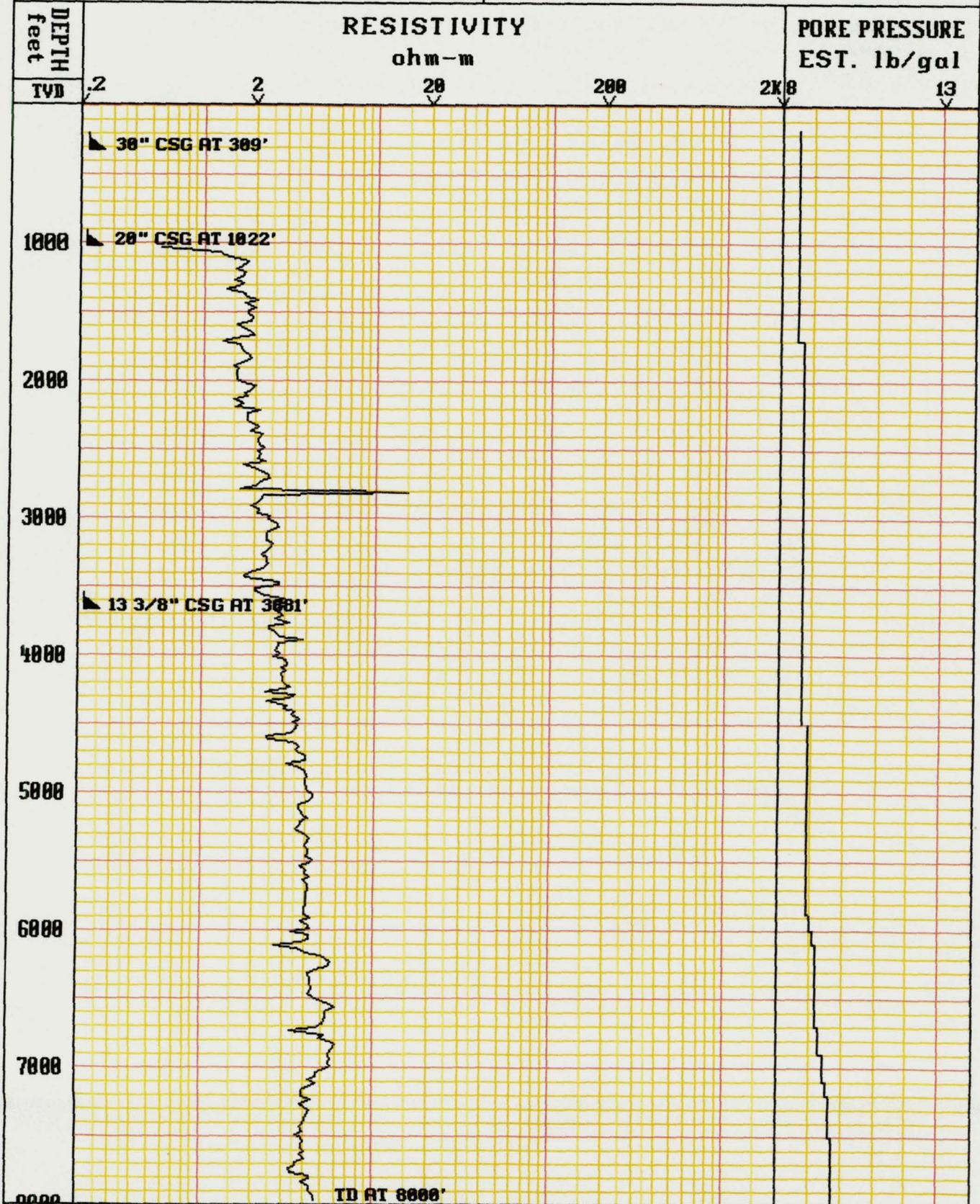
PORE
PRESSURE vs
MUD WEIGHT



SPERRY-SUN LOGGING SYSTEMS
ALASKA DISTRICT

WELL OCS-Y-0866 NO.2 KUVLUM NO. 2
COMPANY ARCO ALASKA, INC.
LOCATION NR6-4 BLK 673, BEAUFORT SEA, AK.

NB New Bit NCB New Core Bit DTG Down Time Gas
 NR No Returns CO Circulate Out OBG Off Bottom Gas
 DC Depth Corr CKF Check for Flow TG Trip Gas
 TCL Trip Chlorides LAT Log After Trip CG (Bar Graph)

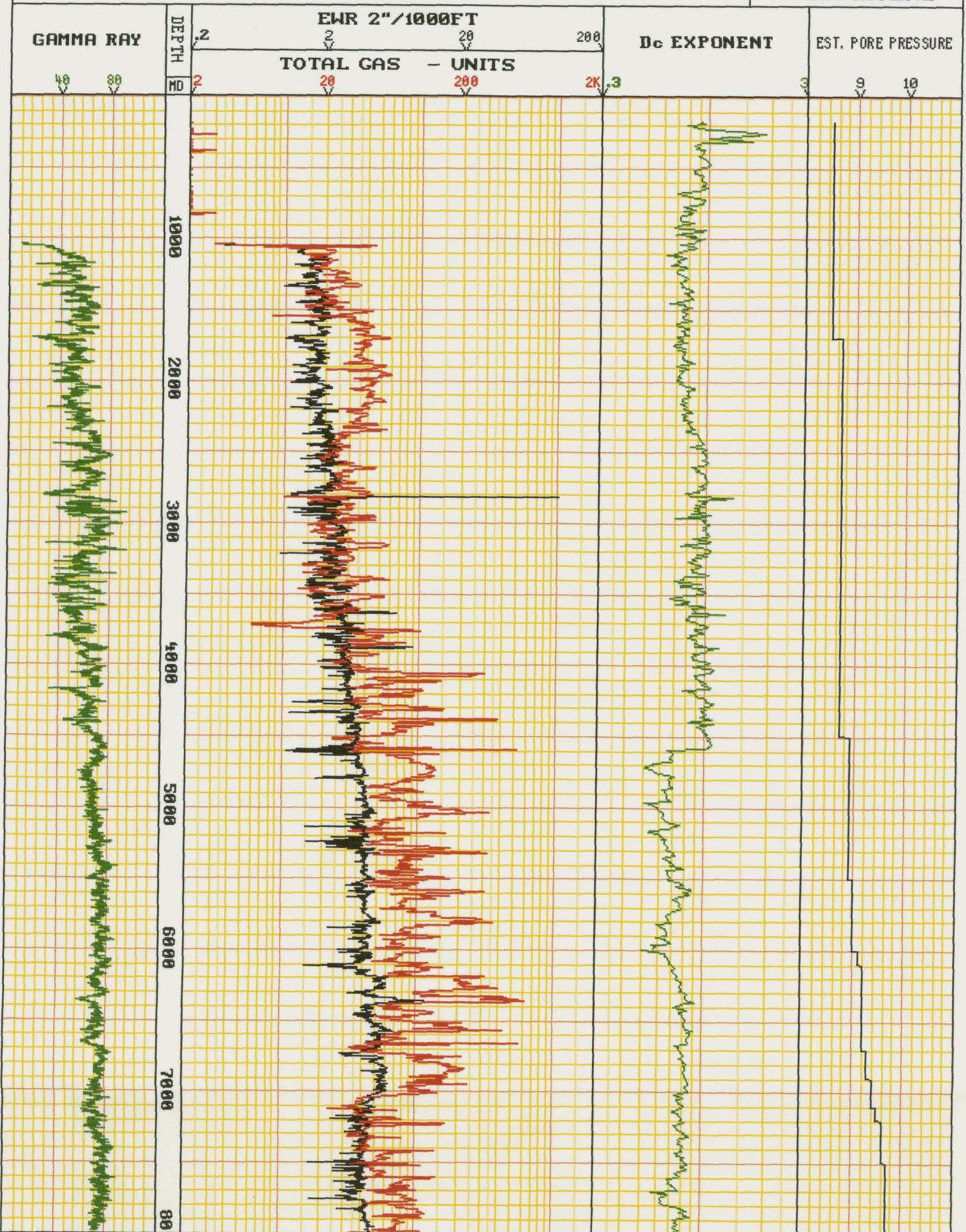


SPERRY-SUN DRILLING SERVICES LOGGING SYSTEMS

WELL OCSY-Y-0866 #2 - KUVLUM NO. 3
 COMPANY ARCO ALASKA, INC.
 LOCATION NR6-4 BLK 674, BEAUFORT SEA, AK.

**BAROID
LOGGING
SYSTEMS**

**PRESSURE
PARAMETERS**



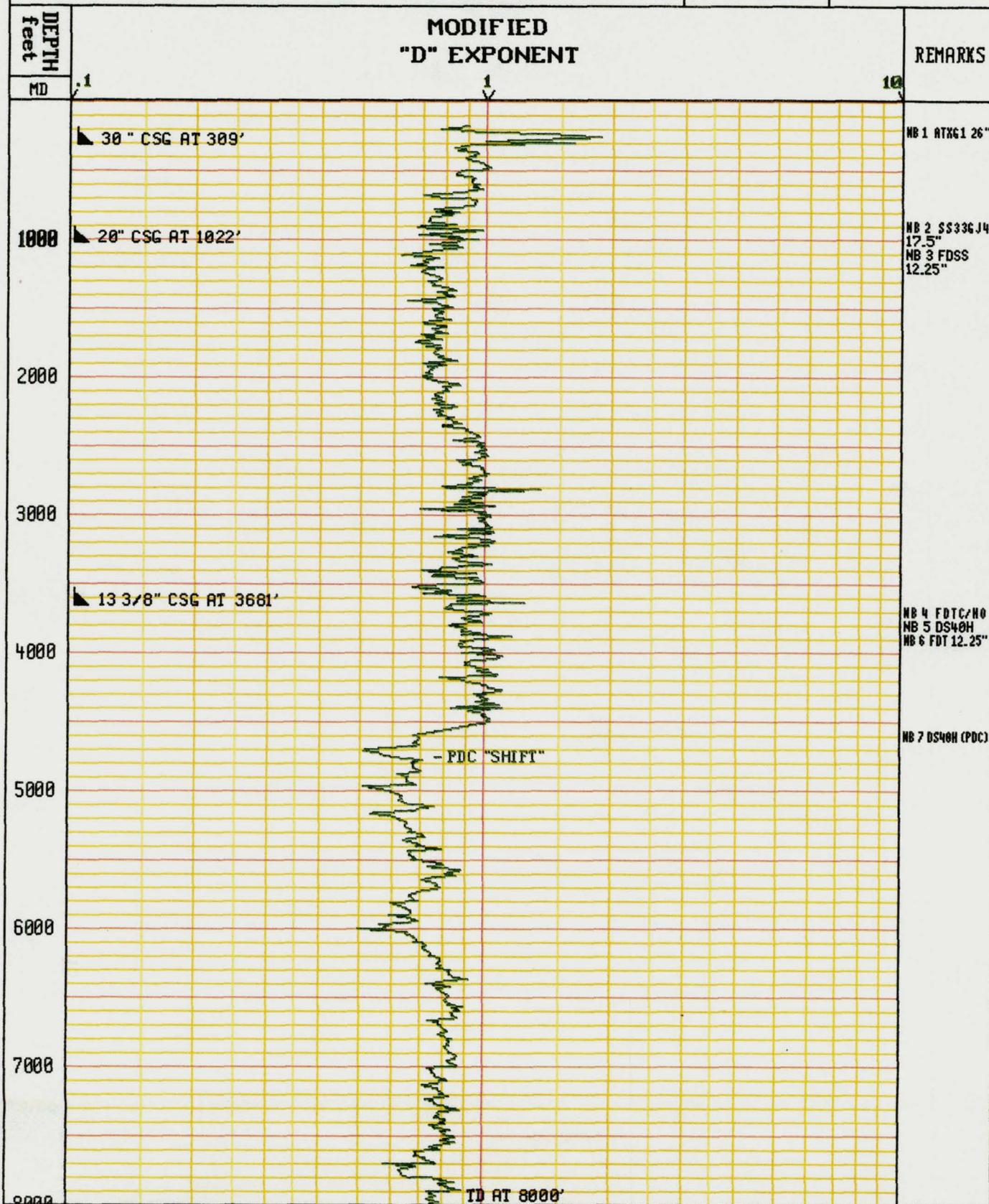
**SPERRY-SUN LOGGING SYSTEMS
ALASKA DISTRICT**

ALASKA
MODIFIED
"D"
EXPONENT

LOGGING
SYSTEMS

WELL OCS-Y-0866-2 KUVLUM NO. 3
COMPANY ARCO ALASKA, INC.
LOCATION NR6-4 BLK 673, BEAUFORT SEA, AK.

"Dc"
LOG



sperry-sun
DRILLING SERVICES
LOGGING SYSTEMS

ADT SERVICE
ENGINEERING LOG
50 feet / 1 inch

COMPANY ARGO ALASKA INC.
 WELL KUYLUM NO. 2
 FIELD BEAUFORT SEA, BLOCK 672
 REGION _____
 LOCATION ALASKA, U.S.A.
 CO-ORDS _____
 CONTRACTOR CANMAR
 RIG/TYPE CDU KULLUK
 TOTAL DEPTH 11125' TVD 11125'
 SPUD DATE 28 JULY 1993

HOLE DATA
 21 (RISER) To 171 17.5 To 3978
 30" To 301 12.25 To 11125
 26" To 1017 To _____

CASING DATA
 30" To 301 To _____
 20" To 1017 To _____
 13 3/8" To 3978 To _____

MUD TYPES
 SEA WATER To 1017
 GENERIC #2 To 11125
 _____ To _____
 _____ To _____

LITHOLOGY SYMBOLS

	Coal		Sandstone
	Tuff		Sand
	Chert		Gravel
	Limestone		Conglomerate

ABBREVIATIONS

DRILLING DATA		LOGGING DATA	
NR	New Bit	LAT	Logged After Trip
RRC	Rerun Bit	U	Gas Units
TB	Turbo Drill	BG	Background Gas
PDCB	Polycrystalline Diamond Compound Bit	TG	Trip Gas
CB	Core Bit	STG	Short Trip Gas
DB	Diamond Bit	CC	Connection Gas
WOB	Weight on Bit	OST	Drill Stem Test
RPM	Revs Per Minute	DS	Direction Survey
CO	Circuits Out	DC	Depth Correction
PR	Partial Returns	C	Carbide Test
NR	No Returns	CKF	Check for Flowline
		FLT	Flowline
		DHT	Differential Hydraulic Test
MUD DATA			
W	Mud Density	PV	Plastic Viscosity
V	Yield Point	YP	Yield Point
FL	Filtrate Loss	S	Solids Content
FC	Filtrate Cake	G	Gels
CL	Salinity	RM	Mud Resistivity
PH	Hydrogen Ion Content	RF	Filtrate Resistivity

ENGINEERING DATA

	Casing No. / Recovery		Gas Traces
	OST / Drill Stem Test No. /		Oil Traces

ELEVATION AND LOGGING DATA
 PERMANENT DATUM MEAN SEA LEVEL
 ELEVATIONS: K.B. 65'
 D.F. 61'
 G.L. / S.F. 101'
 LOG MEASURED FROM K.B.
 LOGGED DEPTHS 100 To 11125
 LOGGED DEPTHS _____ To _____
 SURV. ENGINEER JOHN PATTON UNIT 2219

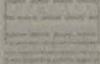
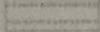
MINERALS MANAGEMENT SERVICE
ANCHORAGE, ALASKA

OCT 08 1993

RECEIVED
 OCS DISTRICT OFFICE

LOGGING ENGINEERS SAY FRENCH
JUSTIN PANTER

OTHER SERVICES: _____

 Dolomite
 Clay
 Shale
 Siltstone

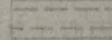
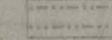
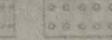
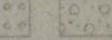
 Sidewall Core
 Interval Tester
 Wireline Log Run
 Leakoff Test
 Pressure Integrity Test
 Water
 Salt Water
 Fresh Water
 Hydrocarbon smell
 H₂S smell

SPERRY SUN DRILLING SERVICES
LOGGING SYSTEMS A Baroid Company

WELL OCS-Y-0863 NO. 1
 COMPANY ARGO ALASKA, INC.
 LOCATION BLOCK 672 BEAUFORT SEA, ALASKA

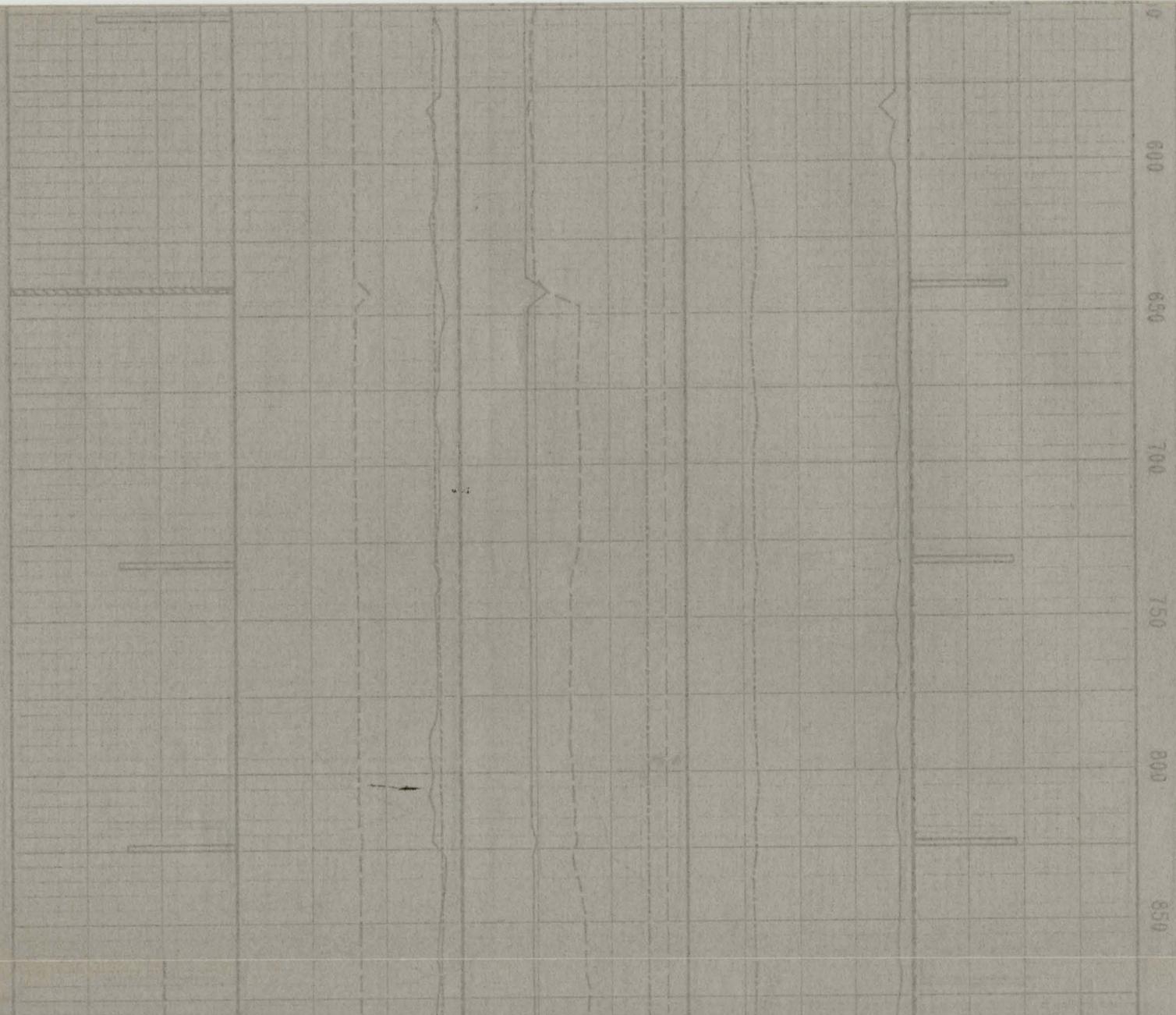
LEGEND

NB New Bit	NCB New Core Bit	CKF Check for Flow
NR No Returns	CO Circulate Out	LAT Log after Trip
IG Trip Gas	CG Connection Gas	OST Drill Stem Test
DC Depth Corr	STG Short Trip Gas	SVY Direct Survey

Clay	Shale	Siltstone	Sandstone	Gravel
				

LOGGING SYSTEMS
ADT SERVICE
ENGINEERING LOG

CONN TIME (sec) (bar graph)	WOB (KLBS)	FLOW IN (GPM)	ROP (FT/HR)	CONN LENGTH (bar graph)	DEPTH-feet	LITHOLOGY	REMARKS
TEMP OUT	RPM	STND PIPE PRES	GAMMA (AAPI)	MAX GAS UNITS			
DRAG	TORQUE (AMPS)	MUD WT IN (PPG)	"Dc" EXPONENT	EWR			
	TORQ DEV.	EST PP (PPG)	SHALE DENS				
					200		PERMANENT DATUM MEASURED FROM HSL: KB: 63' DF: 64' MEAN SEA LEVEL: 101' MD LINE: 166' BELOW KB LOGS MEASURED FROM KB SPUD IN 7-28-93 DRILLING GLORY HOLE JETTING IN 30" CONDUCTOR NO RETURNS 7-28-93 21-21-21-22 JETS IN DEPTH @ 228'
					250		



3 STD WIPER TRIP

7-30-83



900
950
1000
1050
1100
1150

20" CSG

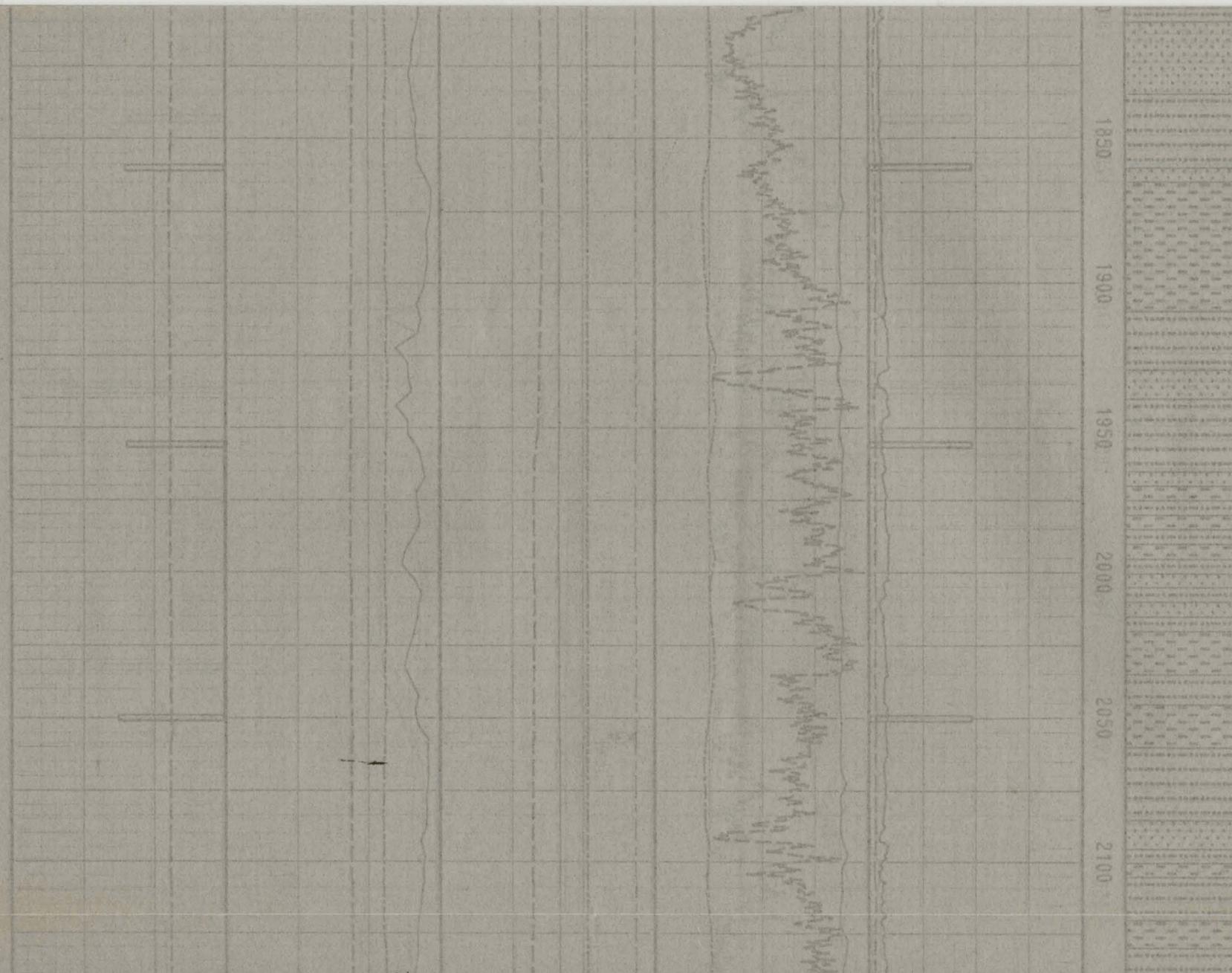
DRILLED TO 1030'
 RUN 20" OD 18.75" ID
 133 LB/FT CSG @ 118'
 LOT-12.9 pps EMW
 7-30/8-2-83
 NB 2 17.5" SS33SGJ4
 18-19-18-11 JETS
 IN DEPTH @ 1030'
 NB 3 12.25" FDTC
 14-14-14-10
 IN DEPTH @ 1040'
 MW 9.8 VIS 50
 PV/YF 19/26
 FL 4.8 PH 8.9 CL 17000

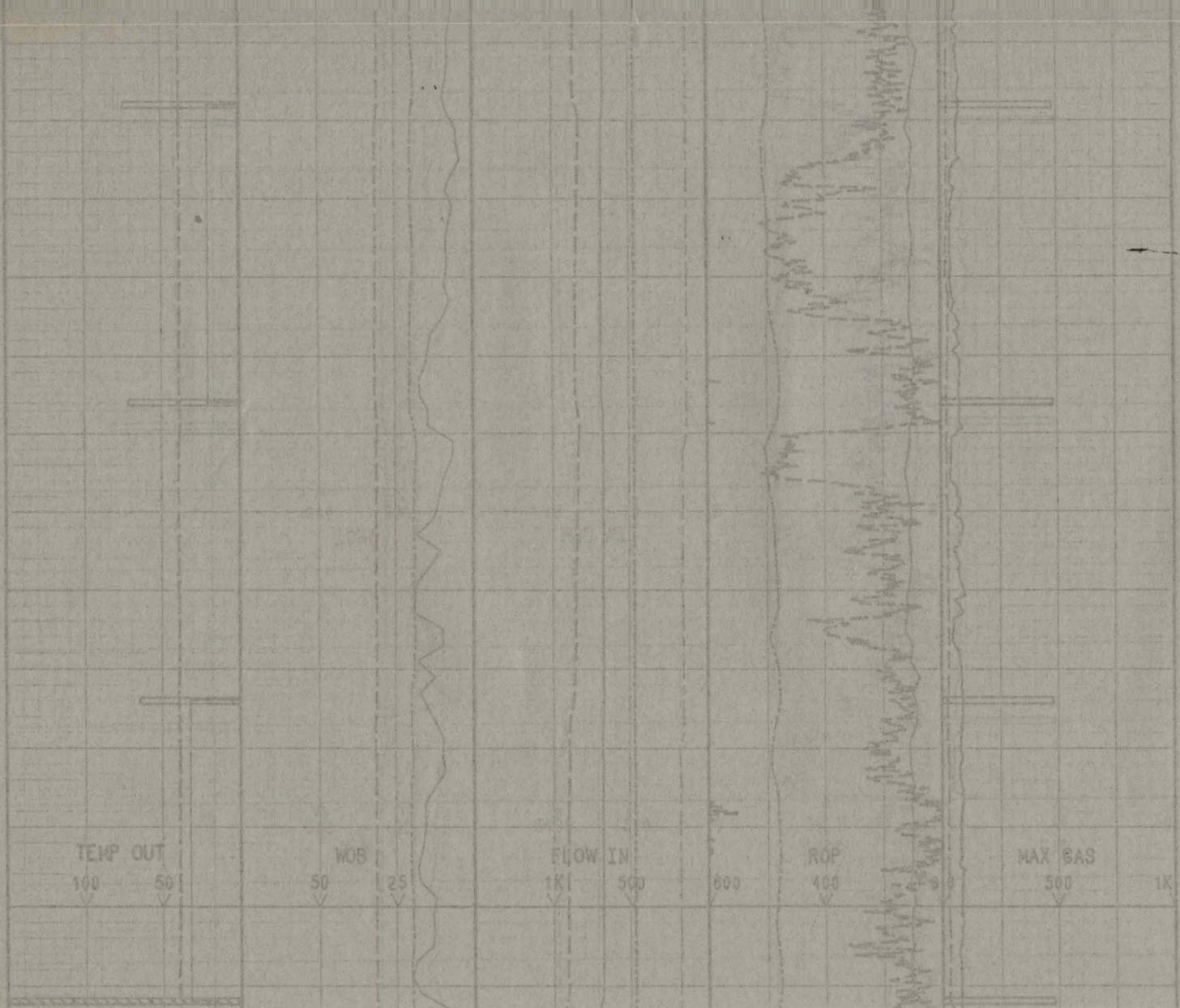
SVY @ 1852' 0.25 Deg.

1850
1900
1950
2000
2050
2100

8-3-83

MW 8.8 VIS 50
PV/YP 24/21
FL 4.6 PH 9.8 CL 16000





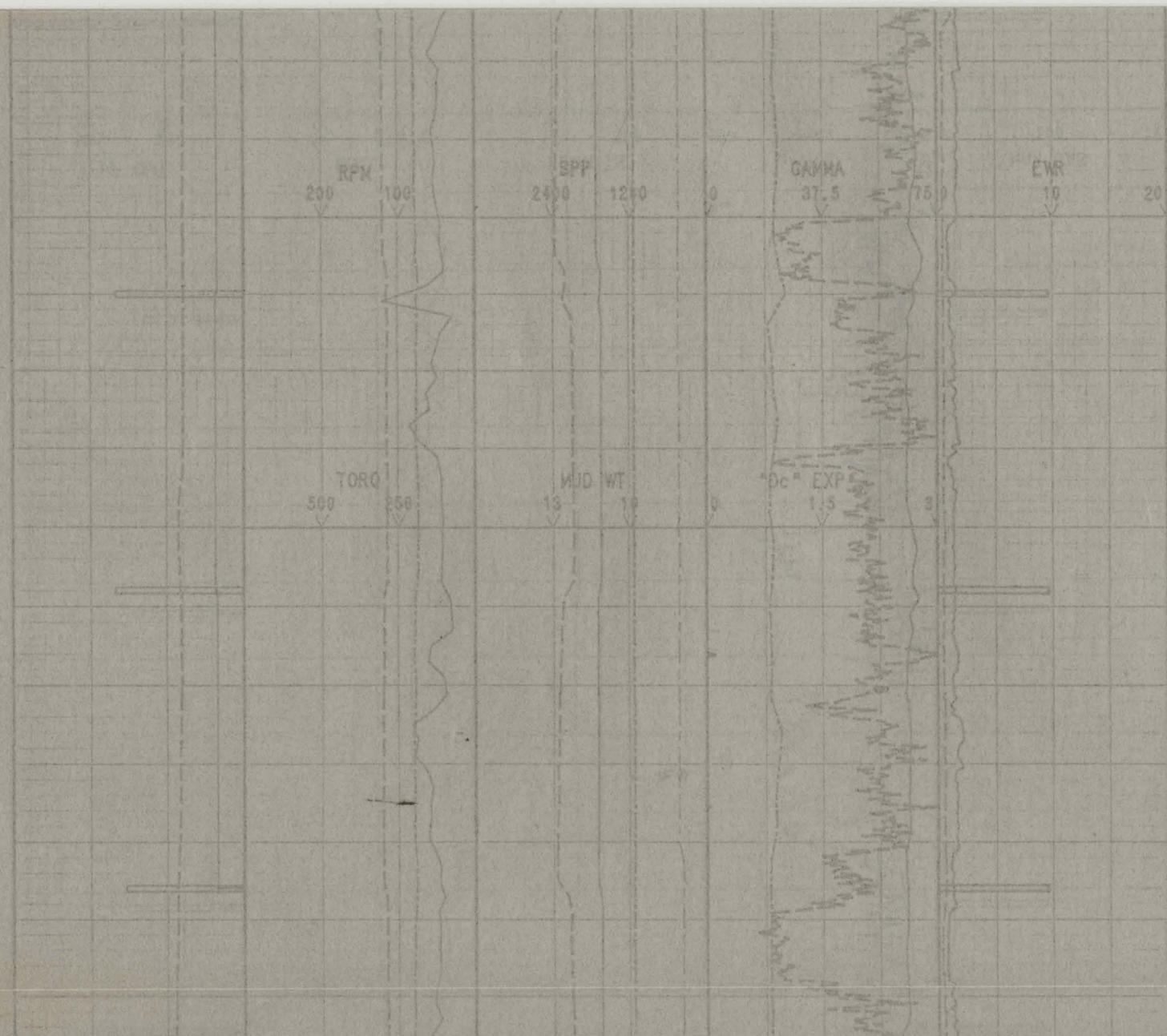
2150
2200
2250
2300
2350
2400



SVY @ 2210' 0.24 Deg.

W 1195 - 1130 140

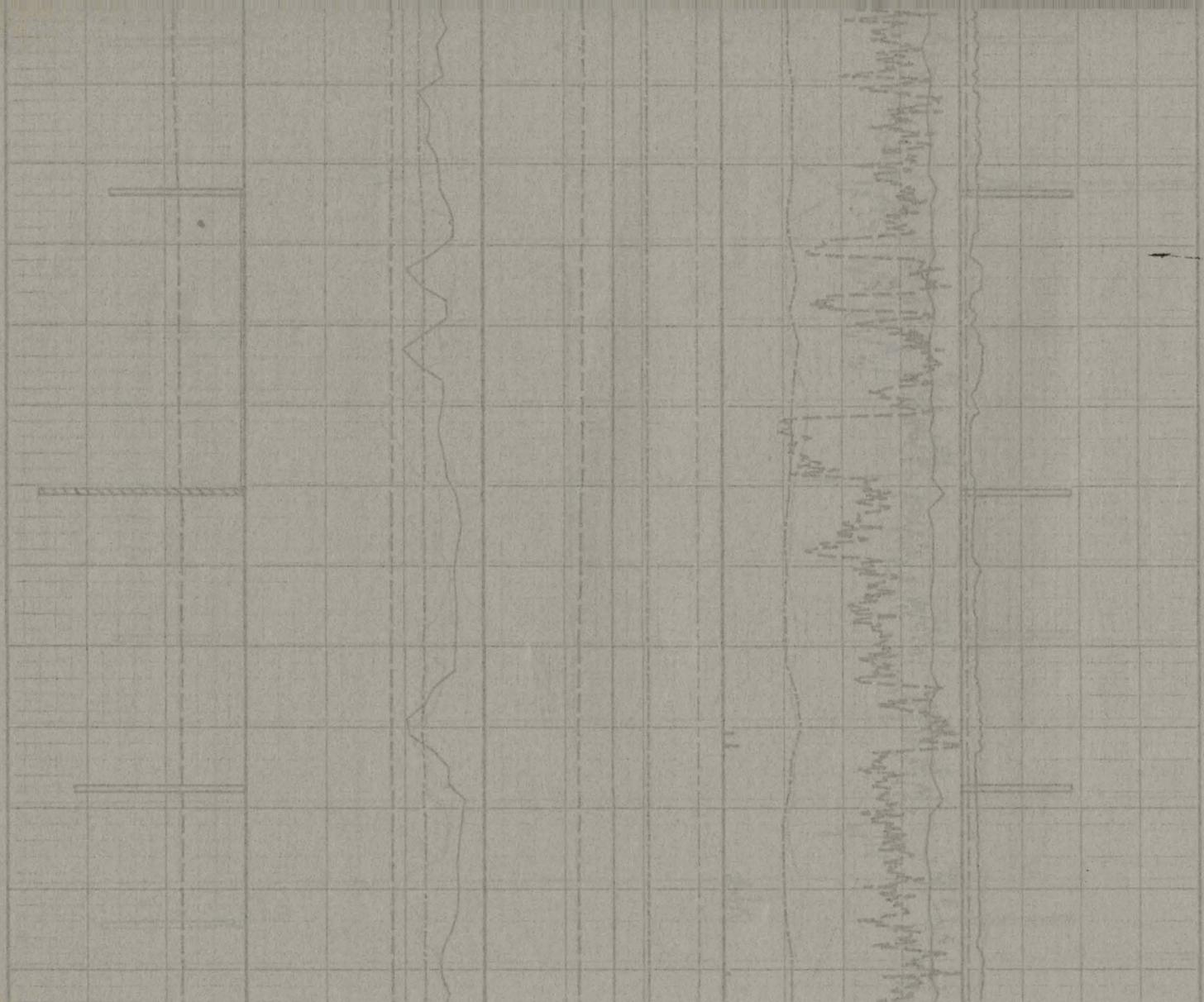
1195
1130



ST # 2435
STG 810

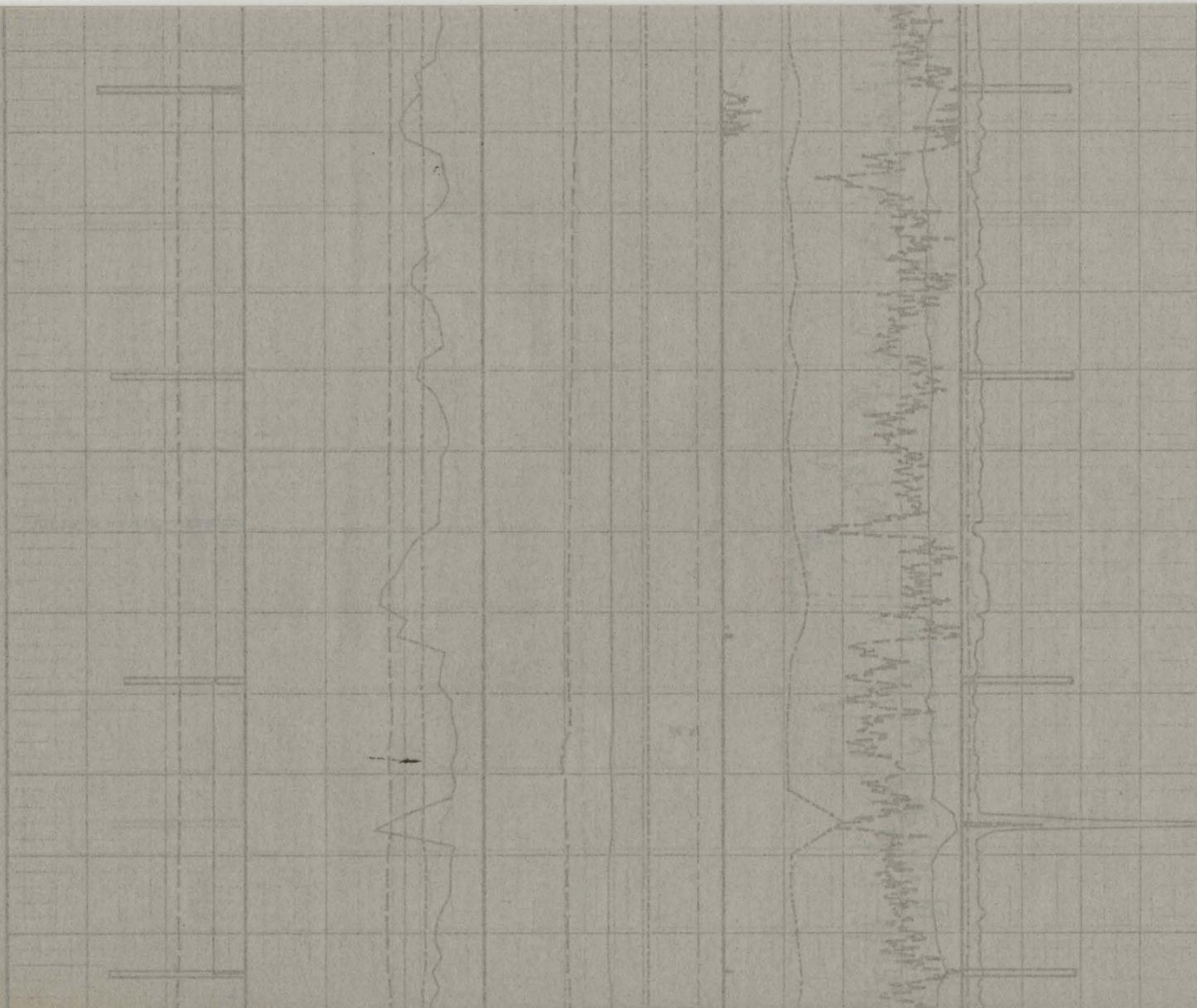
SVY @ 2495' 0.23 Deg.

W 52.0' N 14.0° E



50
100
200
300
400
500
600
700
800
900
1000
1100
1200
1300
1400
1500
1600
1700
1800
1900
2000
2100
2200
2300
2400
2500
2600
2700
2800
2900
3000
3100
3200
3300
3400
3500

SY 2883' 0.37 Deg.



Ally

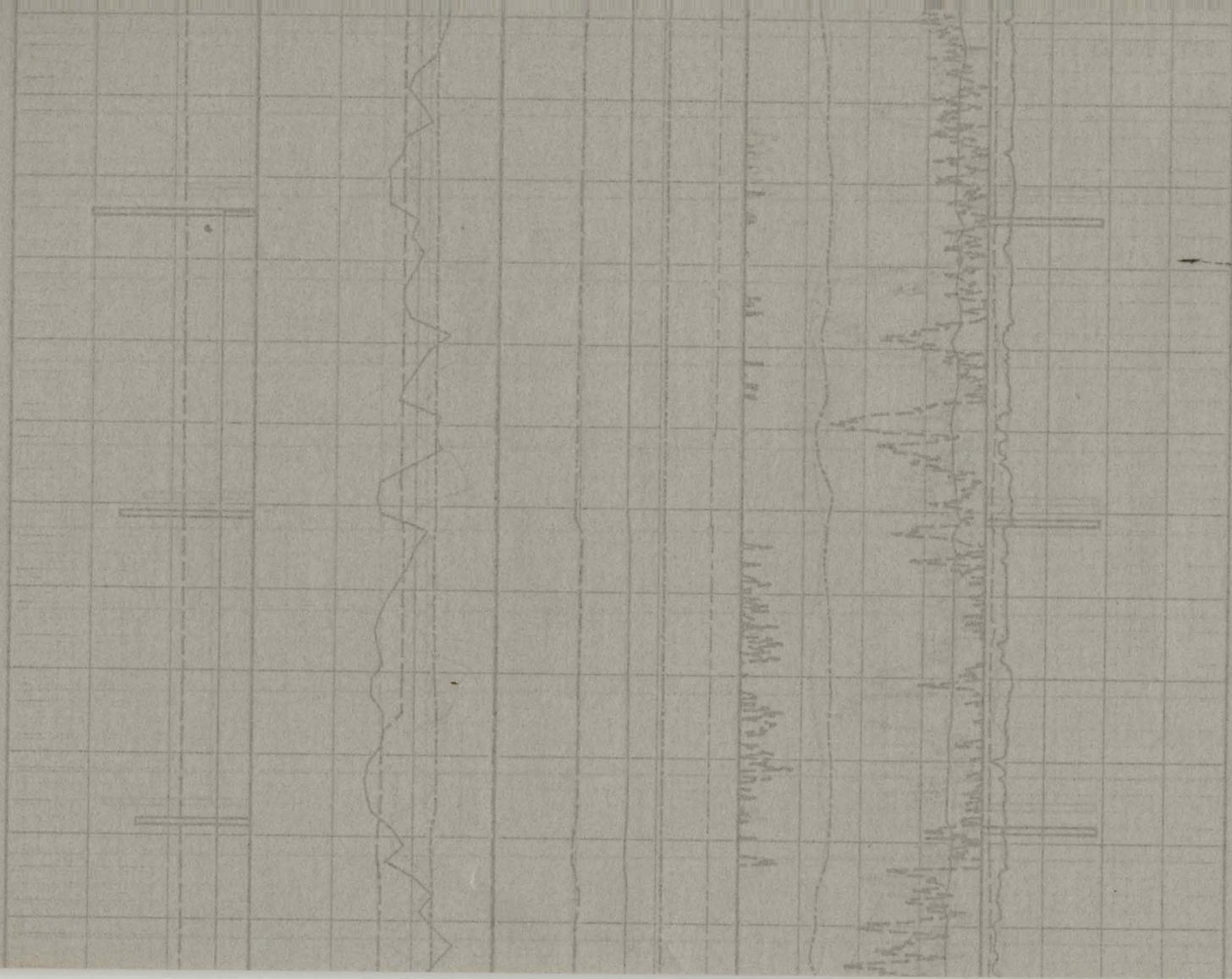
3100
3150
3200
3250
3300
3350



8-4-83

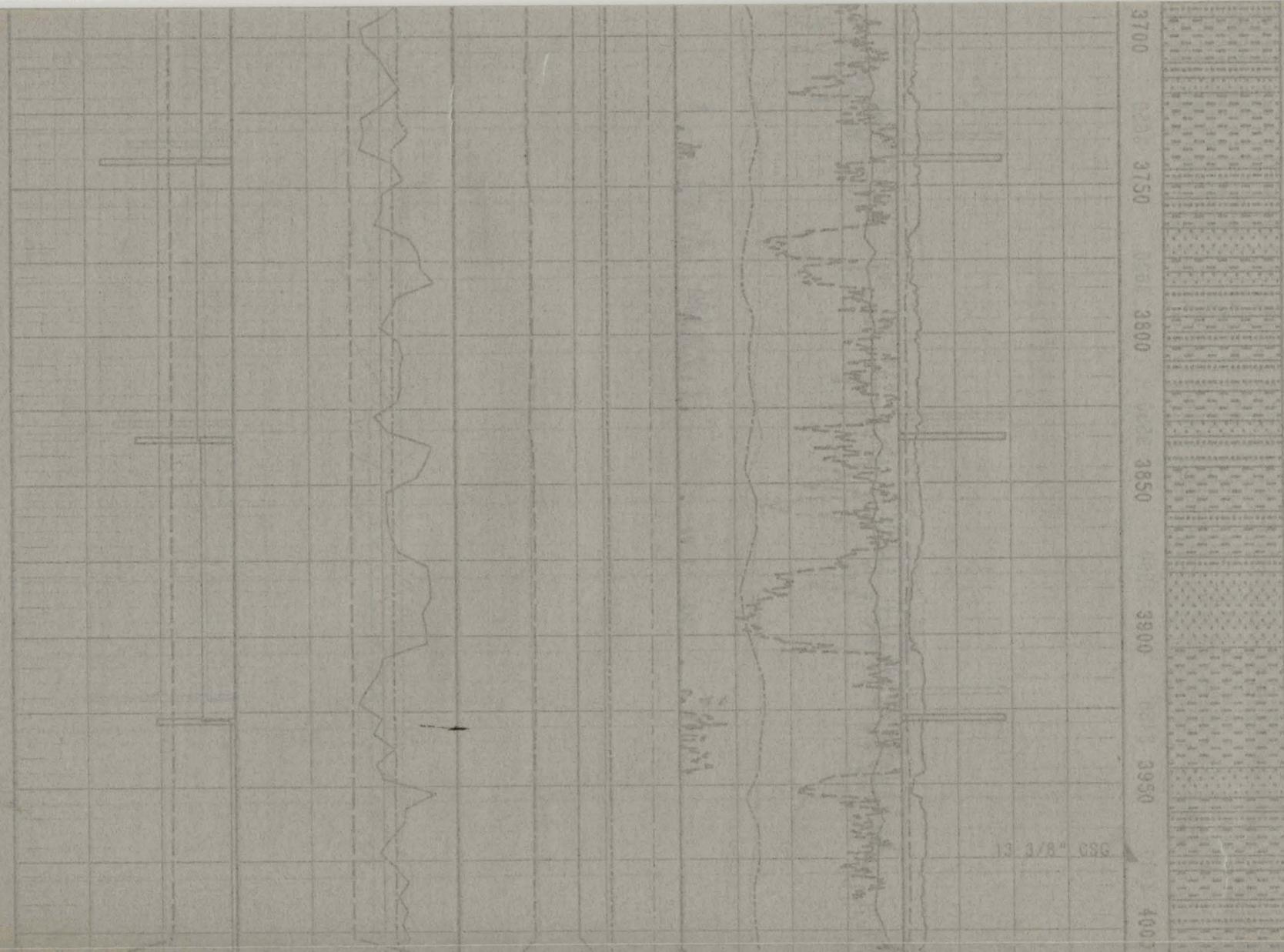
8-4-83

SVY @ 3334' 0.40 Deg.
MW 9.8 VIS 54
PV/YP 27/23
FL 4.0 PH 9.5 CL 16000



400
3450
3500
3550
3600
3650

SVY @ 3614' 0.39 Deg.



SVY # 3977 0.25 Deg

3 3/8" CGG

SVY # 3977 0.25 Deg.

STG 87u
8-5/10-83

STG 13 3/8" CGG

STG 87u
2-5/10-83
SEC 13 3/8" GSI-60071
LOT = 14.9 ppd EMW
NB 4 12.25" FDTCL
12-12-12-12 JETS
IN DEPTH 4005'

MW 9.6 VIS 51
PV/YP 15/17
FL 3.0 PH 9.2 CL 16K

SVY @ 4277'. 37Deg.

4000
4050
4100
4150
4200
4250
4300

200

MW 9.6

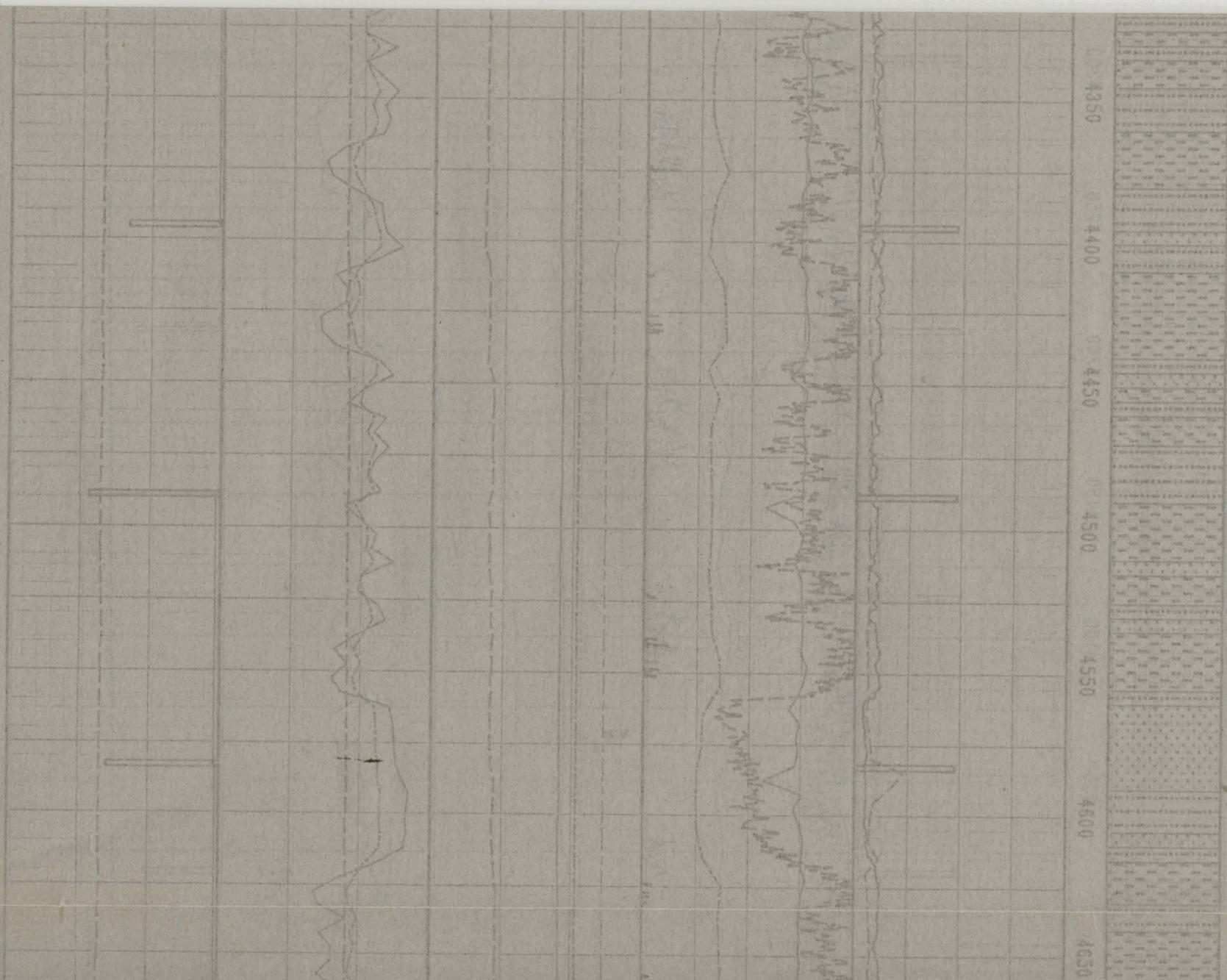
MW 9.6

100

100

100

100



00 4350

05 4400

10 4450

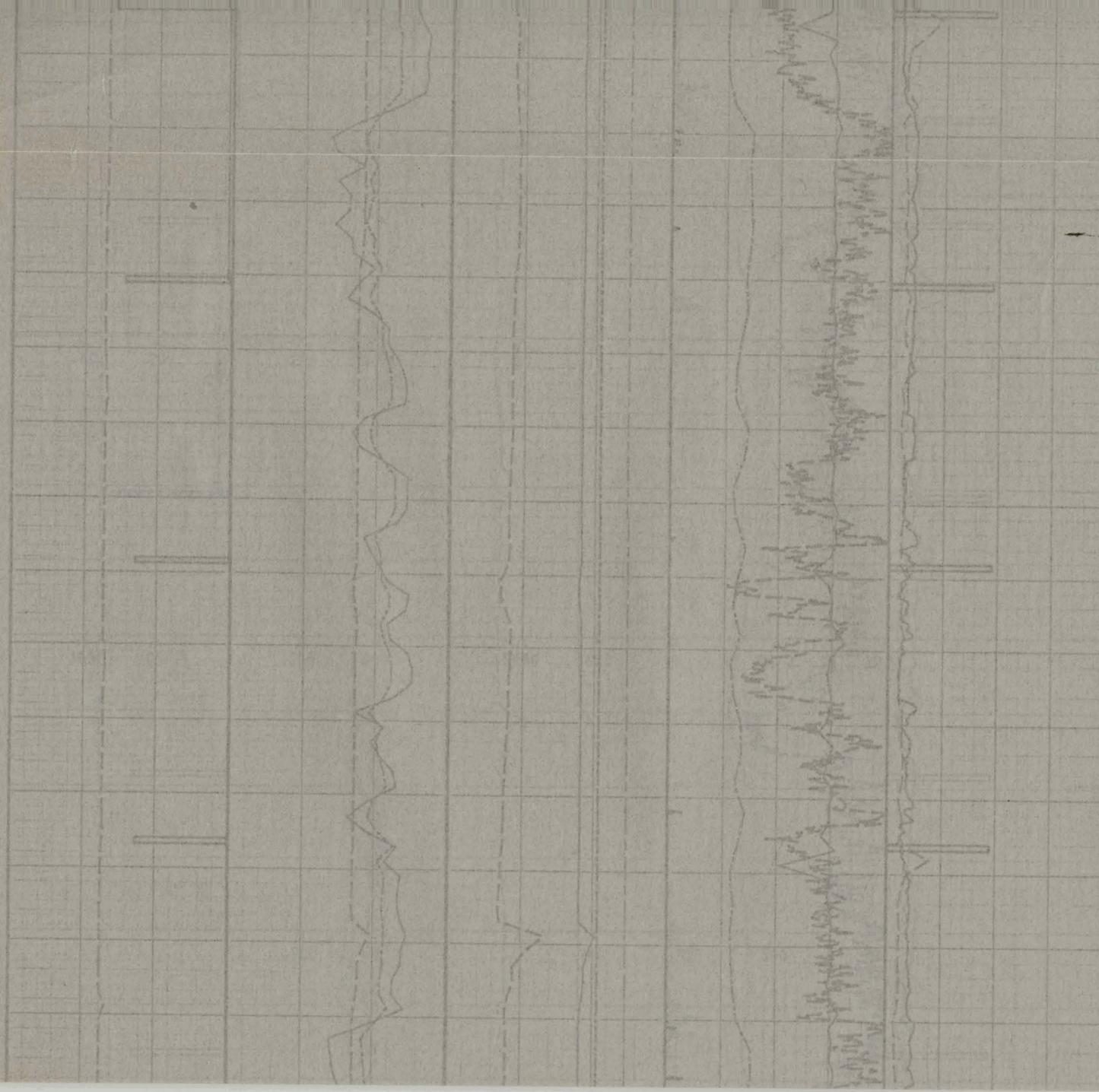
15 4500

20 4550

25 4600

30 4650

SVY @ 452' . 47Deg.



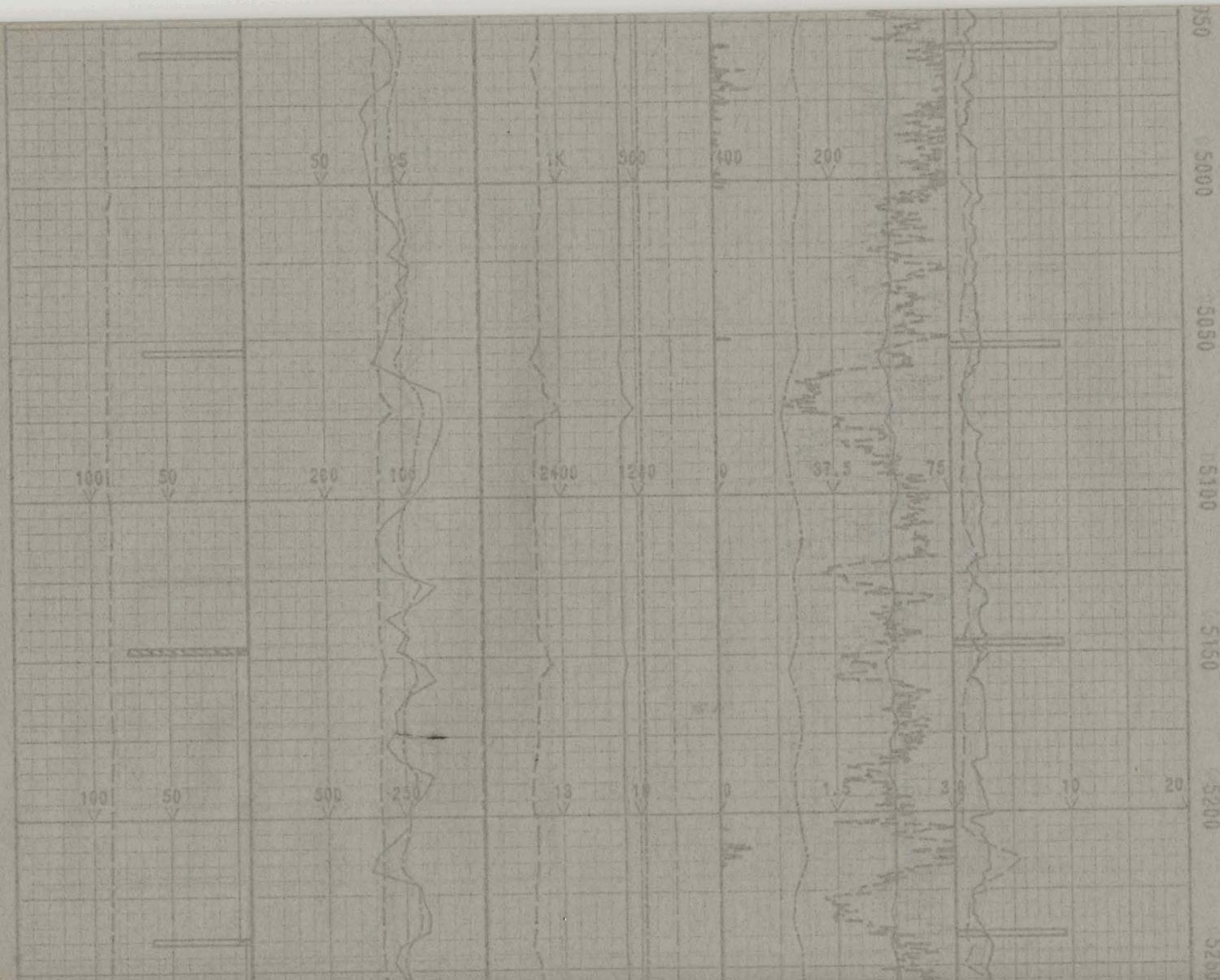
4600
4650
4700
4750
4800
4850
4900



SVY @ 4835' .39Deg.

8-11-93

SV 9 21 VTR 58



PV/YP 19/19
FL 3.2 PH 9.9 CL 17K

SVY @ 5020' .41Deg.

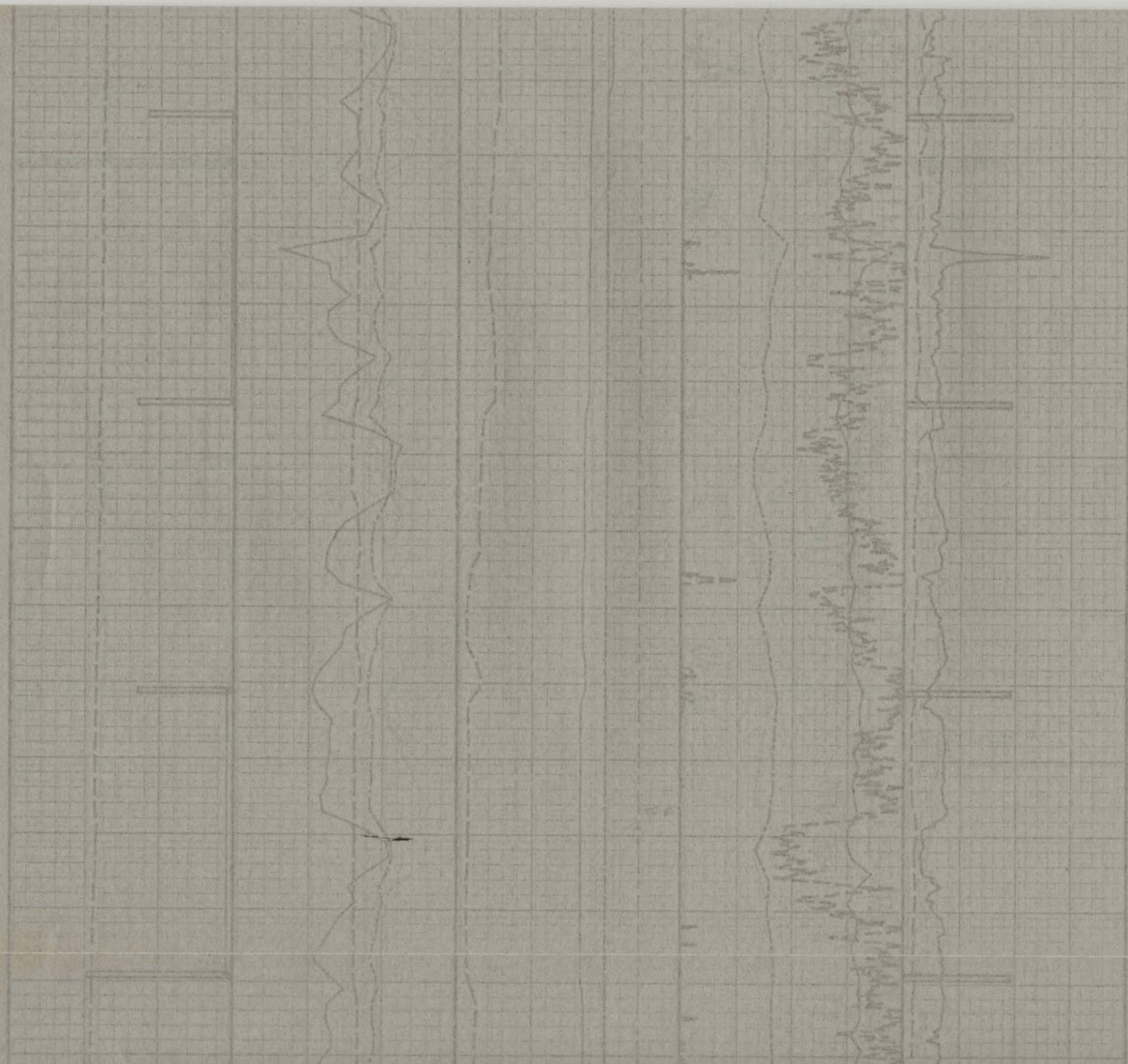
350
5000
5050
5100
5150
5200
5250



5250
5300
5350
5400
5450
5500
5550

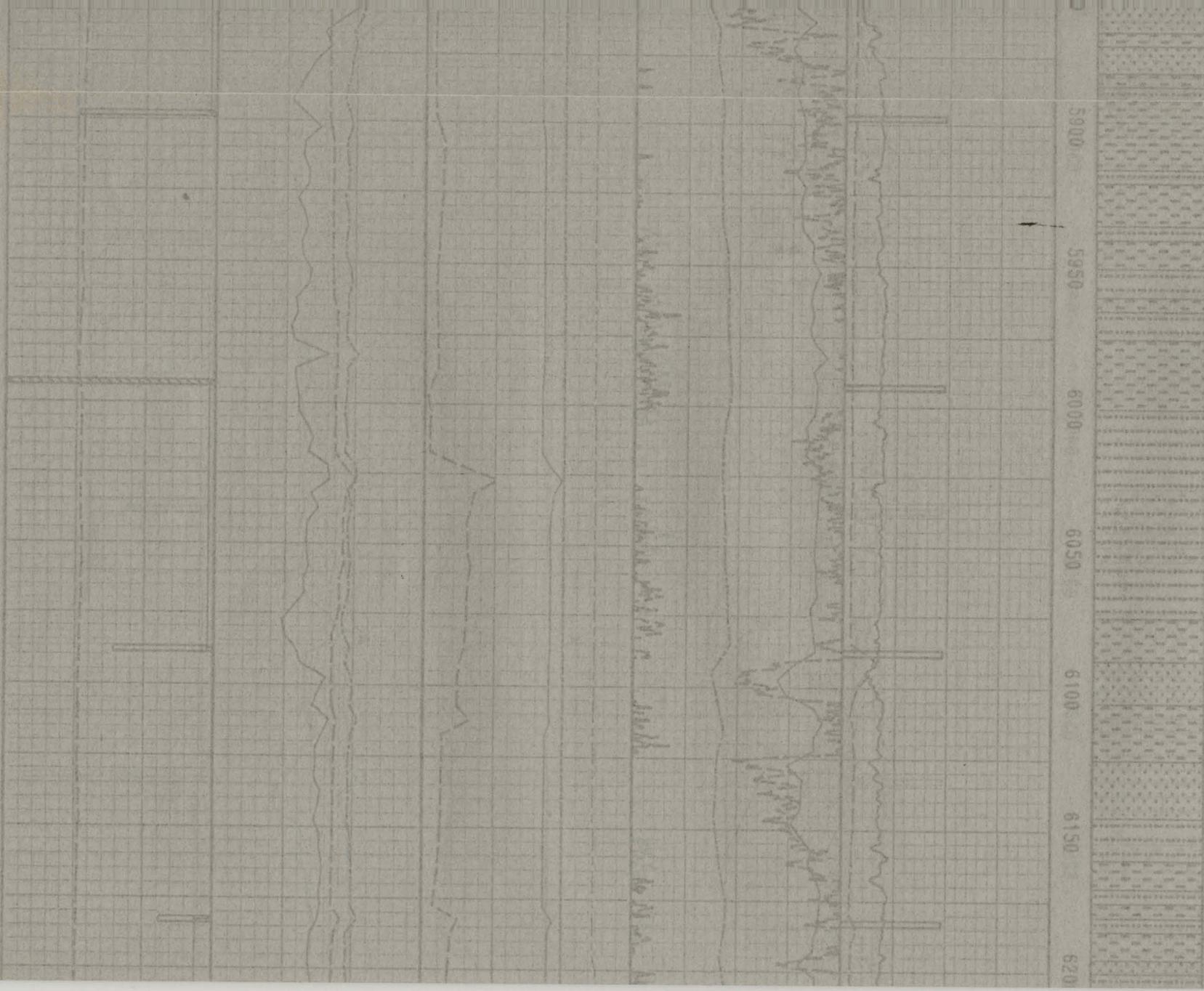


SVY @ 5522' .70deg.
STC 95



6-12-83

MW 10.0 VIS 55
PV/YP 20/23
FL 3.0 PH 9.3 CL 17500



5900
5950
6000
6050
6100
6150
620

SVT @ 5983' 1.24 Deg.

0.015 0.15 0.50



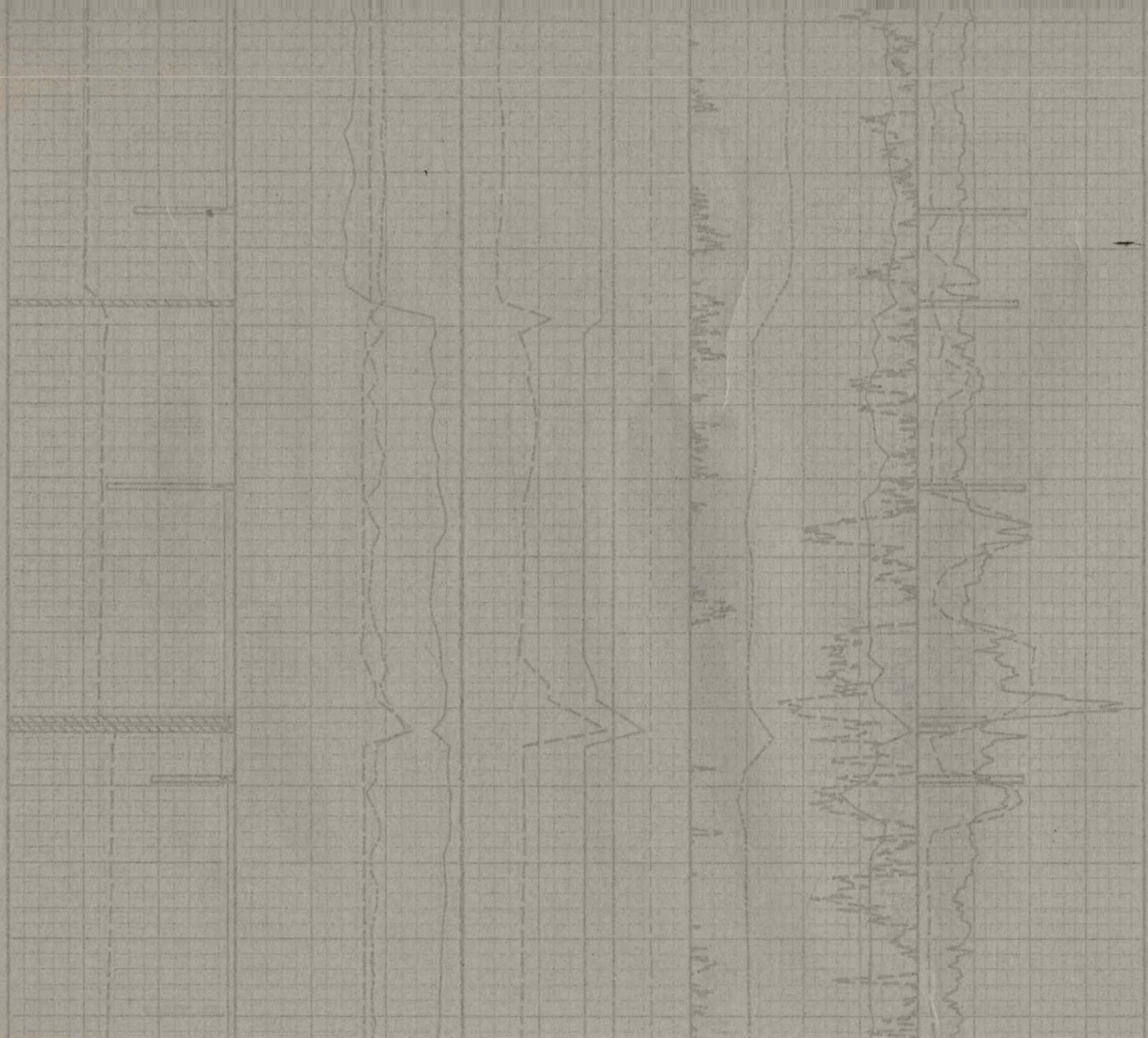
SVY @ 8343' 1.42 Deg.

SVY @ 8363' 1.42 Deg.

SVY @ 8547' 1.42 Deg.

MW 10.0+ VIB 59
 FV/YP 22/28
 FL 2.7 PH 8.1 CL 17K

8-13-93
 NB 5 12.25" DS-40H
 0-14 3-18 JETS
 TG 142



6500
6550
6600
6650
6700
6750
6800

SVY @ 8547' 1.42 Deg.
MW 10.0- VIS 59
PV/YF 22/28
FL 2.7 PH 9.1 GL 17K

8-13-93
NR 5 12.25° DS-40H
2-14 3-18 JETS
TG 142

8-14-93 NORT RC412 TFA 17
CORE #1 6729-6732 NO REC.
TG 98
RRB 3 DS-40H
2-14 3-18 JETS

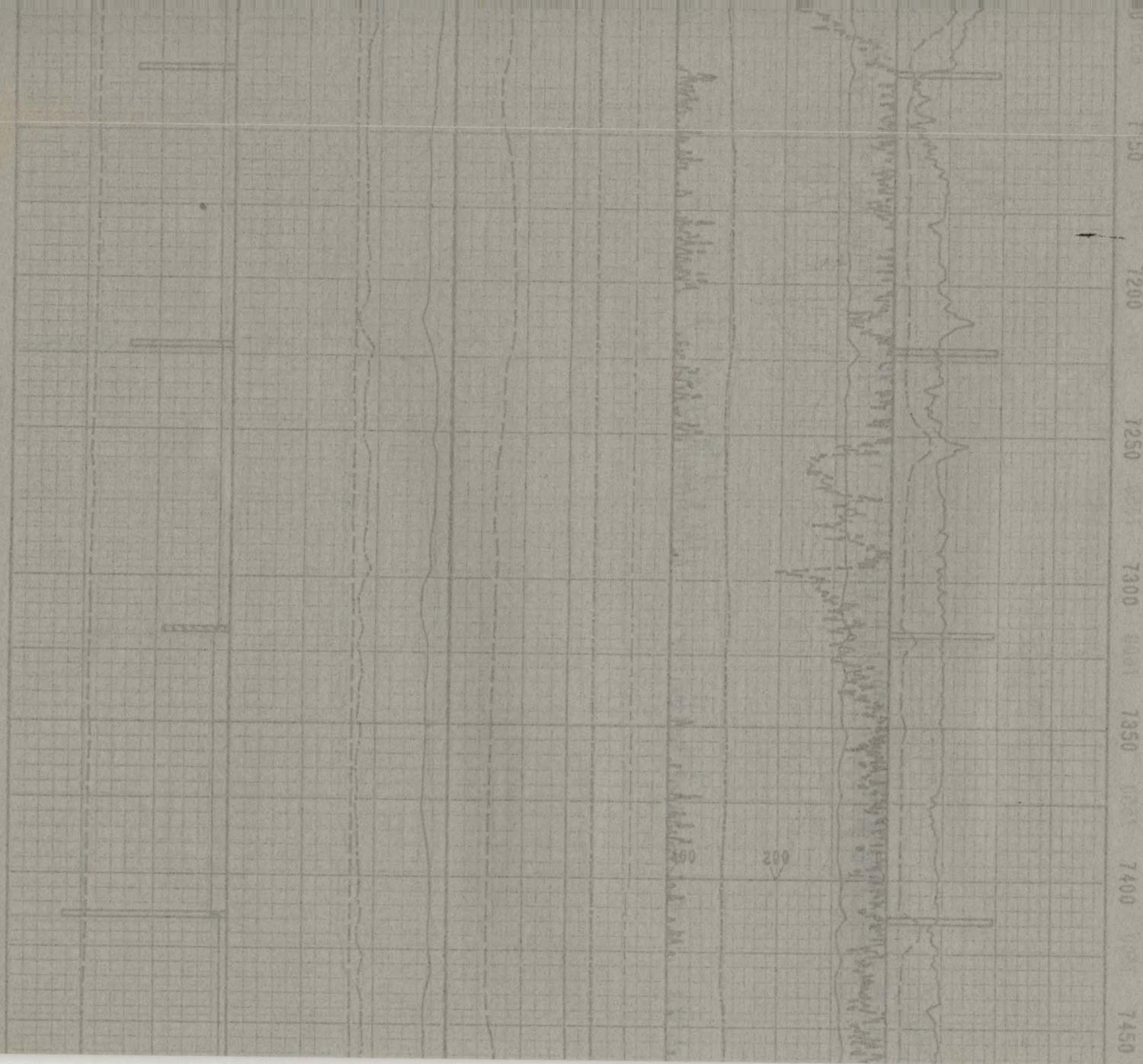
HW 10.1+ VIS 80
PV/TP 24/34
FIL 8.0 PH 8.9 CL 17K

8-15-83

SVY @ 6940' 0.89Deg.

8850 8900 8950 7000 7050 7100 7150

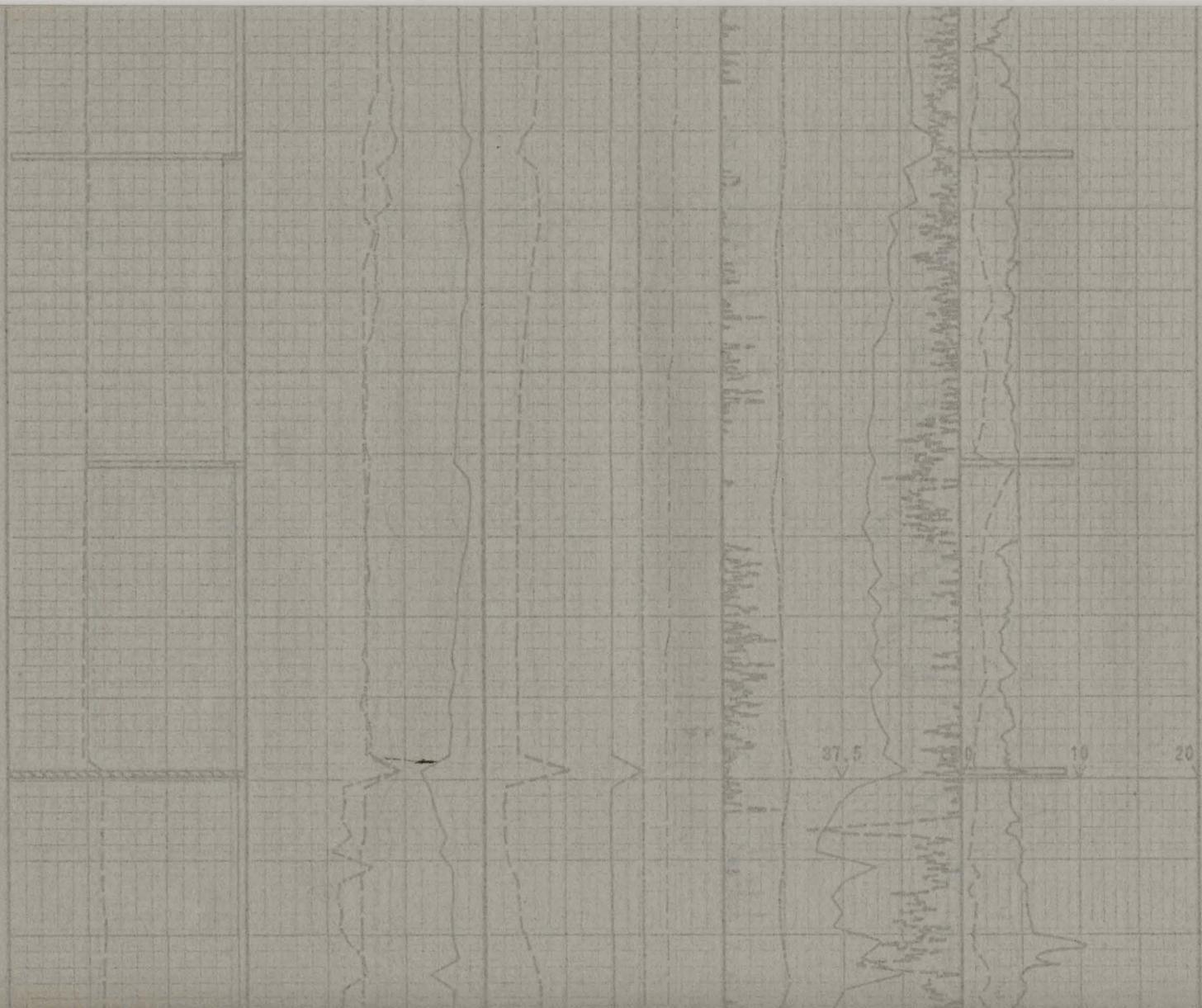




7000
7150
7200
7250
7300
7350
7400
7450



SVY @ 7413' 0.57Deg.

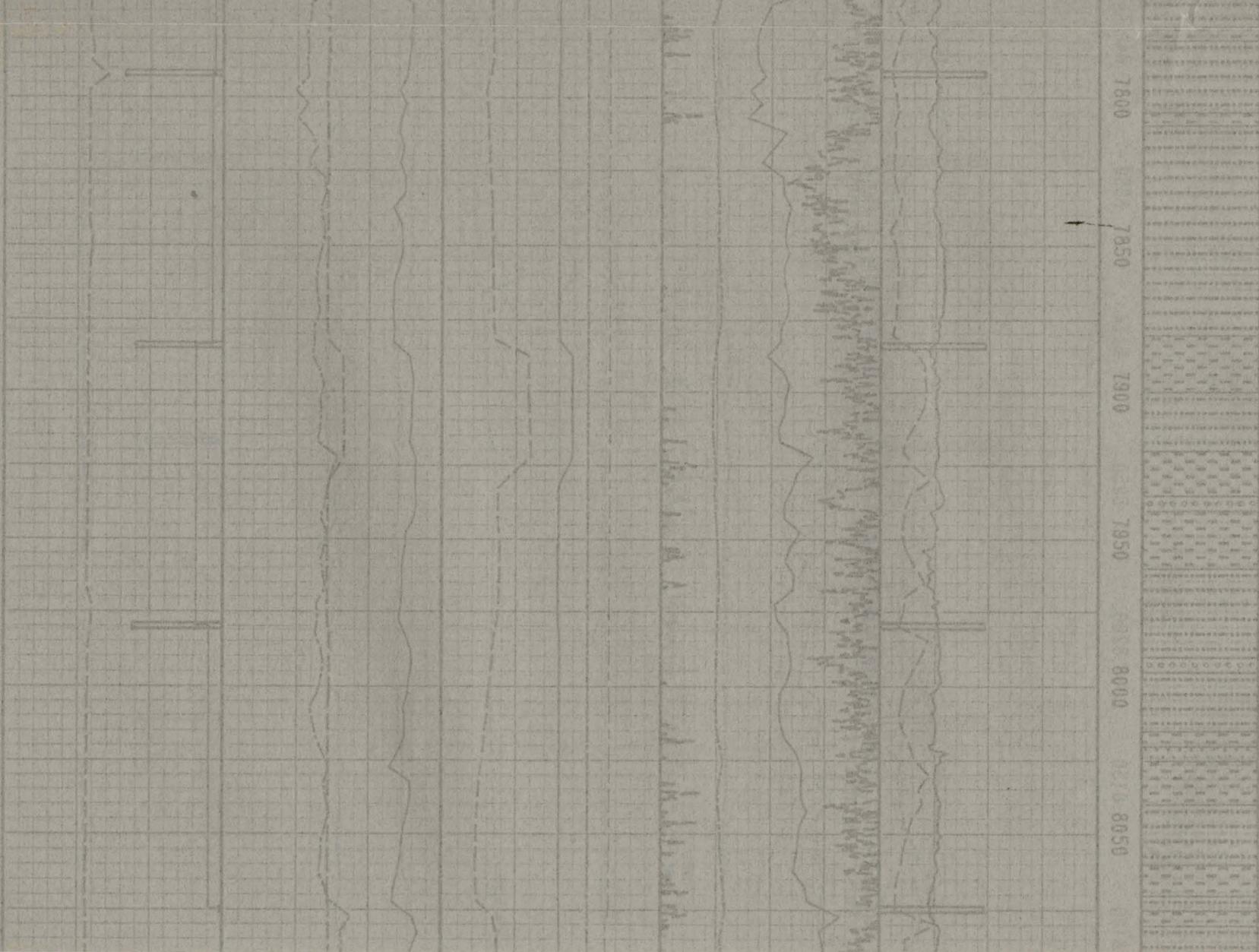


7500
7550
7600
7650
7700
7750

11 6 10 17 2154

6-16-83
STG 625
RW 10.0 VTS 59
PV/YP 25/30 PH 8.6
FIL 2.8 CL 17500

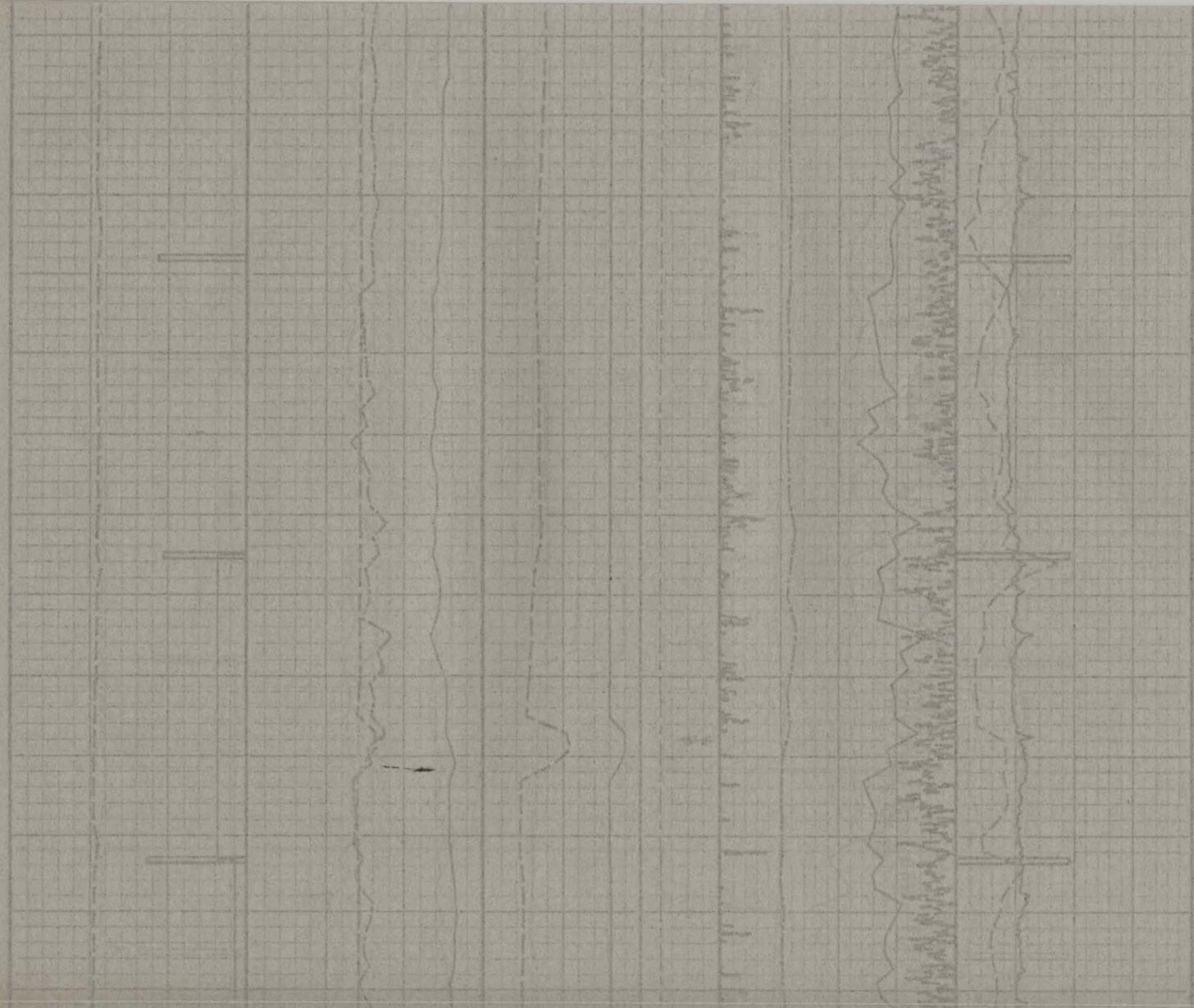
SVY © 7780' .042Deg



7800
7850
7900
7950
8000
8050

SVY © 8169' 0.480mg.

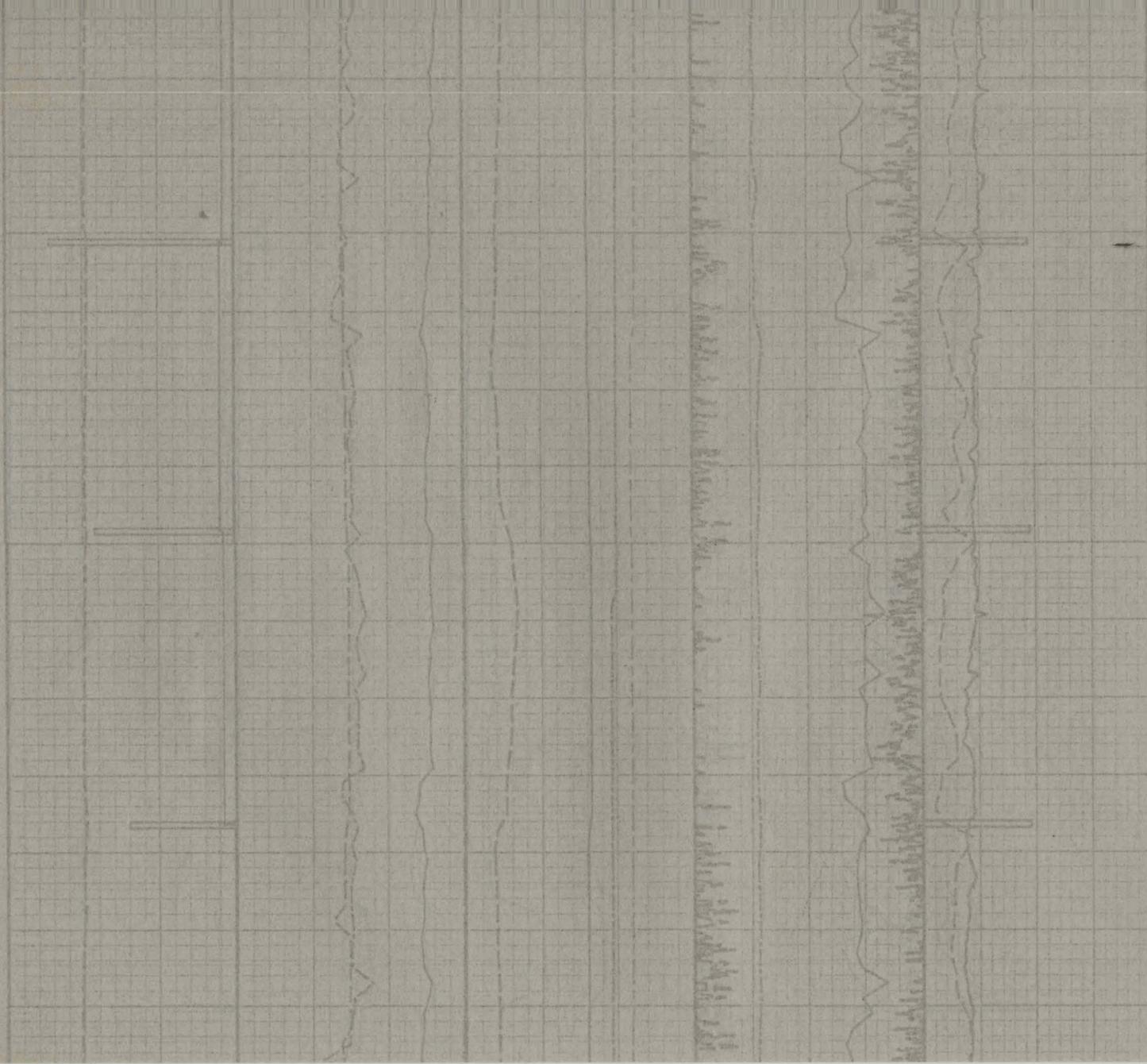
8100 8150 8200 8250 8300 8350 8400



8400
8450
8500
8550
8600
8650
8700

SVY @ 8453' 0.83Degs.

MW 10.2 IN



SVY @ 8735' 0.70Degs.

8750

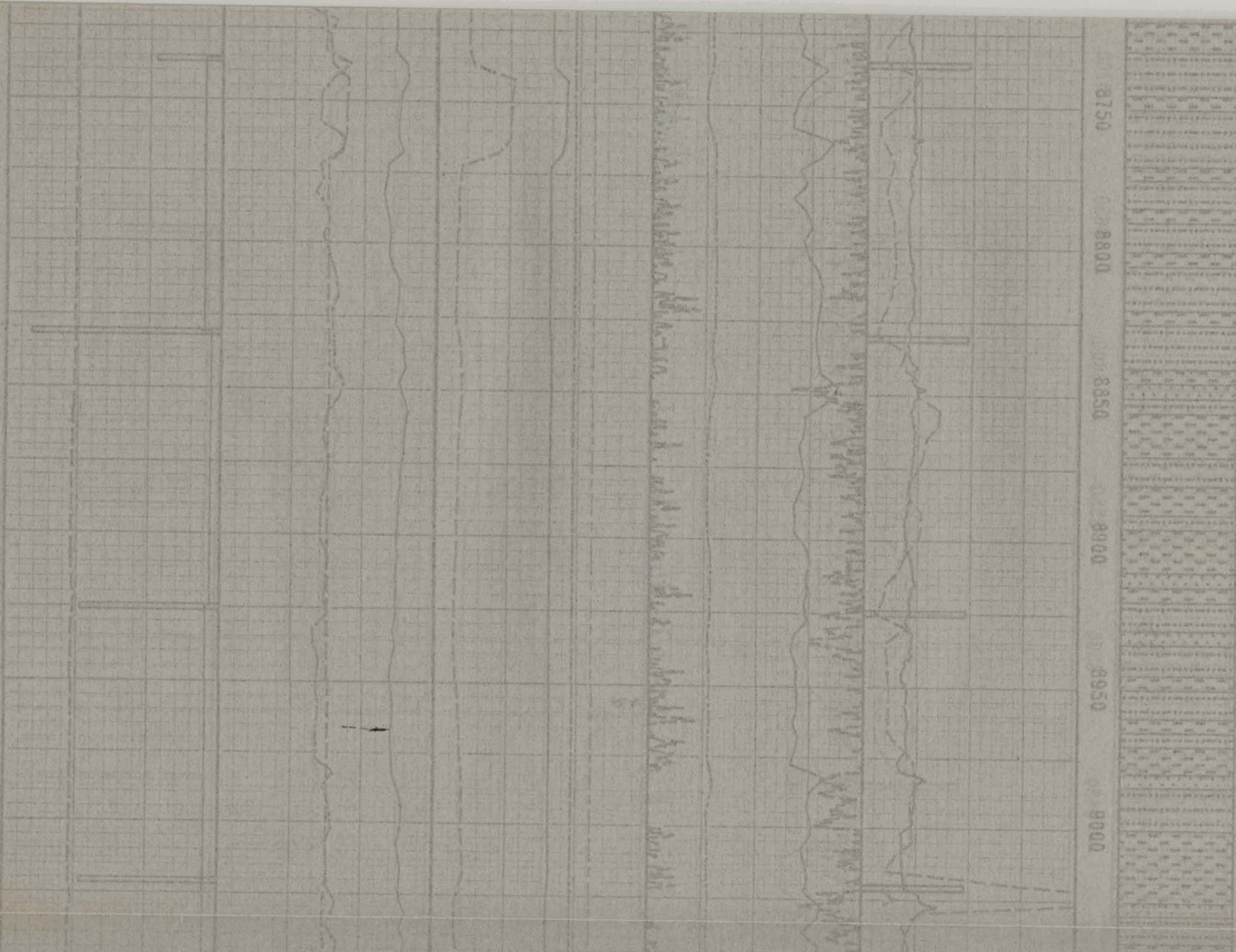
8800

8850

8900

8950

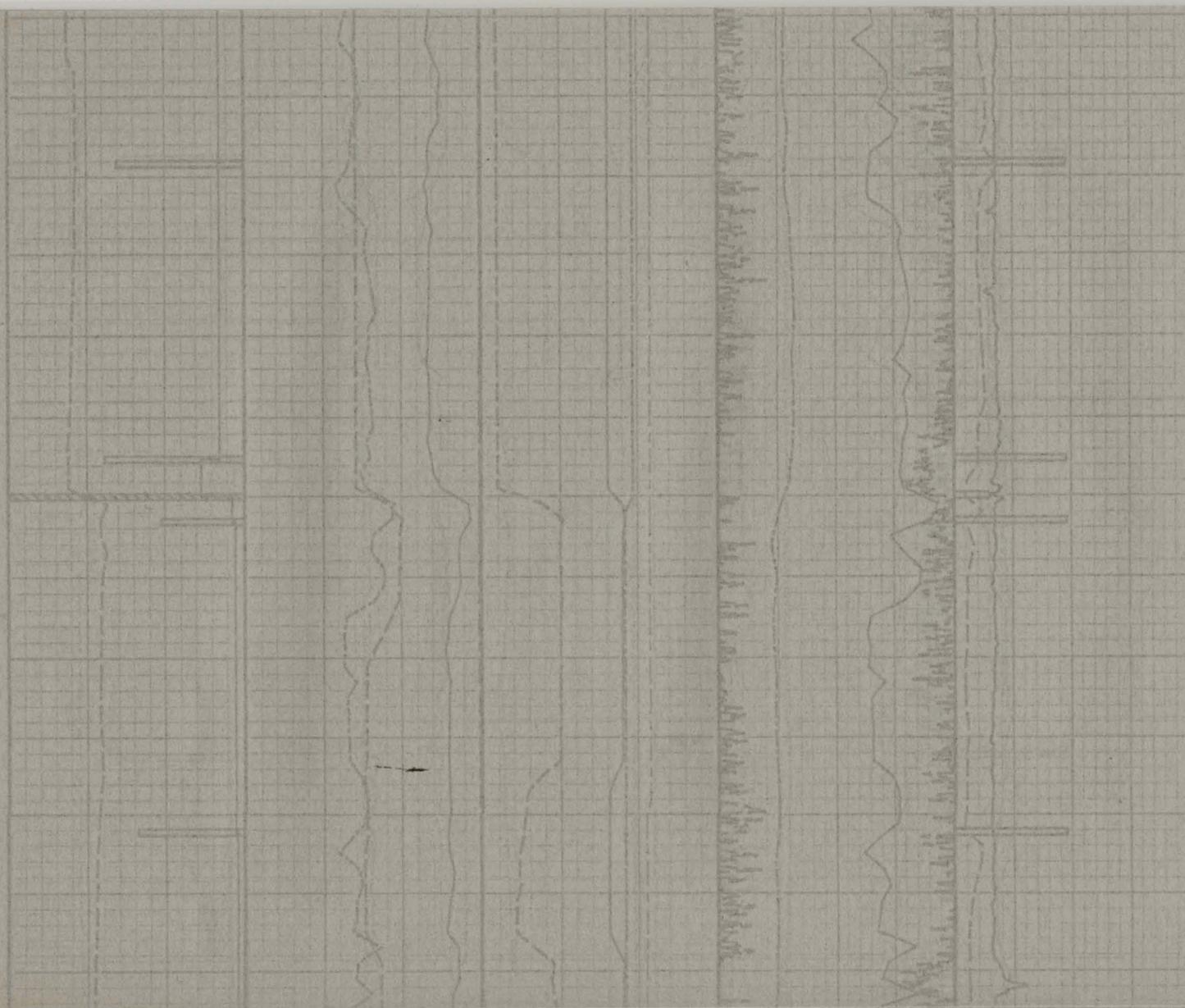
9000





SVY # 9297' 0.87Days.

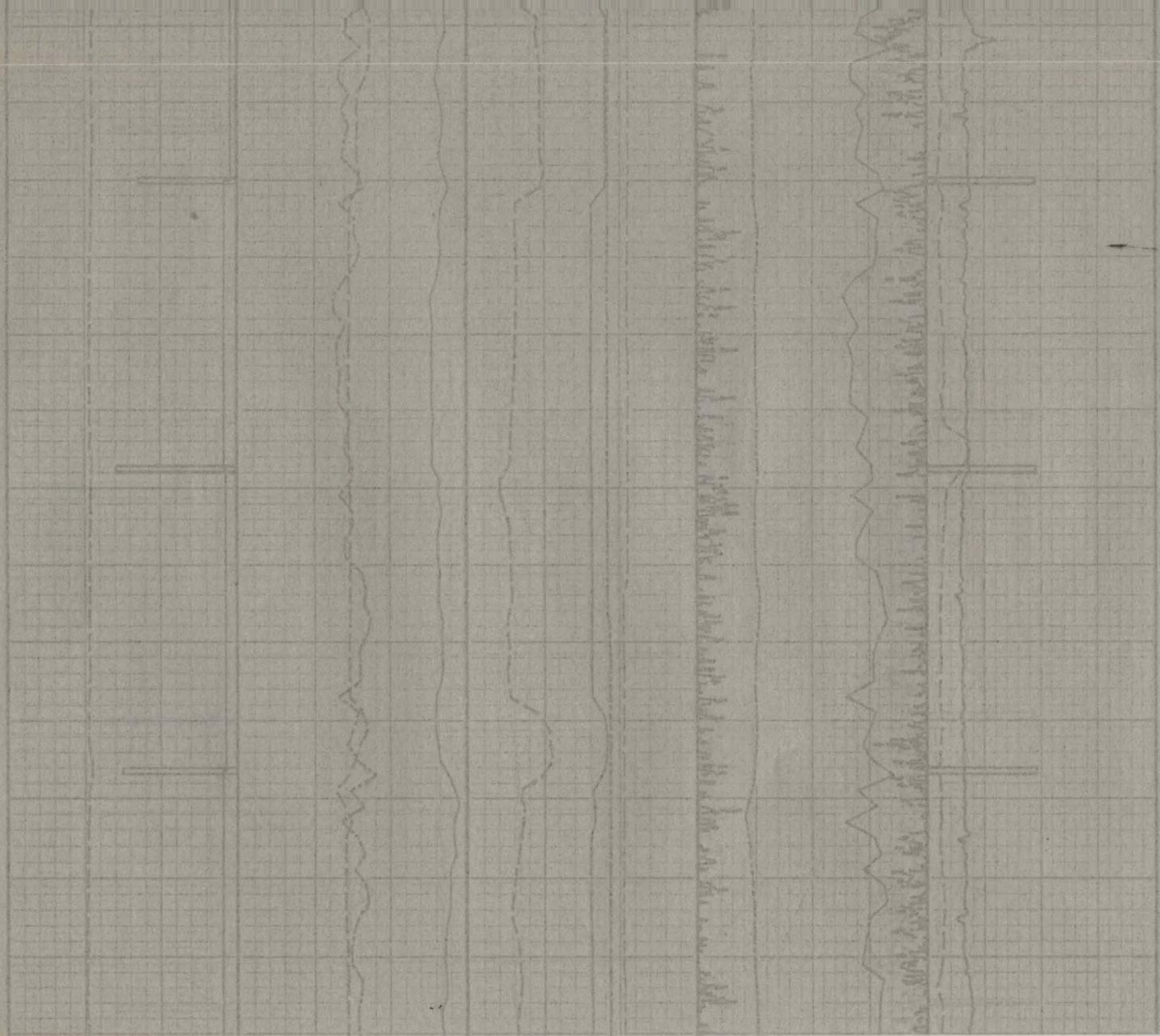
900
9050
9100
9150
9200
9250
9300



850
9400
9450
9500
9550
9600
9650



MW 10.4+ VIS 70
 PV/YP 30/40 PH 8.8
 FIL 2.6 CL 17K
 8-17-83
 SVY @ 8488' 1.25Deps.
 8-18-83
 25 9 13 25" DS40H
 0-13 JTS
 76 1541



9650
9700
9750
9800
9850
9900
9950



12-LEAD ECG

12-LEAD ECG

SVY @ 9984' 1.43Degs.

10000

10050

10100

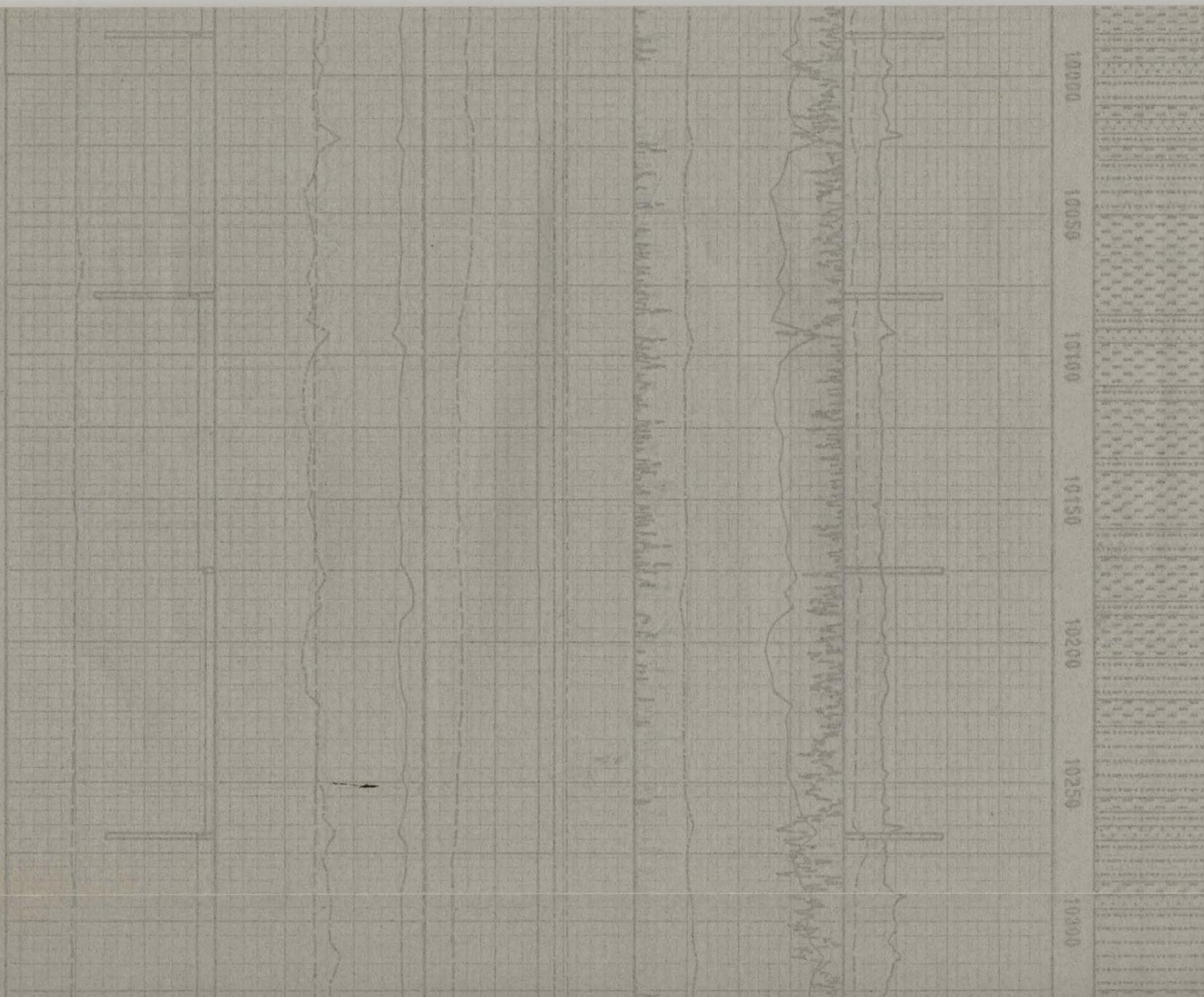
10150

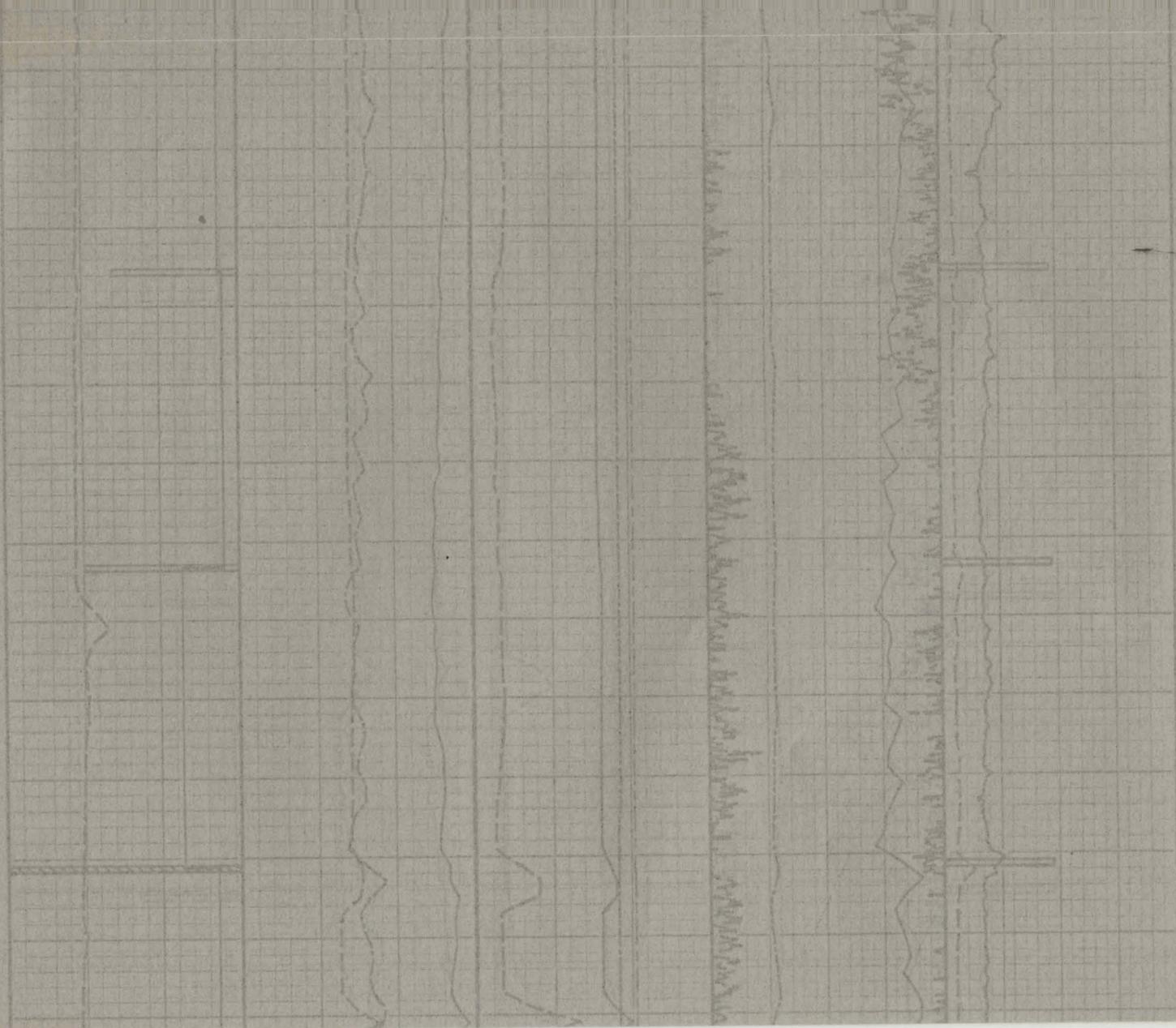
10200

10250

10300

SVY @ 10269' 0.87Degs.





10300
10350
10400
10450
10500
10550
10600



STG 683

8-19-83

STG 683

STG 683



10650
10700
10750
10800
10850
10900



RAISE MW TO 10.8

RAISE MW TO 10.7

10900
10950
11000
11050
11100

RAISE MW TO 10.7

MW 10.7+ VIS 58
PV/YP 27/34 PH 8.9
FIL 3.1 CL 17K

T.D. 11125'
C.D. FOR E-LOGS

CONN TIME (sec) (bar graph) 1K 500	WOB (KLBS) 50 25 RPM 200 100	FLOW IN (GPM) 1K 500 STND PIPE PRES 2400 1200	ROP (FT/HR) 400 200 GAMMA (API) 0 87.5 75	CONN LENGTH (bar graph) 100 200 MAX GAS UNITS 500 1K	DEPTH-feet	LITHOLOGY	REMARKS
TEMP OUT 100 50	TORQUE (AMPS) 300 250 TORQ DEV. 100 50	MUD WT IN (PPG) 12 10 EST PP (PPG) 12 10	"Dc" EXPONENT 1.5 3 SHALE DENS 1.8 2.2 2.0	EWR 10 20			
DRAG 100 50					MD		

SPERTY-SUN
DRILLING SERVICES
LOGGING SYSTEMS

RECEIVED
 OCS DISTRICT OFFICE

OCT 08 1993
 MINERALS MANAGEMENT SERVICE
 ANCHORAGE, ALASKA

COMPANY ARGO ALASKA INC.
 WELL NO. 2
 FIELD NEAUFORT SEA, BLOCK 672
 REGION ALASKA, U.S.A.
 LOCATION ANCHORAGE
 CONTRACTOR CANMAR
 RIG/TYPE SDV XULLUK
 TOTAL DEPTH 11125' TVD 11125
 SPUD DATE 22 JULY 1993

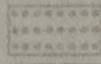
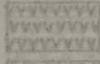
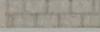
ELEVATION AND LOGGING DATA
 PERMANENT DATUM MEAN SEA LEVEL
 ELEVATIONS: K.B. 93
D.F. 64
G.L./S.F. 101
 LOG MEASURED FROM K.B.
 LOGGED DEPTHS 166 To 11125
 LOGGED DEPTHS _____ To _____
 SUPV. ENGINEER JOHN PATTON UNIT 2215

HOLE DATA
21 (RISER) To 171 17.5 To 3978
30" To 301 12.25 To 11125
28" To 1017 _____ To _____

CASING DATA
30" To 301 _____ To _____
20" To 1017 _____ To _____
13 3/8 To 3978 _____ To _____

MUD TYPES
SEA WATER _____ To 2017
GENERIC #2 _____ To 11125
 _____ To _____
 _____ To _____

LITHOLOGY SYMBOLS

 Coal	 Sandstone
 Tuff	 Sand
 Chert	 Gravel
 Limestone	 Conglom

ABBREVIATIONS
 DRILLING DATA

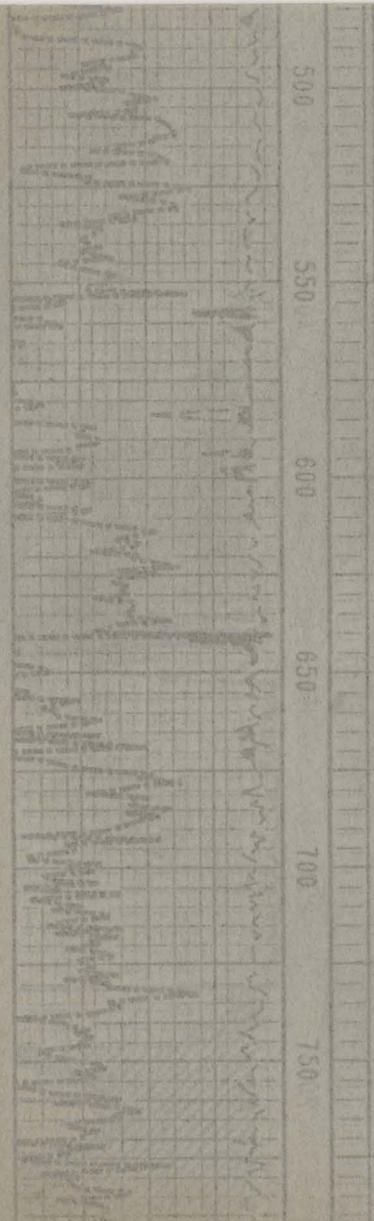
NB	Max Bit	LAT	Logged After Trip
RRB	Acron Bit	U	Gas Units
TB	Turbo Drill	BG	Background Gas
POCS	Polycrystalline Diamond Compound Bit	TG	Trip Gas
CB	Core Bit	STC	Short Trip Gas
DB	Diamond Bit	CG	Connection Gas
WOB	Weight on Bit	DST	Drill Stem Test
RPM	Revs Per Minute	DS	Direction Survey
CO	Circulate Out	DC	Depth Correction
PR	Pullup Return	C	Carbon Test
NR	No Return	CKF	Check for Flow
		FLT	Flaming Lamp
		BHT	Bottomhole Temp

MUD DATA

W	Mud Density	PV	Plastic Viscosity
V	Funnel Viscosity	YP	Yield Point
FL	Filtrate Loss	S	Solids Content
FC	Filter Cake	G	Gels
CL	Salinity	RH	Resistivity
PH	Hydrogen Ion Content	RMF	Filtrate Resistivity

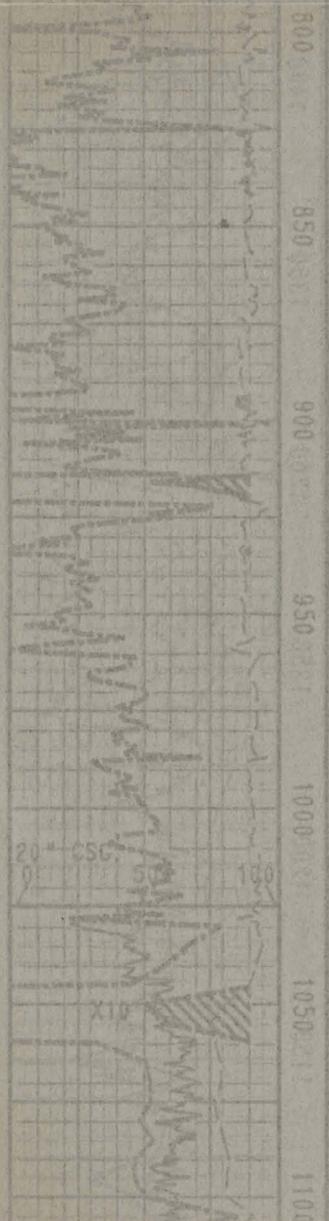
ENGINEERING DATA

	Core No. 1		Gas Traces
	DST 1 Drill Stem Test No. 1		Gas
			Oil Traces
			Oil



3 STD WIPER TRIP

120-83



20" CSC
0 50 100

X10



0.2 2 20 0 1.25 2.5 100 1K 10K

NO 2 17.5"
SS38SG.4
GX18 TX11
IN DEPTH 1030'

DRILLED TO 1030'
RUN 20" OD 18.75" ID
133 LB/FT CSG @ 1018'
LOT=12.9 ppg EMW
7-30/8-2-83
NO 3 12.25" FD7G
14-14-14-10
IN DEPTH @ 1040'
CLY-LTGY. INGY. AMORPH. CALC. MIC
MICA. TR-102 SPRNG-WRND QTZ +
LITH INCL. TR. PRY NODS +
PYR FOSS FRACS. TR. WH-YEL
FOSS SHELL FRACS. HYDRD +
VSFT
ABNDY PYR NODS + WOOD FRACS



SD-WI CLR. TRANSL. BY VOKBRN.
 OCC GRN VE-VEGR OCC PBL S2
 PRED MGR. SERND-BRND P-UNSR.
 INCL IN A CLY MTRX. 60% CLR
 FNSTO QIZ. 40% DRSM LITH GRD.
 NSOFC

SLT-CLR. WI. CY. CALC. CNT. ONLY IF
 PRED. SUSPENDED CRS. IN CLY.
 MTRX. SFT-UNCONS. GRDNG TO CLY

CLY-LTTN. TNGY. CALC. AMORPH.
 MIC. MICA. SD. + SLT. S2. QIZ. +
 LITH. INCL. HYDRD. + VSFT

SD-DK-LTGY. WI. CLR. PRED. DKCY.
 F-VCC. PRED. CCB. OCC. PBL. S2.
 SBANS-WRND. PRED. RND. WSRT.
 UNCONS. 50% LITH. FRAGS. 30%
 CNT. 20% QIZ. TR. PYR. TR. COAL.
 WOOD. FRAGS. TR. PYR. WORM
 BURROWS. SLT. TR. VDUL. TELORNG
 MIN. FLOR. NSOFC

GWL-CY. WI. CLR. YANG. FRAGS. OCC.
 PARTIALLY RND. ON ONE SIDE.
 PRED. FRAG. S2. 3 MM. PRED. QIZ. +
 CNT. INTGD. W/ SD. PROB. CLY.
 MTRX. NSOFC
 SVY. 0-1358'. 0.33 Deg.

CLY-TN. VL TGY. AMORPH. MIC. MICA.
 CALC. TR. CARB. SPECS. PYR. +
 WOOD. + SD. INCL. VSFT. + CHRY.
 HYDRD.



SD-WH. BLK. DKGY. CLR. M-CGR.
 OCC PBL SZ. SBRD-ANG. P.
 MSRT. UNCONS. 40% LITH
 FRAGS. 30% CHT. 30% QTZ.
 PYR. INCL. TR. WOOD. TR.
 COAL. TR. DUL. YEL. MIN. FLOR.

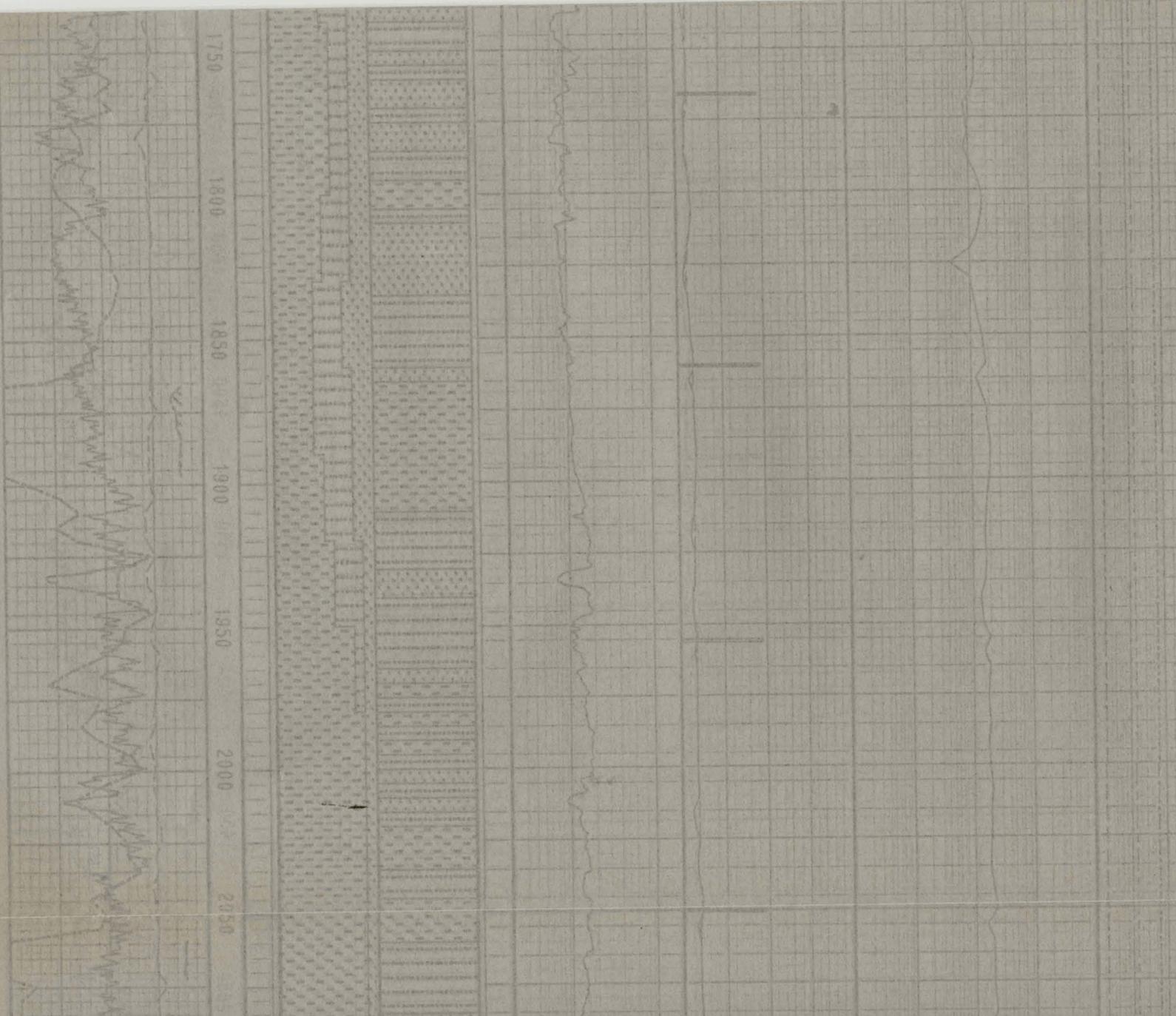
CLY-TN. LTGY. AMORPH. MIC
 MICA. CARB. SPECS. IP. CALC.
 TR. WOOD. HYDRD. VSFT.

ABD. CALC. + SHL. FRAGS.

SD-CLR. WH. BRN. BLK. M-CGR.
 SBRD-ANG. MSRT. UNCONS.
 50% QTZ. 20% LITH. FRAGS.
 30% CHT. TR. PYR. TR. CALC.
 + SHL. FRAGS. NSOFC.

SLTST-TN. LTBRN. M-DKGY. BLKY.
 CARB. LAMS. IP. INTBD. W/SD
 IP. CALC. TR. PYR. TR. CALC. +
 SHL. FRAGS. FRM.

ABD. TUFF-TN. BUFF. AMORPH.
 INTBD. W/SD. GRS. FRM. HD.



CLY-LT-MGY. AMORPH. CARB MAT
IP. CALC. HYDRD. VSFT. ABD
SH FRACS. ABD PYR.

SLT-LT-MGY. CARB SPECS IP.
CALC. F. SD. CRS. IN CLY.
MTRX. GRDC. TO CLY.
SVY @ 1852' 0.25 Deg.

ABD SHL. FRACS. + CALC.

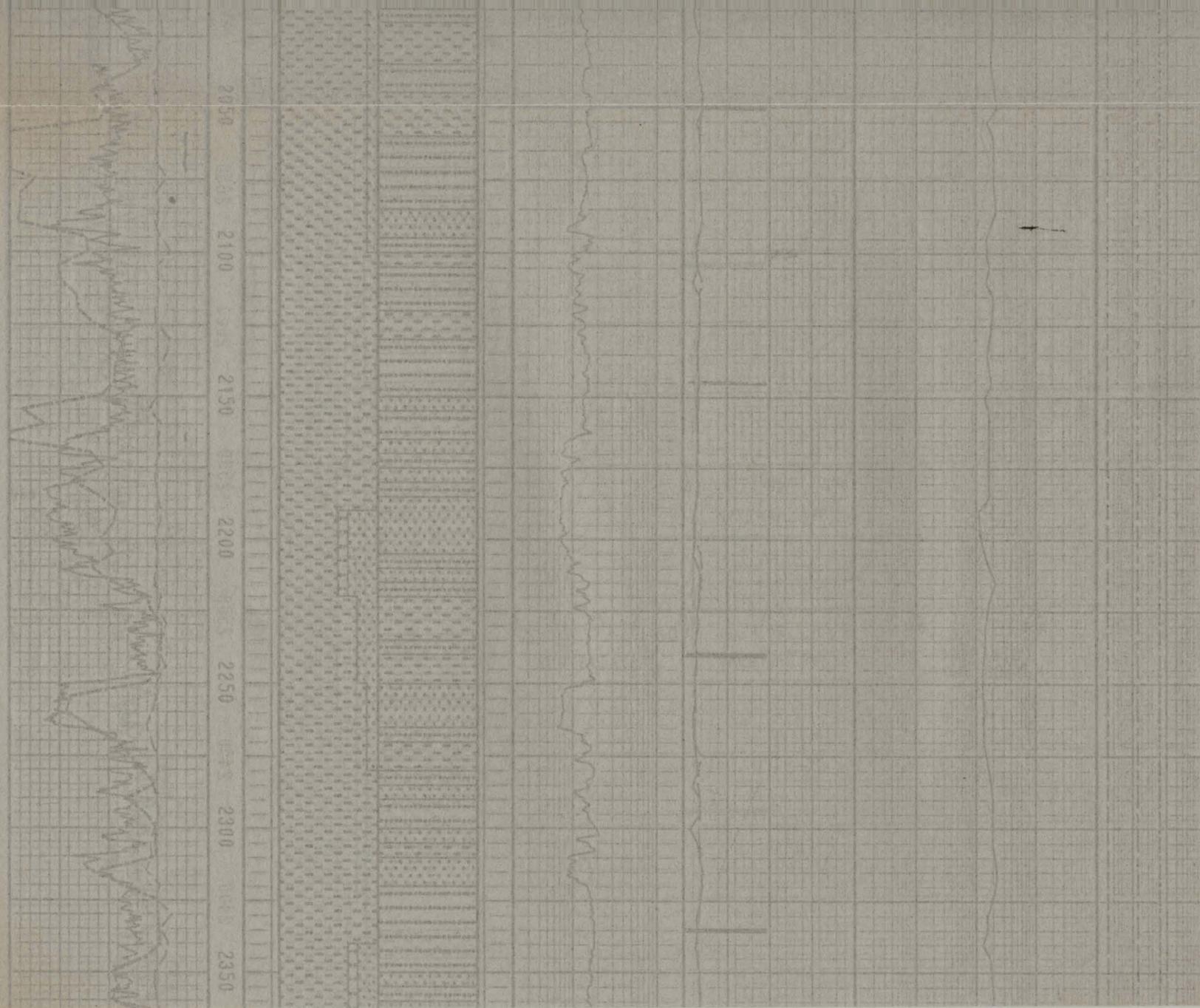
SD-WH. BRN. BLK. CN. F-CGR.
RNOD-ANG. H-PGRT. UNCONS.
40% DTZ. 40% LITH FRACS.
20% CHT. TR. PYR. TR. CALC.
TR. DOL. YEL-ORG. MIN. FLOH.
NSOFC.

CLY-M-OKGY. AMORPH. CARB
SPECS. VFGR. SD. HYDRD.
GMMY. VSFT.
8-3-93

MW 9.8 VIS 50
PV/YP 24/21
FL 4.8 PH 9.8 CL 19000

CLY-M-OKGY. AMORPH. CARB
MAT. VF-FGR. SD. SLI. CALC.
GMMY. SET.

SD-CLR. WH. BRN. BLK. VF-
FOR. OCC. CCR. SRANG. CCRH
WSRT. IMBDD. IN CLY. UNCONS.



SD-CLR. W. BRN. BLK. VF-
6MM SFT.

SD-CLR. W. BRN. BLK. VF-
FOR OCC. CGR. SBAND-CGRD
WSRT. IMBD IN CLY. UNCONS.

CLY-MGY. M-ORRN. AMORPH.
CARB. SPECS. VF-FGR SD. CGR.
SLI CALC. HYDRD. TR. CALC. VSFT.

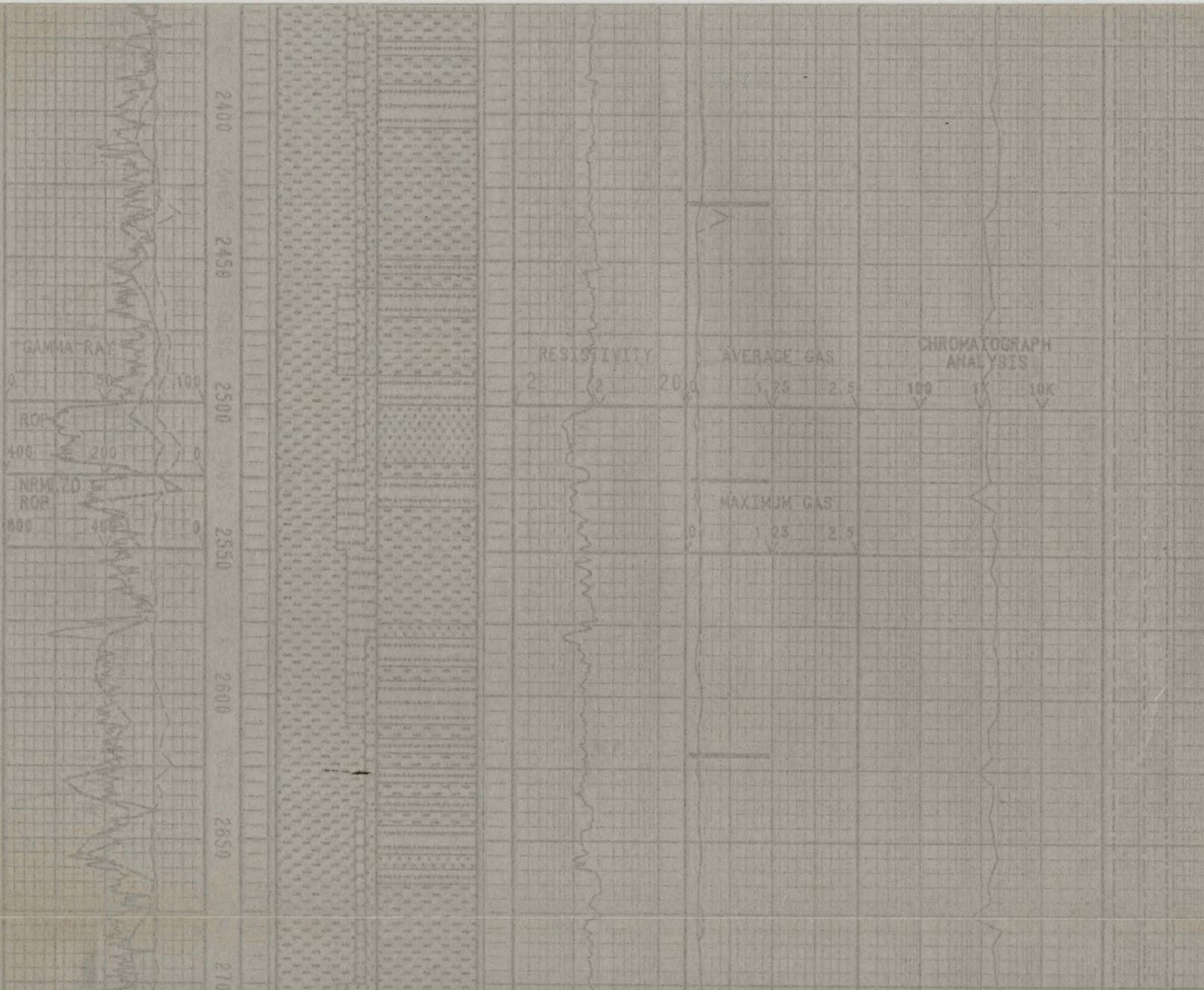
CLY-MGY. MORN. AMORPH. CARB
SPECS. IP. SLI CALC. HYDRD.
TR. CGR. SD. TR. CALC. VSFT.

SVY @ 2210' 0.24 Deg.

SD-CLR. W. BLK. F-CGR.
SBRD-ANG. M-WSRT. UN-
CONS. 30% QTZ. 50% LITH
FRAGS. 20% CHT. TR. PYX.
TR. CALC. NSOFC.

CLY-MGY. AMORPH. CARB
SPECS. VF-FGR SD. OCC
CGR. SD. SLI CALC.
HYDRD. VSFT.

SD-CLR. W. BLK. F-CGR.
SBRD-ANG. MORN. UNCONS.
30% QTZ. 50% LITH
FRAGS. 20% CHT. TR. PYX.
TR. CALC. NSOFC.



CLY-LTH. VLTGYBRN. AMORPH. CAL.C.
AREN IP. SLT + FGR. SD INCL.
DCC MGR. SD. MIC. MICA. TR. CARB.
SPECS. HYDRTO. VSFT

ST @ 2435'
STC 61u

CVL-DK-LTCY. M-DKBRN. WI. CLR.
CCR. SD-PBL. SZ. FRACS. SBAND-
MRO. PRED. AND. SMC. ANG. FRACS.
SUSPENDED INCL. IN CLY. MICA.
80% CHT + LITH. FRACS. 20%
CLR-FRSD. QVZ. TR. PYR. NODS.
SVY @ 2485' 0.23 Deg.

ABNOD. CARB. LAMS + CARB. SLTST.
STRNGRS. INTSD. IN CLY.

SLTST-TN. CY. CLR. NUTT. IP. AMORPH-
BLKY. ARG. CLY. MTR. ERTHY. SLT-
VCL.C. CRDNG. TO. VFCR. SS. IP.
TR. F-MGR. SD. INCL. TR. CARB.
SPECS. + LAMS. IP. SFT +
HYDRTO-HD + BRIT. IP.

CLY-TN. VLTGYBRN. AMORPH. MIC.
MICA. AREN. IP. CRDNG. TO. SLT.
IP. TR. VFCR. SD. INCL. TR. PYR.
NODS. TR. CARB. LAMS. CHMY.
HYDRTO + VSFT



SD-LT-DKGY. CLR. WH. M-CGR.
 PRED. CCR. SBANG-WIND. PRED.
 SBAND. MSRT. UNCONS. POSS. CLY
 MTRX. 60% CHT + LITH FRAGS.
 40% CLR-FASID. QTZ. PYR. NODS.
 NSOFC

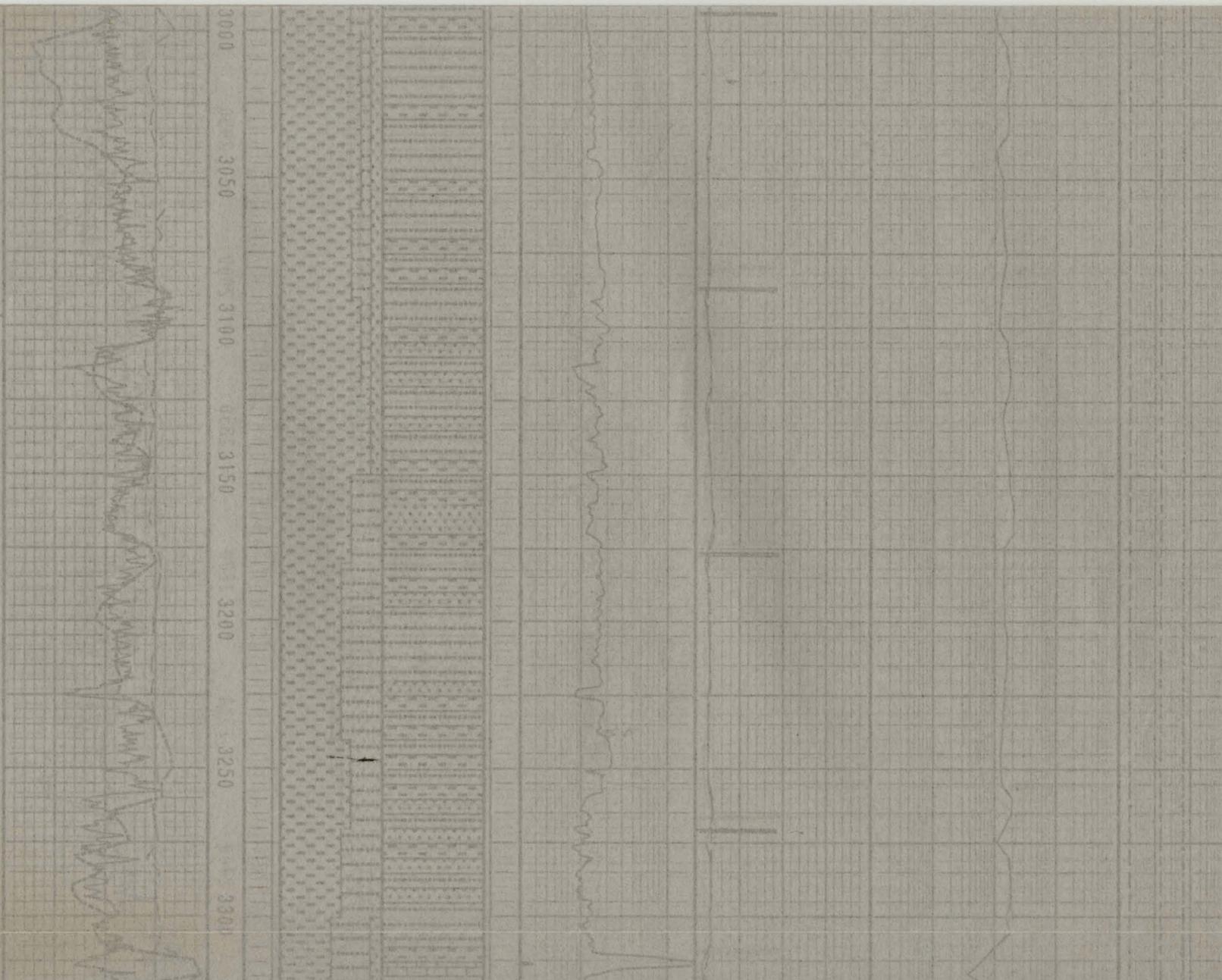
CLY-LT-MGY. MBRN. AMORPH.
 MIC. MICA. TR. VF-FGR. SD.
 INCL. OCC. CCR. SD. CALC.
 TR. PYR. TR. CALC. TR.
 FORAMS. HYDRTD. VSFT.

CLY-LT-MGY. MBRN. AMORPH.
 TR. VF-FGR. SD. INCL. OCC.
 CCR. SD. CALC. TR. PYR.
 HYDRTD. VSFT.

SD-CLR. WH. BLK. VF-MGR. OCC.
 CCR. PRED. SLT. SZ. ANG-
 RND. WSRT. UNCONS. IN
 CLY. MTRX. 80% QTZ. 20%
 LITH FRAGS. 20% CHT.
 TR. PYR. TR. CALC. NSOFC.

SVY @ 2883' 0.37 Deg.

SLT-LT-MGY. AMORPH. VAREN.
 CARB. SPECS. IP. HYDRTD.
 GMMY. IP. VSFT.



CLY-MGY. MBRN. AMORPH.
MIC MICA. CALC. TR
PYR. HYDRD. VSFT.

SLT-LT-MGY. AMORPH. AREN.
CARB MAT. IP. HYDRD.
GMVY IP. TR PYR. VSFT.

CLY-LT-MGY. MBRN. AMORPH.
CALC. TR PYR. HYDRD.
VSFT.

SLT-MGY. AMORPH. AREN.
VFGR QTZ GRS. OCC CGR
SD. CALC. HYDRD. VSFT.

CLY-MGY. MBRN. AMORPH. CALC.
MIC MICA. CARB SPECS IP.
HYDRD. GMVY. SFT.

8-4-03
TR LS-MY. LTCY. AMORPH-

SL191-M-LTGY-LTBRK AMORPH. BLKY
IP CALC. REF. CLT. HENK. WFR. 30

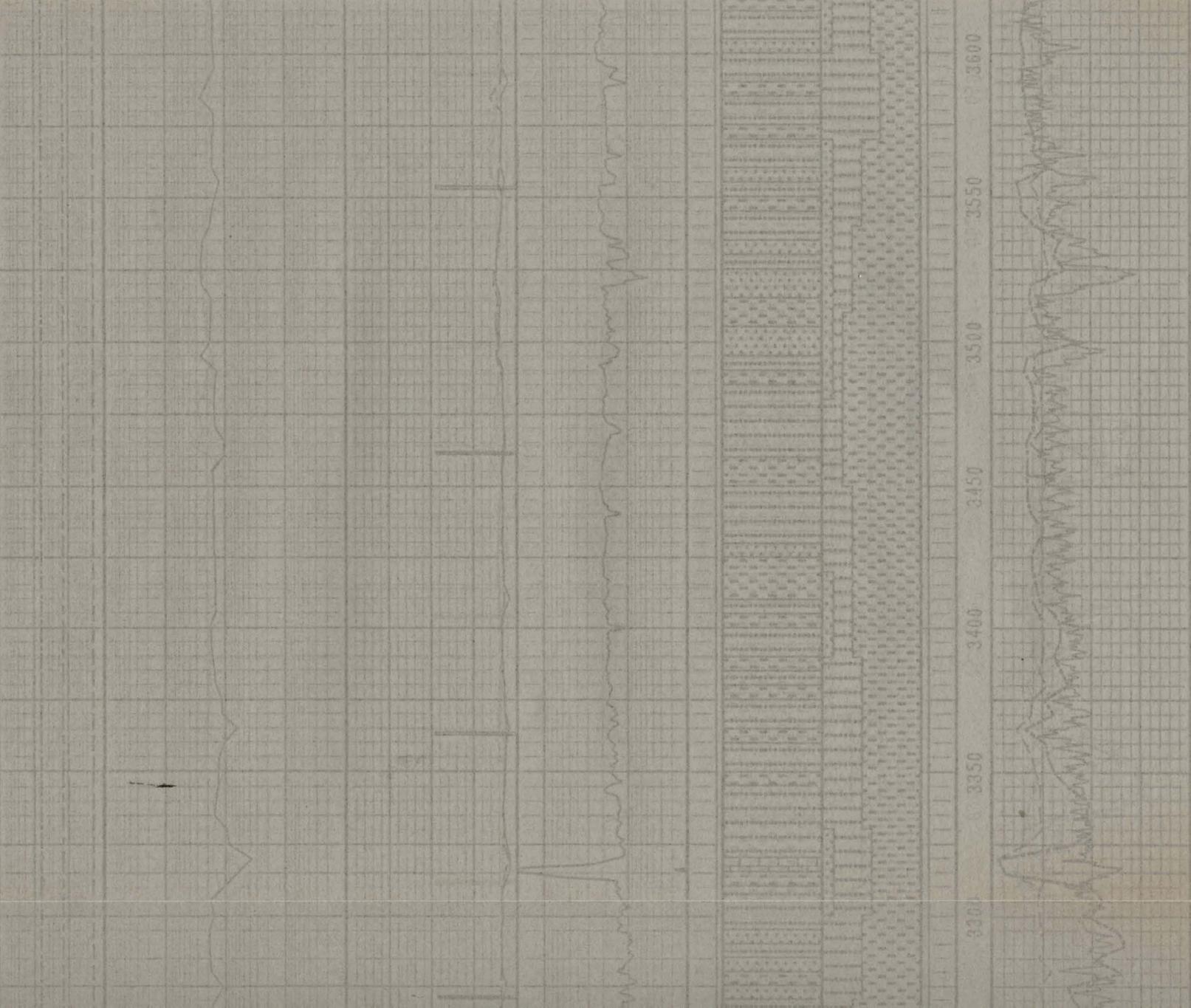
NSOFC
OHT. TR. P.YR. TR. CALC.
40% LITH. FRACS. 20%
MSRT. UNCONS. 40% Q1Z
DCC. CGR. SBRD. ANG. M.
SD-CLR. MH. BLK. WF-MGR

CLY-LI-MGY-MBRN. AMORPH.
CARR. SPECS. IP. ARG. DCC
F-CGR. 50. HYDRID. CMY. SFT.

SL1-LI-MGY. AMORPH. AREN.
VFR. Q1Z. CGR. DCC. CGR.
SD. CALC. HYDRID. VSET.

18-LS-M-LTGY. AMORPH.
BLKY. CH. KY. CARR. SPECS.
IP. RBY. IP. V. CALC. HYDRID.
VSET.
SVA. 9.2234. 0.40 D&G.
MM. 8. 8. VIS. 34
PV/VR. 21/23
FL. 4. 0. PH. 9. 5. CL. 16000

CLY-MGY. MBRN. AMORPH. CALC.
MIC. D.V. CARR. SPECS. IP.
HYDRID. CMY. SFT.



SWY # 3614 0.39 Deg.

CLY-INDY. VLTBRN. AMORPH. INTBD
W SLT + VFGR QTZ SD INCL.
SLI-MCALC GRDNG TO SLTST IP.
ABDNT CARB LAMS. HYDRTO. SFT

SD-LTCY. CLR. WH. TRANSL. VF-MGR.
OCC CGR. PRED FGR. ANG-SBRND.
PRED SBANG. PSRT. UNCONS. TR
PYR. CNT. PROB. CLY. MIXX. TR
CALC. CNT. IP. TR. CARB. LAMS.
TR. BLK. PYR. FOSS. BRACH. 70%
QTZ. 30% LITH. FRAGS. NSUFC

COAL-BLK. VOKBRN. PLTY. PKLY.
BLKY. IP. SBVIT. PYR. MOO. FRAGS.
INTBD. W. SD + CLY. FRM. MID +
BRIT

CLY-LTTH. VLTGY. AMORPH. SLI. CALC.
SLTY. GRDNG TO SLI. IP. TR. WGR
SD INCL. HYDRTO. SFT

SD-M-DKCY. BLK. CLR. WH. M-CGR.
OCC. PBL. ST. PRED. MGR. ANG-
SBRND. PRED. SBANG. P-MSRT.
UNCONS. TR. CALC. CNT. IP. PROB.
CLY. MIXX. IP. SLI. TR. CALC. XLS.
TR. WH. FOSS. SHELL. FRAGS. TR.
TRFF. SLI. IN. DR. YEL. MIN. CLDR

SWY # 3877 0.25 Deg.



SVY @ 3977' 0.25 Deg.

STG-87a
8-5/10-83
SET 13 3/8" CSG @ 3977'
LOT # 14.9 pag ENW
MR 4 12.25" FDTOL
12-12-12-12 JETS
IN DEPTH 4005'

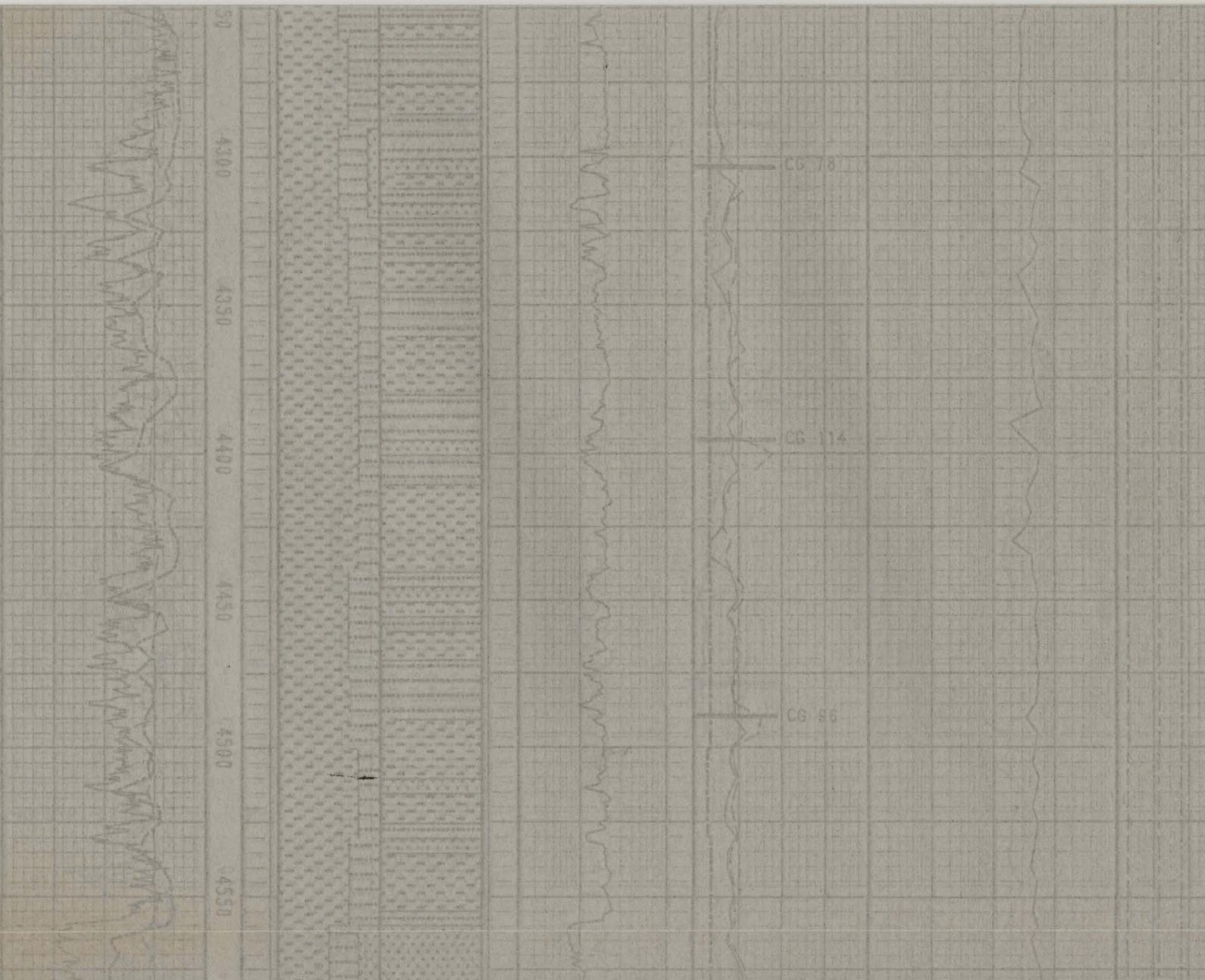
CLY-LT-MCY GYTH AMORPH SLTY
GRONG TO SLT IP. TR CGR
SD INCL VHYDRID + VSET

TR GOAL-BLK SLKY HKLY IP
SHVIT. LRS FRACS INTBD W CLY
+ SLT. HD + SKIT

MW 8.8 VIS 51
PV/YP 15/17
FL 3.0 PH 9.2 CL 16000

SD-CLR. LT-DKCY. TRANSL. W/ WGR.
SBANG-RND. PRED SBRND.
PSRT UNCONS. CLY MTRX PROB
SD ENCL IN CLY GRONG TO SLT
SL GRS. INTBD W/ CLY + BLT.
MSDFC





SVY @ 4277', 37Deg.
 CLY-TH LTGYBRN. ANDRPH. CALC.
 MIO MICA IP. VSLI TY GRDNG
 TO SLT IP. VHYDRID + VSFT

SLTST-LT-MGY. LTGYBRN. SFT.
 SLT CALC-CALC. STKY. CMNY.
 VARG. CRDC TO SLTY CLY.

CLY-LT-MGY. LTGYBRN. SFT.
 SLTY IP. STKY SLI CALC.
 CALC TR SD. TR COAL FRAGS.

SD-CLR. LTGY. BLK. VF-FGR. SB
 ANG. VSFT UNCONS. TO QTZ.
 30%LITH FRAGS. NSOFC

CLY-LT-MGY. GYBRN. SLTY. VSLI
 CALC IP. TR SD. OCC COAL SPKS.
 SFT. STKY.

SVY @ 4552', 47Deg.
 CLY-LT-MGY. LTGYBRN. STKY.
 SLTY. TR SD. VSLI-N CALC.
 VSFT

SD-W-VOKGY. TR BRN CLR. MIO
 F-MGR. TR CCR. PRED ANG-SB
 ANG. OCC. SBRNO. M-PR. SRTD.

SVY 8 432 470eg.
CLY-LT-MGY LTGYBRN. STKY.
SLTY TR SD. VSLI-N CALC.
NSPT

SD-M-VDKGY TR BRN CLR WH.
F-MGR TR CGR FRED ANG-SB
ANG. OCC SBRND. M-PR. SPTD.
ABNT CLR. VF-SLT SZ. ANG. QTZ
GRS. FLTG IN SLTY CLY MFL.

CLY-MGY. CYBRN. SLTY. OCC.
SDY. NSCALC. STKY. SFT.

SLTST-LT-MGY. VARG. TR SD.
NSCALC TR. COAL SPKS. GRDG
TO WGR SD. IF. SFT.

SD-OKGY. BRN. BLK. CLR. WH.
F-MGR. ANG-SBANG. M-PR.
SPTD. UNCONS. 40%LITH FRAGS.
40%HT. 20%QTZ. NSOFC.

SD-CLR. LTGY. VF-FGR. SBANG-ANG.
M-NSRTO. GRDG TO SLTST. PRED
CLR. QTZ. UNCONS. NSOFC.

SVY 8 4835 1.380deg.

8-11-43
CLY-LT-MGY-MGYBRN. SLTY.





OSC VGR FLTG SD NCALC.
TR PYR. STKY. SFT.

SLTST-LT-MGY CRDG TO VF
GR SD IP VARG TR PYR.
NCALC. SFT.

MW 9.84 VIS 58
PV/YP 19/19
FL 3.2 PH 8.9 CL 17000

CLY-LT-MGY CYBRN NCALC.
SLI-VSLTY FLTG SD GRG:
GMY. SFT.

SVY @ 5020' +1Deg.

SLTST-LT-MGY VARG ABNT VF
GR SD NCALC. TR PYR. SFT.

SD-CLR. LT-DKCY. BLK. BRN.
VF-MGR SBANG-ANG. PR-M
SRTD. FLTG IN SLTST & CLY
MTX. UNCON. NSOFC.

CLY-LT-MGY CYBRN. SLTY. SLI
SOY. SLI. CALC. TR PYR. STKY.
GMY. SFT.

TR AMBER

SLTST-LT-MGY VARG. DECR VF
DTZ SD TR PYR. SLI. CALC.
TR BOL ORG & PINK MIN FLUOR.
GT. SFT.

SLTST-M-DKCY. TR IP. ANORPH. BLKY
IP. CALC. VCALC. TR VGR SD. IF
ARG. ORGNS TO CLY. TR CARB
SPECS. SFT. + HYDRD-MGD IP



SLTST-M-DCY IN IP AMORPH. BLKY
 IP CALC-VCALC TR VFGR SD IP
 ARG GRDNG TO CLY TR CARB
 SPECES: SFT + HYDRTO-MHD IP

LS-IN ORNGYEL. BLKY SLTY AREN.
 GRDNG TO VCALC SLTST IP TR
 CARB SPECES TR CALC XLS. MHD

SD-CLR. TRANSL. MGY BLK WF-FGR.
 PRED VFGR OCC MGR ANG DYE
 ANG-SBRNG. PRED SBANG. P-MSRT.
 UNCONS. SLI TR CALC CMT IP
 ARG CLY + SLT MTRX. 80% DTZ.
 20% HRBLND + LITH. MSOFC

SLTST-M-LTCY AMORPH. ARG. GRDNG
 TO CLYST. VCALC. TR VFGR SD
 INCL. TR CARB MAT. VSFT

SD-CLR. M-LTCY. MLI. TRANSL. BLK.
 WF-FGR. PRED VFGR. ANG-SBRNG.
 PRED SBANG. P-MSRT. UNCONS.
 PROB. INCL. IN CLY MTRX. 70%
 DTZ. 30% HRBLND + LITH. TR
 CARB SPECES. MSOFC

NOTE SCALE CHG:
NRM. ROPS
400

5550
5600
5650
5700
5750
5800
5850

CG 32

CG 19

GVY 0.5322 70deg
STB 03

TUF-LTGY. WH. ORG. SLTY IP.
WXY IP. HEM STN IP. SFT.

SLTST-LT-MGY. PRED. SDY. ARG
IP. OCC. CARD. SPECS. TUF IP.
VSLI-NCALC. SFT-SLI FRM.

CLY-LT-MGY. GYBRN. SLTY. TR
PYR. VSLI. CALC. HYDRD. SDY
IP. CHY. SFT.

8-12-93
LS-LTGY. LTCYBRN. SLTY.
TR. PYR. ARG. FRM.

CLY-LTGY. LTCYBRN. SLTY.
TR. PYR. CALC-VCALC. CHY.
STKY. SFT.

SLTST-LT-MGY. ARG. SFT. SDY. TR
CARD. SPECS. SLI. CALC. SFT.

TUF-LTGY. WH. SLTY. IP. ARG.
ALT. TO BENT. IP. OCC. WXY
TEXT. SFT.

SD-CLR. LT-BKCY. WF-FGR. OCC. MGR.
SP. NG. W-PORID. SLTST/CLY. MTR.
TR. PYR. NSOPC.

MW 10.0 VIS 55
TYPE 22/48
P. 3.0 FR 8.3 CL 17500

CLY-LT-MGY. GYBRN. SLI. CALC.
SLTY-SDY. OCC. BENT. CHY. SFT.

SD-LTGY. CLR. TR. BRN. VFGR.

5800
5850
5900
5950
6000
6050
6100

10% LITH FRAGS & HRDL
TR PYR NSOFC
WV 10.0 VIS 55
15.0 FR R. 3 CL. 11500
CLY-LT-MGY. CYBRN. SLI. CALC.
SLTY-SDY. OCC BENT. GMY. SFT
SD-LTGY. CLR. TR BRN. VFGR.
TR F-MGR. SBANG-ANG. M-W
BRTO. CLY/SLTST. MIX. TR
TUF. TR MICA. N-SLI. CALC.
60% QTZ. 20% LITH FRAGS. 10%
HRDL. UNCONS. NSOFC
CLY-LT-MGY. SLTY-SDY. TR
PYR. N-SLI. CALC. OCC TUF
STRGRS. GMY. SFT
SVY @ 5983' 1.24 Deg.
TUFF. W/ TR. YEL. ORNG. BLK. SLTY
IP. CHKY. W/ IP. NICKL. TR
TRPH. STN. TR DUL. ORNG. W/ TR FLOR.
SFT-MFRK
START 10' SAMPLE INTERVAL
SLTST-MGY. MGYBRN. ANORPH. FLKY. IP.
ARG. CLY. MTRX. MCALC. TR VFGR
SD INCL. GMY. SET + HYDRID
SD/SS-CLR. TRANSL. BLK. W/ CY.
SH. SLTY-VFGR. SBANG-RND. PRED.
SERND. PSRT. PRED. UNCONS. ARNBT
CLY. MTRX. MAT. TR. CHKY. W/ CASE
OR ALTRD. CLY. MTRX. TR. CARB.
SPEC. 80% QTZ. 20% BLK + CY
LITH FRAGS. NSOFC
TR VFGR. DKGY. RND. LITH. GRS

CG 44



6150
6200
6250
6300
6350
6400
6500

CG 82

CG 71

CG 87

CG 68

NOTE:
C2

NOTE:
C2

SLTST-DKGYBRN. SLEY. CALC. TR
VFGR. SD INCL. + INTBDS. PRED
QTZ INCL. TR. GARD FLKS. VARG.
SFT-FRM + BRIT.

SLTST-A/A BOWNG FRML. N-VCALC.
TR. WH. CALC. CLY. STRNGRS. OR
INTBDS. OCC. F-MER. SRND. QTZ.
INCL. VARG. CRDNG. TO. CLYST. IP.
SFT-FRM

SD-CLR. CY. BLK. CRN. SLT-VFGR.
TR. OCC. MGR. SBANG-RND. PRED
SBAND. E-MERT. UNCONS. ARNDT.
CLY. MIXX. INTBD. OR. INCL. IN
SLTST + CLYST. 80-90% QTZ.
10-20% LITH. GRS. NSOFC

SVY @ 6343' 1.42 Dwg.
FR. DISSEN. MECHLN. PFR. IN. SMPL.

CLYST-TN. LT-MGYBRN. AMORPH.
SLT-MCALC. SLTY. AREN. TR-10%
VFGR. QTZ. SD. INCL. STKY. GMY.
VSFT + VHYORID

SLTST-LT-MGY. CYBRN. TN. ARG.
AREN. VSLLI. CALC. TR. PFR. SFT.
GMY.

SD-CLR. LTGY. OCC. BLK-BRN.
VFGR. OCC. F-ER. ANG-SBAND.
N. SRTO. PRED. QTZ. OCC. LITH.
FRAGS. CLY/SLTST. HTX. W. PR.

SLTST-1-T-MCY, CYORN, TN, ARG
AREN, VSLI, CALC, IN, PYR, SFT,
GNY

NOTE SCALE CHG
NRM, ROP
1200 800 0



SD-CLR, LTGY, OCC BLK-BRN,
VFGR, OCC F GR, ANG-SBANG,
M SRTD, PRED QTZ, OCC LITH
FRAGS, CLY/SLTST MTRX W/ PR
POR, <5% MUL, ORG-ORG FLUOR,
TR YEL/GN FLUOR, FR YEL CUT
FLUOR IP, N STN, N ODR

CLY-LT-MGY, LTGYBRN, SLTY-
VSLTY, SLI-VSDY, OCC CARB
SPECS, SLI-M CALC, GNY, SFT

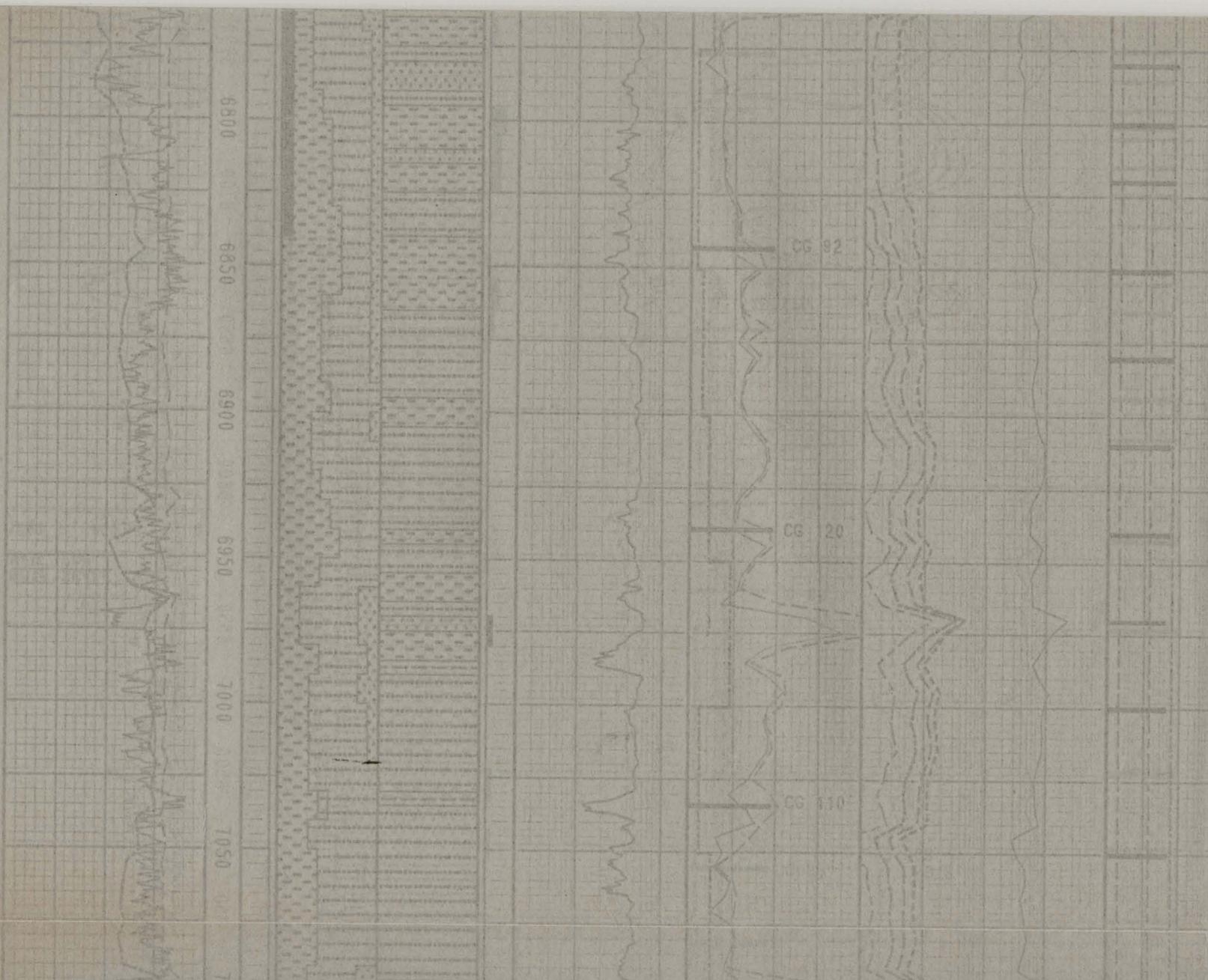
SVY @ 6547' 1.42 Deg.
HW 10.84 VIS 59
PV/YP 22/28
FL 2.7 PH 8.1 CL 17000

8-13-83
NB 5 12.25" DS-40H
2-14 3-13 JETS
TG 142

SD-CLR IN, LTGY, BLK IP, SLT-VGR,
SBANG-SBRNG, PRED SBANG, F-NSRT,
VARG-UNCONS, ASNDT, CLY MTRX
MAT 80-90% QTZ, 10-20% LITH,
W-BRI GRNOLD FLOR IN 50% OF
SMPL SURFACE FAIR, SMO-MKY
YEL CT FLOR, GD YEL WH RESID
CT FLOR, RING, OIL, ODR,
NO VIS STN

SD-OKGY, BLK, CLR, TRANSL, MGY,
VF-MGR, PRED MGR, OCC C-VGR,
SBANG-MIND, PRED SBANG, F-NSRT,
ARG-UNCONS, SLTY, CLY MTRX
MAT 60-70% CHL + LITH GAS
SD-40% CLR-FRSTO QTZ, TR PYR,
SD-70% W-BRI GRNOLD SURFACE
SMPL FLOR, GD FAST STRMG
MKY WHYEL CT FLOR, GD WHYEL
RESID CT FLOR, RINGS, OIL, ODR,
SLT TR, TW-LTRB, STN, DRY IP.

8-14-83 NCB1 AC412 TFA 17
CORE #1 6729-6732 NO REC.
TG 88
RRB 5 DS-40H
2-14 3-13 JETS
SD-OKGY, BLK-BRN, LTGY, CLR,
F-MGR, SBANG-ANG, W-PR



SRTD. TR PYR. PRED. CNT. &
 LITH. FRACS. 30-40% DTZ.
 SLTY. CLY. MTK. UNCONS. 40%
 MOD. YEL. GRN. FLUR. CO. M.L.K.Y.
 CUT. FLUR. YEL. GLO. RESID. CT
 SLTST-LT-MGY. ARG. SLI-VSDY.
 TR. THN. COAL. STRGRS. TR.
 PYR. SLI. CALC. SFT.

CLY-LTGY. VSLTY. SDY. STRGRS.
 SLI. CALC. TR. TN-BRN. FOS.
 FRACS. W/ ORG. MIN. FLUR.
 TR. BITMN. SFT.

MW 10.1+ VIS 80 FIL 3.0
 PV/YP 24/84 PH B.9
 CL 17000

SLTST-LTGY-LTGYBRN. 90Y.
 ARG. SLI. CALC. TR. TN-BRN.
 FOS. FRACS. W/ DUL. ORG.
 MIN. FLUR. TR. BITMN. SFT.
 SLTST-LTGY-TN. MOTT. IP.
 TR. TN-BRN. FOS. MAT. W/
 DUL. MOD. ORG. FLUR. 50Y.
 ARG. SLI. CALC. SFT.

8-15-82

SVT # 6240' 0.89Deg.
 CLY-LT-MGY. GYBRN. SLTY.
 F-M. GR. FLTG. SD. CRS.
 OCC. TN-BRN. FOS. FRACS.
 W/ DUL. ORG. MIN. FLUR.
 SLI. CALC. SFT.

SD-LT-OKGY. BLK. CLR. F-M.
 GR. SB. ANG-ANG. M-PR.
 SRTD. PRED. UNCON. TR. W/
 TT. CALC. CNT. 45% OF. SAMP.
 SURF. W/ YELCN. FLUR.
 FR. STRMG. YEL. CT. IP.

SH-MGY. SLTY. OCC. 50Y.
 CALC-V-CALC. HD.

SLTST-LTGY. LTGYBRN. ARG. SLI-
 MOD. CALC. OCC. TN-BRN. FOS.
 FRACS. W/ DUL. ORG. MIN. FLUR.
 TR. CARB. SPECS. SFT.

WHEN QUANTIFIED IN CORE LOGS
FRAGS W/ DUL ORG MIN FLOR.
TR CARB SPECS. SFT

7100
7150
7200
7250
7300
7350

CG 82

CG 124

SD-M DICY. CLN. TRNSL. WH. F-CGR.
PRED CGR. ANG-SBRNG. PR. SRTD.
UNCONS. TR. CALC. CMT. IP. 60%
LITH. FRAGTS. 20% QZ. 10% DUL.
ORG. MIN. FLOR. 10% RT. YEL.
WH. SAMP. FLOR. N. RESID. CT.
N. STN. SLTY. CLY. MIX.
CLY. LT-MGY. TN. SLTY-SDY.
MOTT. IP. SLI. CALC-CALC.
TR. FOS. SFT.

ABNDT. CALC. FRAGS.
SLTST-LT-MBRN. TN. BLKY. AMORPH.
IP. CALC. OCC. VCALC. CMTD.
STRNGRS. ABNDT. F-MGR. SD. INCL.
CRDNG. TO. CLYST. IP. SFT-HD +
BRIT.

SS-BLK. CY. S4P. WH. F-VCGR. PRED.
MGR. ANG-SBRND. PRED. SBANG.
PSRT. MCMT. UNCONS. IP. CALC.
20% DUL. ORNG. MIN. FLOR. NSOC.

SLTST-LT-MBRN. TN. DKBRN. + WH.
MOTT. IP. BLKY. UNCONS. VCMT. IP.
VCALC. ARG. TR-10% VF-FGR. SD.
INCL. CRDNG. TO. SH. IP. TN. CARB.
SPECS. TR. MVEL. CALC. STRNGRS.
TR. DUL. ORNG. MIN. FLOR. ONLY. IP.
HYDRD-HD + BRIT.

CLYST. TN. LTGYBRN. AMORPH. TN.
SAPL. AREN. MCALC. SLTY. TR. VF-
OCC. CGR. SD. INCL. PRDG. INBD.
W/ SD. STRNGRS. PRDG. CRDNG. TO.
HYDRD. SH. IP. CMMY. STKY. VSET +
HYDRD.



TR PYR NODS IN CLYST + SLTST
SVY @ 2418' @ 570deg.

SLTST-TN. LTGYBRN. AMORPH-
UNCONS. ARG PROB CLY MTRX
MAT. CALC. OCC. YCALC STRONG
OR-10% VFGR SO INCL. CRDNG
TO CLYST. VSFT + VHYDRD

RESUME 30' SAMPLE INTERVAL

SLTST-LT-HBRN. TN. AMORPH-PLTY
IP. ARG. MCALC. BCMNG FRMR. TR
VFGR SO ENCL. PRED. SBND. QTZ.
SLY TR PYR NODS. VSFT + HYDRD-
FRM + DRIT

CLYST-TN. LTGYBRN. AMORPH IN
SWPL. SLI-MCALC. ABEN. 10% VFGR
QTZ SO INCL. CRDNG TO SLTST
IP. CMY. STRY. VSFT + VHYDRD

SO-CLR. W/LTGY. OCC. HBR. VF-HGR.
PRED. VFGR. SBAND. VBRND. PRED.
SBAND. PSRT. UNCONS. INCL. IN
CLYST + SLTST. PRED. QTZ. TR
LITH + CARB FRAGS. NSOFC

8-16-82
STC 625

NO. 18.0 VLS 33
PV/VF 23/30 PH 8.8
FIL 2.5 CL 17300
SS-LTGY. VF-FGR SBAND-
SBAND. MSRTD. GRDG TO
SLTST IP. CALC. CMT. TT.
DUL. ORG. MTR. FLUOR. NCT.

8-18-83
STG 625

10.0 715 20
PV/YF 25/30 PH 8.8
FIL 2.8 CL 17500
SS-LTCY. VF-FGR SBANG-
SBRND MSRTD. GRDG TO
SLTST IP. CALC GMT. TT.
DUL ORG MIN FLUOR. NCT.
NSTN

LS-MCY TN. BRN. MI. MICR-FXLN.
VFOS IP. CHLKY IP. FRED
VDNS. OCC SDY. SFT-HO
DUL-BRT ORG/PNK MIN
FLUOR. N STR. N ODR
SVT @ 7790' .0420g

SLTST-LT-MCY. PRED. ARG. SDY
IP. SLT. CALC-CALC. TR. CARB
SPEGS. ABVT. FOS. SHEL. FRAGS.
SFT. PRED. UNCON

SLTST-LTGY. TN. CALC. VSDY
IP. OCC. FOS. FRAC. TR. CARB
SPEC. ARG. SFT

ABNDT CLAY BALLS OVER SHRS

CLYST-H-OKCYBRN. MBRN. MI + TN
MOTT IP. AMORPH. HALLED. AREN.
VSLTY IP. INTBD W/ VFGR SD +
INCL. CALC. TR. VCALC. STRNGRS.
GHWY. STKY. SFT

SD/SS-SY. MI. CLR. BCK. VF-FGR

7700
7750
7800
7850
7900
7950
8000

NOTR SCALE CHG:
TOTAL GAS

CG 220

GAS PEAKS
DUE TO



OCC MGR. SBAND PERT. UNCONS-
 ABNDT CLY MTRX. SMC WH ALTRD
 CLY OR CALC PNT. CRDNG TO
 SLTST IP. VS LI TR WGRN-YEL
 SNPL FLOR. CO FAST STRNG WH CT
 FLOR. IP. CO WH RESID CT FLOR
 NO STR. NO ODR

TR DISSEM PYR IN SLTST
 SVY @ 8180' 0.460eg.

SD-CLR. LTGY. WH TRANSL. TR LTGRX.
 W-FGR. OCC W-CGR QTZ. SBAND-
 RND. PRED SBAND. PERT. UNCONS
 IN SNPL. PROB INCL. + STRNGRS
 IN SLT + CLY. SLT CALC. CARR
 PRNGS. TR PYR. MORT-DUL. YEL WH
 FLOR. IN 5X OF SNPL. CO FAST
 STRNG WH CT FLOR. FR WH
 RESID CT FLOR. NO STR. NO ODR

SD/SLTST-A/A. TR CALC. FRAC. FILL
 DUL. WH EL. FLOR. IN SP. OF SNPL.
 VPR. VS LO. FNT. WH CT. FLOR.
 NO RESID. CT FLOR. NO VIS. STA.
 VNT ODR

IN SNPL. VARG. CRDNG. IN V-GR
 SD IP. TR MGR. SD. SLT. CALC.
 TR CARR. SPECS. 40X. DUL. WH
 CRDNG. SNPL. FLOR. CO. WH. RES.

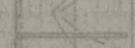
8350
8400
8450
8500
8550
8600



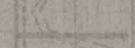
CG 288



CG 225



CG 225



CG 214

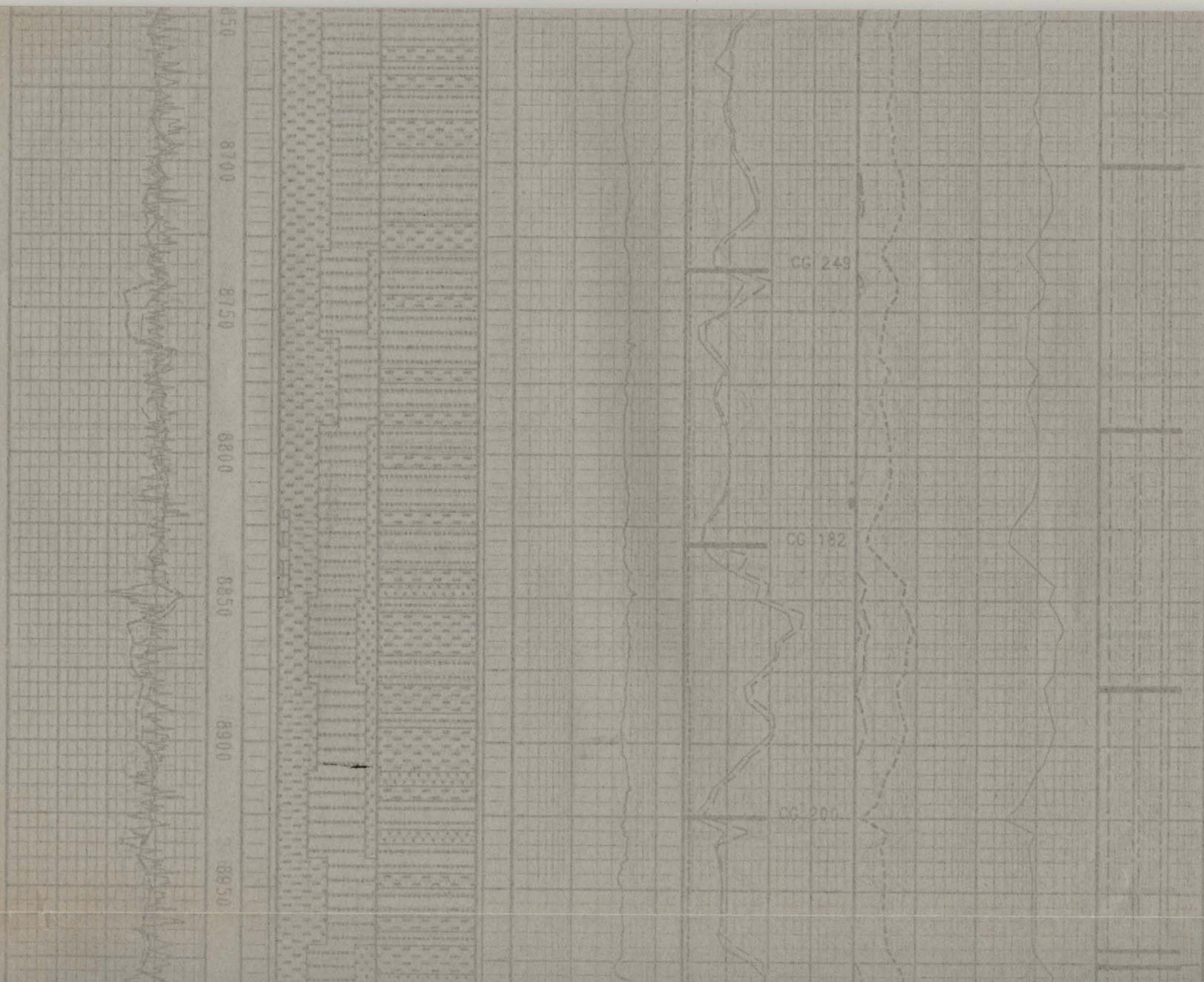
SLTST-IN. LTGYBRN. WH. IP. VGRD
IN SWPL. VARG. GRDNG TO VGRD
SD. IP. TR. WCR. SD. SLI. CALC.
TR. CARB. SPECS. 10% DOL. WH.
GRNCL. SWPL. FLOR. CD. WH. FLSH.
CT. FLOR. CD. STRNGS. WHYEL. CT.
FLOR. FR. PR. RESID. CT. FLOR.
TR. LTBRN. DOL. IN. SWPL. FMT.
OODR.

SVY @ 8450' 9.53Degs.
SLTST-IN. LTGYBRN. AMORPH. IN.
SWPL. VARG. ABNDT. CLY. MTRX.
MAT. GRDNG TO CLYST. SLI.
CALC. 10% WGR. QTZ. SD. INCL.
5% DOL. LTGRN. SWPL. FLOR. PR. FR.
WHYEL. CT. FLOR. BR. RESID. CT.
FLOR. NO VIS. STN. NO OODR.

MW 10.2 IN.
CLYST-IN. AMORPH. IN. SWPL. SLTY.
AREN. SLI. MCALC. GMMY. STKY.
VDFT + VHYDRD.

SLTST-IN. LTGYBRN. WH. + CT. VDTT.
IF. AMORPH-BLKY. ONLY. IP. VARG.
SLI. MCALC. GRDNG TO VGRD. SD.
IP. TR. CALC. ONTO. STRNGS. TR.
CALC. XLS. SFT + HYDRD-MCT +
WFRM.

CALC. FRAC. FILL. BRN. YEL. XLN.



TR PYR MOOS TR LRG XLS

CLYST-TN VLTGYBRN AMORPH IN

SLTST-TN LT-NORN TH + MI MOTT
 IP VARG SLI-NCALC OCC CALC
 STRGRS CNDNG TO CLYST TR
 VFGR QTZ SD GRS TR PYR NSOFC

SVY @ 8735' @ 700gpa.

CLYST-TN VLTGYBRN AMORPH IN
 SMPLE AREN IP VSLTY PROB
 LYRD W/ SLTST TR VFGR SD
 INCL STKY OHY VSTF + HYDRTO

SD-CLR LT-ONGY BLK VF-FGR
 PRED VFGR SBANG MSRTD
 FLTG IN SLTY CLY MTX
 CALC IP ABNT FOSS FRACS
 DUL ORG MIN FLUOR IP
 NSTN. NCT

SLTST-LTGY LTOYBRN MOTT SLI
 CALC OCC FOS FRACS ARG
 SDY IP TR CARB SPECS OCC
 W/ CLAY STRGRS TR PYR
 SFT

SS-LT-MCY W/ VFGR SBANG

0
8950
9000
9050
9100
9150
9200
9250



CG-200
75
MAX GAS
CG-241

SLTST-LTGY, LTGYBRN, MOTT, SLI
CALC, OCC, FOS, FRAGS, ARG,
SDY, IP, TR, CARB, SPECS, OCC,
WH, CHLKY, STRGRS, TR, PYR,
SFT.

SS-LT-MCY, WH, VFGR, SBANG,
CHLKY, CALC, CMT, IP, YSLTY,
ARG, N, VIS, POR, TR, CUL, ORG,
MEN, FLUOR, NSTN, NCT.

CLY-LTGY, TN, LTGYBRN, SLTY,
SLI, CALC, OCC, WH, CHLKY,
STRGRS, OCC, SDY, STRGRS,
TR, FOS, SFT, CMT.

SLTST-LTGY, TN, TR, WH, SLI-VARG,
SLI, CALC, W/, OCC, WH, CHLKY,
STRGRS, INTRSD, W/, CLY, & SD,
STRGRS, TR, FOS, FRAGS, SFT.

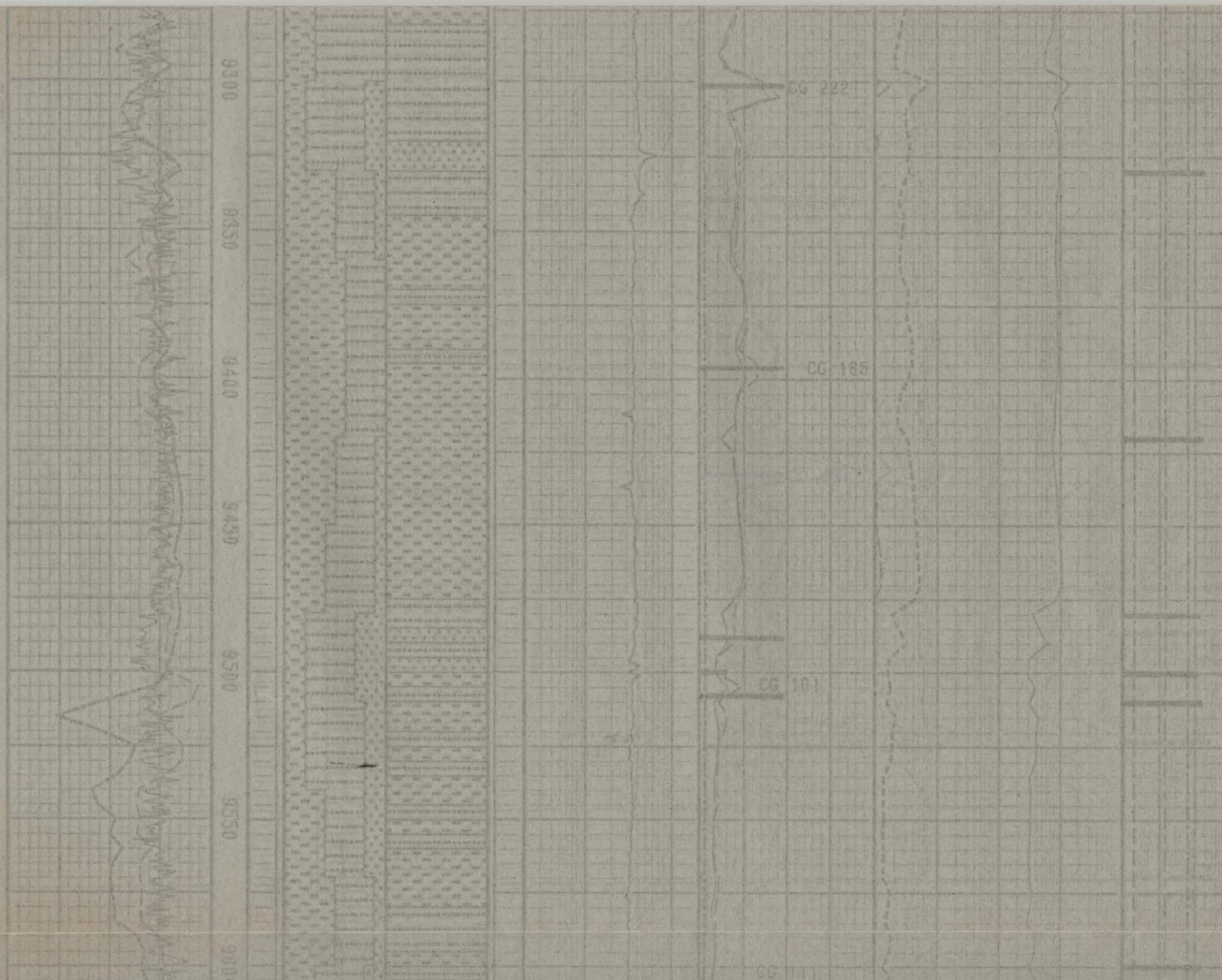
SLTST-LTGY, TN, OCC, MGY, WH,
MOTT, IP, N-SLI, CALC, TR, FOS,
FRAGS, VFGR, SDY, STRGRS,
SLI-VARG, TR, PYR, N, FLUOR,
N, STN, SFT.

CLY-LTGY, TN, SDY, GRDG TO
SLTST, SLI, CALC, SFT.

SVY @ #207* 0.87Degs.

SLTST-LT-MCY, OCC, WH &
CHLKY, MOTT, ARG, OCC,
CARB, SPECS, SDY, STRGRS,
TR, FOS, FRAGS, NSOFC.

CLY-LT-MCY, GYBRN, OCC, WH



SLTY-SDY, VSLI CALC TR
CALC FRAC FIL, SFT, GRV

SS-CLR, WH, LTGY, BLK, TN, VF-
FGR, FRED, VFGR, SBANG, M-FR
SFTD, SLI-YSLTY, CRDG TO
SLTST, N-SLT CALC, FRI,
NSOFC

CLY-LT-MCY, CYBRN, OCC WH MOTT,
SLTY-SDY, VSLI CALC, CRONG TO
SLTST, SLI CALC FRAC FIL, SFT.

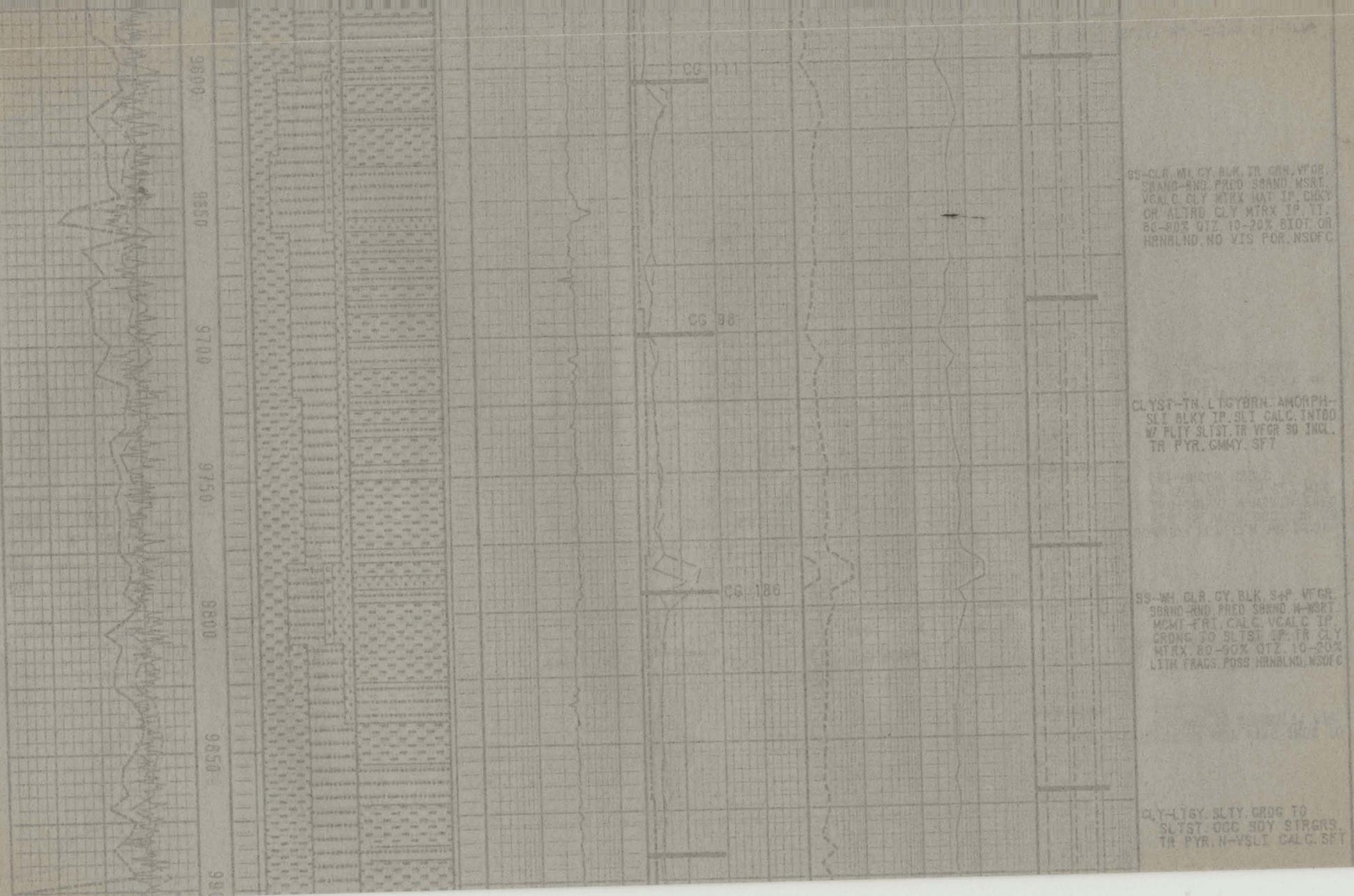
SLTST-LT-MCY, OCC WH + CHKY
MOTT, VARG, OCC CARB
SPECS, OCC SD STRNGRS, TR
FOSS FRACS, NSOFC

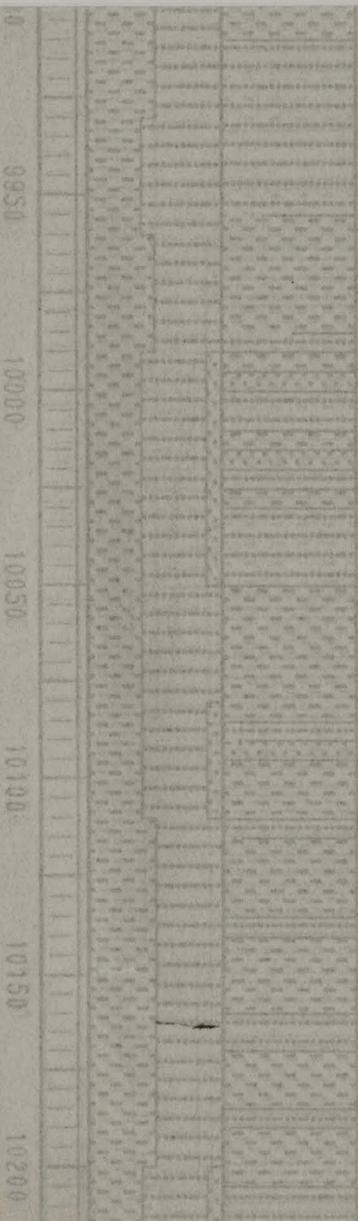
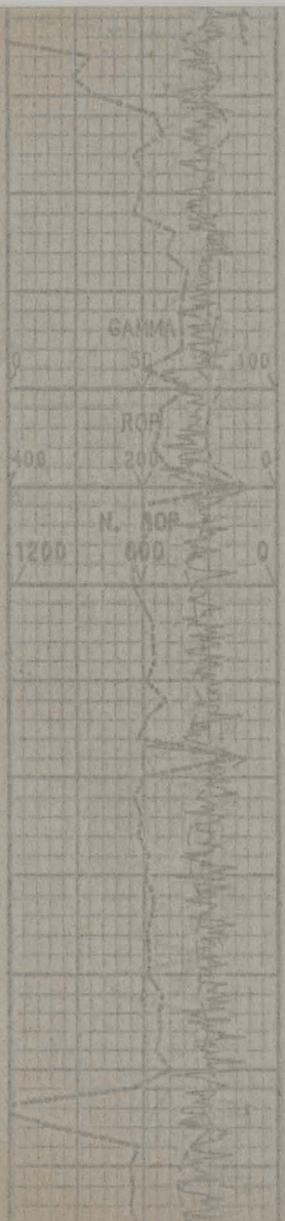
MW 10.44 VIS 70 FXL 2.9
PV/YF 30/40 PH 2.3 CL 17000
8-17-83

SVY @ 9488' 1.25Degs.

8-18-83
NB @ 12.25" DS40H
5-15 JETS
TG 1541

SLTST-M-OKBRN, WH MOTT IP, BLKY
IP, PLY IP, ARG, CRONG TO
CLYST IP, SLI CALC TR, PYR,
TR VFGR, Q12 SD INCL, SFT-
MFRM + BRIT





9950
 10000
 10050
 10100
 10150
 10200

SLTST-LT-MCY VARS GRDS TO
 CLY OCC SD STRGRS TH PYR.
 NCALC. SFT

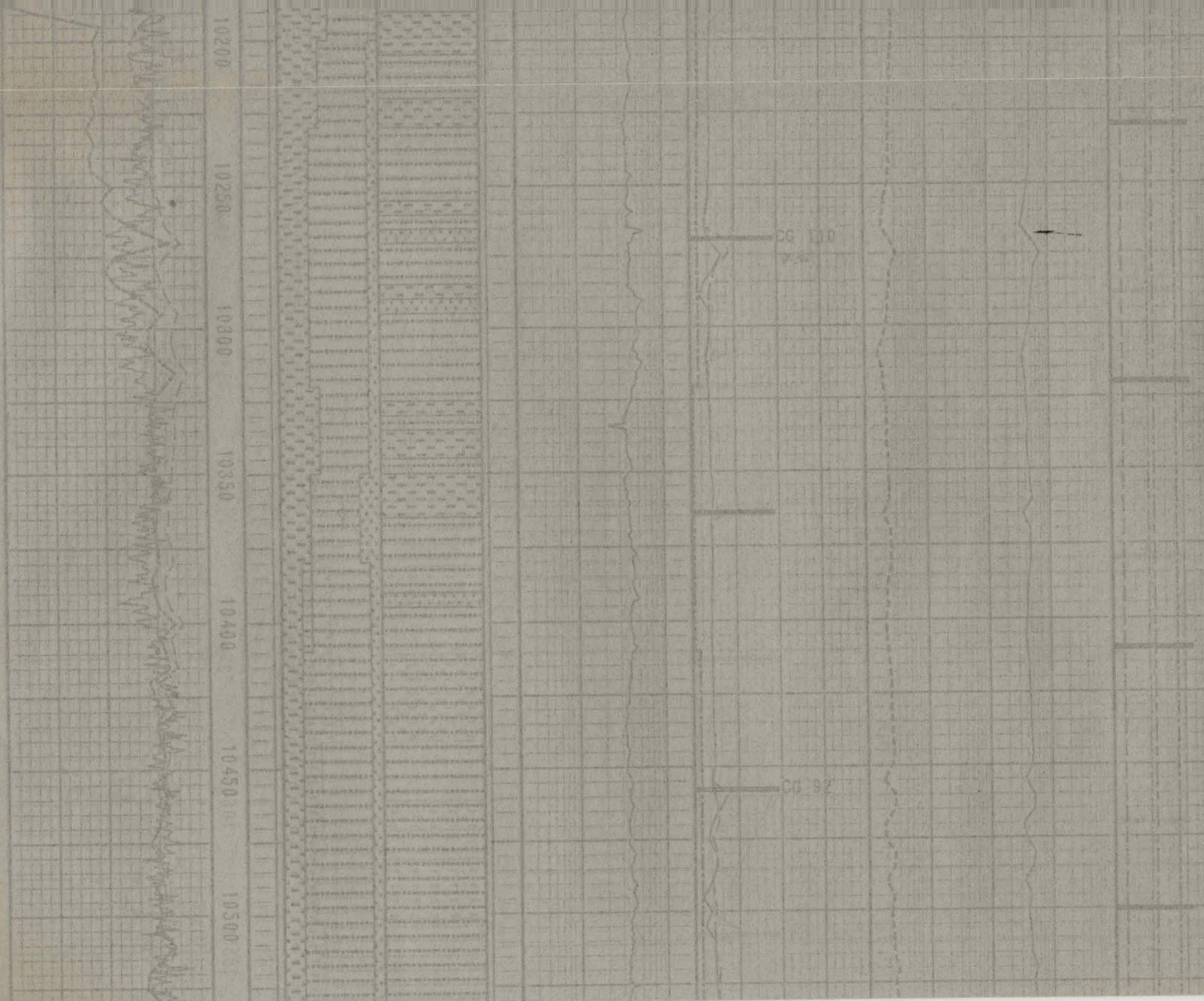
SVY w 9864° 1.43Degs.

SDASS-LTGY CLR WH DKGY-
 BLK TN VFGR OCC FGR SB
 ANG-SBRND. M-WSRTO. PRED
 W/ SLI CALC WH CLY MIX.
 FRI-UNCON. NSOFC

CLY-LTGY LTGYBRN SLTY
 OCC MOTT W/ CHLKY WH.
 SDY IP. N-VSLI CALC.
 SFT. CHY.

SLTST-LTGY-LTGYBRN TN WH
 MOTT IP. ARG. VV FLTG SD
 GR. NCALC. SFT. UNCONS.

SLTST-MCY-GYBRN SLI-VARG
 CONSOL. IP. SLI-VSDY SFT.



SLTST-MGY-GYBRN.SLI-VARG
 CONSOL IP.SLI-VSDY.SFT

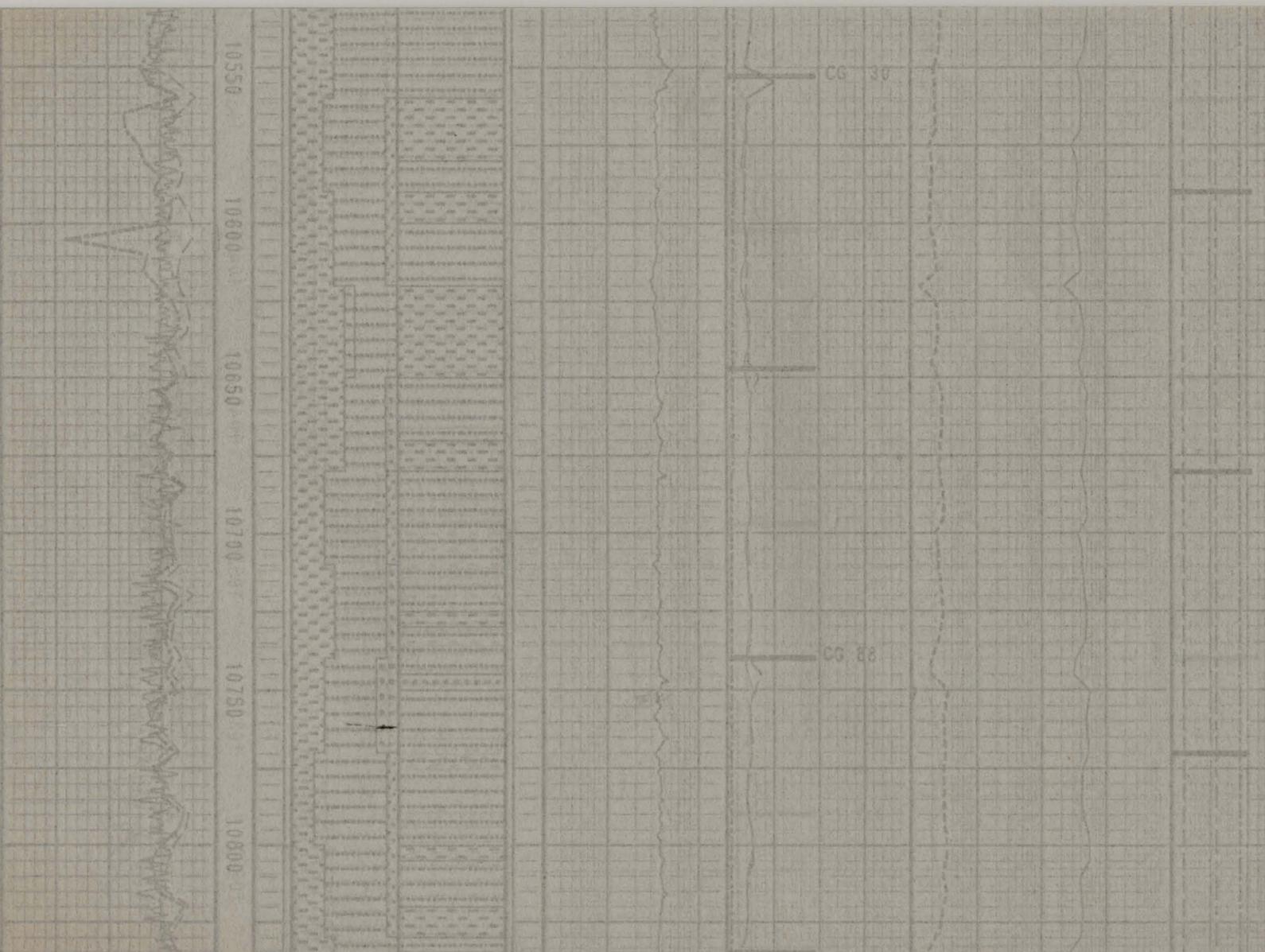
SVY @ 10280' 0.87Deg,
 SD288-WILT-MGY.VFGR OCC
 FOR SBANG-SBRND.M-WRTO
 ABRT W/ CLY NTK OCC CALC
 XLS.TR CARB SPECS.FRI-
 UNCONS.NSOFC

SLTST-LTGY-GYBRN.LTBRN.W/
 STRGRS.SLI-VARG.SDY IP W/
 SDY STRGRS.TR CARB PRIGS
 & SPECS.W-VSLI CALC.TR
 CALC XLS.SFT.BONG INCRLY
 CONSOL

6-19-93

SLTST-LT-MGY.GYBRN.SDY
 W/ OCC THN SS STRGRS.
 SLI CALC IP.TR CARB
 SPECS INCR CONSOL.TR
 CALC XLS.SFT-SLI FRM

SLTST-LT-MGYBRN.LT-MGY
 SLI CALC IP.ARC SDY W/
 OCC THN SS STRGRS OCC
 CARB SPECS.TR CARB
 PRIGS CONSOL IP.SFT-
 FRM



9TC 883
 CLYST-TN. VLTRN. AMORPH-SLI
 BLKY IP SLI CALC. ARG IP.
 GRDNG TO SH IP. INTBD W/
 PLTY SLTST. VSFT + HYDRD

SLTST-MBRN. RDCYBRN. BLKY. ARG.
 UNCONS IP. NCALC. CLY. MTRX.
 MIC MICA. TR. VFGR. SD. TR. CARB
 SPECS. SFT-FRM

RAISE MW TO 10.6

ABNDT. WH. CHKY. CALC. STRGRS
 SLTST-TN. LT-MCY. OCC. WH.
 CHKY. STRGRS. OCC. THN. SS
 STRGRS. TR. MICA. TR. CARB
 SPECS. ARG. IP. SFT-SLI. FRM

800
10850
10900
10950
11000
11050
11100

CLYST-TR LTRN ANORPH-BLKY.
SLI CALC. VANEM INTBD W/
PLTY SLTST + CARB SPECS
IP. CMMY. VSFT + HYDRD.

SLTST-M-DKBRN. BLKY. PLTY.
ARG. SLI CALC. CLY MTRX.
INTBD W/CARB SPECS. SFT-
FRM.
RAISE MW TO 10.7

CLY-LT-MGY. GYBRN. SLTY-SLI
SDY. NCALC. OCC THN CALC
SLTST & SS STRGRS. TR FOS
FRAGS. PRED HYDRATED. SFT

SH-DKGY. SLTY. OCC CARB SPECS.
MCR MICA. CARB. SLI CALC.
SB FIS. SFT-SLI FRM

CLY-LT-MGYBRN. SLI-VSLTY.
OCC THN SDY STRGRS. VSLI
CALC IF. TR FOS FRAGS. OCC
CARB SPECS. HYDRD. CMMY.
SFT

MW 10.7+ VIS SS
PV/VP 27/84 PH 8.6
FIL 3.1 CL 17000
SLTST-LT-MGY. OCC DKGY. GYBRN.
ARG. TR TRN SS STRGRS. M-SLI
CALC. OCC CARB SPECS. OCC
MCR MICA. TR PYR. SFT-FRM

SH-M-DKGY. SLTY-SDY. OCC
MCR MICA. SLI CARB W/
OCC CARB SPEC. SB FIS-
BLKY. FRM-MWD

T.D. 11125"
C.D. FOR E-LOGS

CASING PROGRAM	30	inch at	301	ft
	20	inch at	1017	ft
	13 3/8	inch at	3978	ft
		inch at		ft
		inch at		ft

DRILLING MUD RECORD

COMPANY ARCO ALASKA INC.
 WELL KUVLUM #2
 CONTRACTOR CANADIAN MARINE DRILLING
 MUD COMPANY M & I

FIELD/BLOCK OCS BLK 672 NR6-4
 LOCATION BEAUFORT SEA
 STATE ALASKA
 SPUD DATE 28 JUL 93

DATE	DEPTH ft	WEIGHT lb/gal	VIS sec	PV cp	YP lb/hf2	GELS 10 sec/ 10 min	FLTR ml/30m	HTHP /deg F	CAKE 1/32	SOL %	OIL %	WATER %	SD %	CEC meq/hg	pH	PM	Pf/Mf	Cl- ppm	CA ppm
07-29-93	1030	8.6	300	48	56	38/75													
07-29-93	1030	8.6	100																
07-30-93	1030	8.6																	
07-31-93	1030	9.8	90	28	19	4/8	5	-	1	6.3	0	93.6	0	NA	9.5	1.8	.5/1.8	17500	1560
08-01-93	1040	9.8	50	19	26	5/8	8	-	1	5.6	0	94.4	0	5	9.9	2.2	.1/2.9	17000	400
08-02-93	1956	9.8	50	24	21	4/5	4.6	-	1	6.3	0	93.7	0	0	9.6	1.3	.8/1.7	16000	840
08-03-93	3300	9.8	54	27	23	3/5	4.0	-	1	8	0	92	0	3.25	9.5	1.1	.6/1.5	16000	1200
08-04-93	4005	9.8	52	24	22	3/5	4.2	-	1	7.8	0	92.2	1.25	3.75	9.5	1.8	.8/1.9	16000	800
08-05-93	4005	9.8	52	24	22	3/5	3.8	-	1	7.8	0	92.2	1.25	3.75	9.5	1.8	.8/1.9	16000	200
08-06-93	2240	9.8	65	26	30	3/6	4.2	-	1	8.3	0	91.7	3.0	5.0	9.2	1.3	.5/1.6	16000	600
08-07-93	4005	9.8	52	24	26	3/4	5.2	-	1	8.3	0	91.7	1.5	3.75	9.3	1.2	.4/1.6	16000	680
08-08-93	4005	9.8	50	23	21	3/4	3.8	-	1	8.3	0	91.7	1.75	3.5	9.4	1.2	.4/1.4	16000	640
08-09-93	4005	9.8	51	15	17	3/4	3.0	-	1	8	0	92	.8	3.5	9.2	1.0	.3/1.5	16000	600
08-10-93	4900	9.8+	58	19	19	3/4	3.2	-	1	8	0	92	1.5	3.0	9.9	1.0	.3/1.6	17000	860
08-11-93	5645	10.0	55	20	23	3/6	3.0	-	1	8.5	0	91.5	1.0	4.5	9.3	.7	.15/1.4	17500	680
08-12-93	6593	10.0+	59	22	28	5/9	2.7	-	1	8.5	0	91.5	1.0	4.5	9.1	.5	.1/1.3	17000	920
08-13-93	6729	10.0	79	26	32	5/10	2.6	6.4 @150	1	9	.5	90.5	1.25	4.5	9.0	.5	.1/1.3	17500	1040
08-14-93	6768	10.1	69	24	34	5/12	3.0	6.8	1	11	T	89	.75	5.5	8.9	.3	.1/1.3	17000	920
08-15-93	7698	10.0	59	25	30	3/8	2.8	6.0	1	9	T	91	1.0	6.0	8.6	.3	.1/1.3	17500	880
08-16-93	9500	10.4+	70	30	40	5/15	2.9	6.8	1	10.5	T	89.5	1.25	6.5	8.8	.3	.1/1.4	17000	920
08-17-93	9500	10.4	68	23	35	4/7	.3	6.8	1	10	T	90	.75	5.5	8.8	.3	.1/1.5	17500	920
08-18-93	10270	10.5	64	26	34	4/12	3.4	6.8	1	10	TR	90	1.0	6.5	8.6	.45	.25/1/5	17000	920
08-19-93	11125	10.7	58	27	34	3/9	3.1	6.0	1	11.5	T	88.5	1.0	6.5	8.6	.3	.2/1.5	17000	960
08-20-93	11125	10.8	56	28	36	3/13	3.0	6.2	1	11.5	TR	88.5	.75	7.0	8.5	.3	.15/1.4	17000	920
08-21-93	11125	10.9	68	28	37	3/12	2.6	7.0	1	12	T	88	1.0	7.0	8.5	.3	.15/1.4	17000	840

8

CASING PROGRAM	30	inch at	309	ft
	20	inch at	1022	ft
	13 3/8	inch at	3681	ft
		inch at		ft
		inch at		ft

DRILLING MUD RECORD

COMPANY ARCO ALASKA, INC.
 WELL OCS-Y-0866 NO. 2 KUVLUM # 3
 CONTRACTOR CANMAR
 MUD COMPANY M & I

FIELD/BLOCK NR6-4 BLOCK 673
 LOCATION OFFSHORE - BEAUFORT SEA
 STATE ALASKA
 SPUD DATE 9-9-93

DATE	DEPTH	WEIGHT	VIS	PV	YP	GELS	FLTR	HTHP	CAKE	SOL	OIL	WATER	SD	CEC	pH	PM	Pf/Mf	Cl-	CA
1993	ft	lb/gal	sec	cp	lb/hf2	10 sec/ 10 min	ml/30m	/deg F	1/32	%	%	%	%	meq/hg				ppm	ppm
09-09-93	309	8.8	70	16	16	12/28	-	-	-	-	-	-	-	-	9.0	-	.15/.3	650	400
09-10-93	10040	9.6	58	16	18	6/14	13	-	1	-	-	-	TR	-	9.5	.4	.2/.5	14000	560
09-11-93	1040	9.6	58	16	18	6/14	13.0	-	1	-	-	-	TR	-	9.5	.4	.2/.5	14000	560
09-12-93	1040	9.8	53	18	19	4/4	4.1	-	1	6	0	94	0	1.5	9.0	.4	.2/.8	18000	1800
09-13-93	1284	9.7+	43	16	18	3/3	5.1	-	1	6.5	0	93.5	.75	1.5	10.0	1.5	.4/1.3	17400	1560
09-14-93	2702	9.7+	72	29	35	4/5	3.2	-	1	7	0	93	2	3.5	10.1	1.3	1.1/2.7	17300	880
09-15-93	3705	9.9	82	37	44	6/9	2.2	-	1	7	0	93	1.75	4.5	9.8	1.2	.9/2.3	17100	680
09-16-93	3705	10.1	74	31	39	6/9	2.4	-	1	8.5	0	91.5	2	4.5	9.8	1.2	.9/2.4	17000	720
09-17-93	3705	10.0	54	21	26	3/4	2.8	-	1	8	0	92	.5	4.0	9.5	.5	.5/1.3	17000	480
09-18-93	2900	9.9	60	29	34	4/6	2.0	-	1	7.5	0	92.5	1.75	3.75	9.7	.5	.5/1.5	17000	240
09-19-93	3705	9.8+	80	30	42	5/9	3.6	-	1	7.5	0	92.5	1.75	4.0	9.5	.6	.5/2.5	16800	100
09-20-93	3705	9.9	62	22	21	3/6	2.4	6.4	1	7.5	0	92.5	1.5	4.0	9.9	.6	.6/1.9	17000	320
09-21-93	3705	9.8	58	19	20	3/4	3.4	7.8	1	7.2	-	92.8	.75	3.75	9.0	.6	.25/1.5	17000	360
09-22-93	3705	9.7+	56	18	20	3/4	3.4	8.0	1	7.2	-	92.8	.75	3.75	9.0	.6	.25/1.5	17000	360
09-23-93	3875	9.7+	74	20	20	2/3	3.4	6.8	1	7.0	0	93	.7	4.0	9.0	.2	.15/2.5	17000	400
09-24-93	5147	9.8	60	25	31	3/5	3.8	7.8	1	7.5	tr	92.5	.8	4.25	9.0	.5	.2/2.8	17000	240
09-25-93	6658	10.4	64	30	41	4/8	3.0	6.6	1	10.0	0	90	.5	4.5	9.1	.5	.25/2.9	17000	200
09-26-93	7036	10.5	57	25	29	4/8	2.8	6.8	1	10.0	0	90	.5	6.0	9.2	.6	.3/2.0	17000	320
09-27-93	7170	10.5	60	25	30	3/8	2.8	8.0	1	10.5	0	89.5	.5	6.0	9.2	.6	.3/2.0	17000	280
09-28-93	8000	10.6	60	31	43	4/9	3.0	7.6	1	11	0	89	.75	6.0	9.1	.6	.2/2.0	17500	320
09-29-93	8000	10.7	62	30	42	7/16	3.0	7.8	1	11.5	0	88.5	.75	5.0	9.0	.4	.15/1.9	17500	360
09-30-93	8000	10.7	65	28	40	5/14	3.0	8.0	1	11.5	0	88.5	.75	5.0	9.0	.3	.15/2.0	17500	360
10-01-93	8000	10.7	81	25	33	4/9	2.6	8.2	1	11.5	0	88.5	.75	5.0	9.0	.3	.15/1.7	17800	320
10-02-93	8000	10.5	59	20	24	3/6	3.2	8.2	1	10.5	0	89.5	.75	4.5	9.1	.3	.15/1.6	18000	320
10-03-93	8000	10.5	61	19	24	3/6	3.2	8.2	1	10.5	0	89.5	.75	4.5	9.1	.3	.15/1.5	18000	360

ARCO ALASKA, INC.
WILDCAT
AKMM930511:55-171-00009
JULY 1993

KUVLUM #2 OCS-Y-0865-1
KULLUK
NORTH REFERENCE : TRUE NORTH
SHORT COLLAR METHOD
MAG. FIELD STRENGTH (NT) : 57558
DIP ANGLE : 81.01
TOTAL CORRECTION : 31.55

MEASURED DEPTH	ANGLE DEGREE	DIRECTION DEGREE	VERTICAL DEPTH	LATITUDE FEET	DEPARTURE FEET	VERTICAL SECTION	DOG LEG SEVERITY
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1074.00	0.74	253.92	1073.97	-1.92	-6.65	-6.45	0.07
1170.82	0.48	251.58	1170.78	-2.22	-7.64	-7.41	0.27
1266.93	0.36	265.10	1266.89	-2.37	-8.32	-8.05	0.16
1358.72	0.33	259.03	1358.68	-2.45	-8.86	-8.52	0.05
1452.16	0.30	276.86	1452.12	-2.47	-9.37	-8.93	0.10
1547.36	0.19	262.30	1547.32	-2.46	-9.77	-9.25	0.13
1641.35	0.22	294.50	1641.31	-2.40	-10.08	-9.47	0.12
1738.12	0.43	249.86	1738.08	-2.45	-10.60	-9.90	0.33
1831.76	0.25	269.73	1831.71	-2.58	-11.13	-10.40	0.23
1927.19	0.36	260.92	1927.14	-2.62	-11.64	-10.83	0.13
2021.51	0.17	252.23	2021.46	-2.71	-12.06	-11.23	0.21
2115.73	0.25	255.09	2115.68	-2.81	-12.39	-11.54	0.08
2210.30	0.24	259.98	2210.25	-2.89	-12.78	-11.91	0.00
2306.32	0.12	18.84	2306.27	-2.83	-12.95	-12.00	0.33
2401.20	0.28	51.44	2401.15	-2.59	-12.73	-11.68	0.20
2495.88	0.23	60.47	2495.83	-2.35	-12.39	-11.26	0.07
2592.00	0.17	86.01	2591.95	-2.25	-12.08	-10.96	0.11
2687.19	0.06	223.74	2687.14	-2.27	-11.98	-10.89	0.22
2781.63	0.33	81.34	2781.58	-2.23	-11.66	-10.61	0.28
2869.95	0.24	95.79	2869.90	-2.21	-11.22	-10.25	0.13
2963.60	0.37	56.65	2963.54	-2.06	-10.77	-9.80	0.26
3060.21	0.32	47.83	3060.15	-1.70	-10.31	-9.22	0.08
3149.29	0.43	32.30	3149.23	-1.26	-9.95	-8.66	0.16
3242.22	0.51	31.18	3242.16	-0.61	-9.55	-7.95	0.09
3333.90	0.47	1.97	3333.83	0.11	-9.33	-7.34	0.27
3440.99	0.40	6.58	3440.92	0.91	-9.27	-6.80	0.06
3521.14	0.15	332.77	3521.07	1.28	-9.29	-6.59	0.35
3614.39	0.25	5.33	3614.32	1.59	-9.32	-6.43	0.15
3710.52	0.23	23.76	3710.45	1.97	-9.23	-6.12	0.08
3805.60	0.37	8.93	3805.53	2.46	-9.10	-5.73	0.17
3899.58	0.38	5.71	3899.51	3.07	-9.02	-5.29	0.03
3977.56	0.39	26.62	3977.48	3.57	-8.88	-4.87	0.18
4085.83	0.31	53.21	4085.75	4.07	-8.48	-4.25	0.16
4180.66	0.33	48.27	4180.58	4.41	-8.07	-3.72	0.02
4277.02	0.37	27.97	4276.93	4.87	-7.71	-3.16	0.13
4365.48	0.44	41.01	4365.39	5.37	-7.36	-2.57	0.13
4456.40	0.40	35.58	4456.31	5.89	-6.95	-1.93	0.06
4552.26	0.47	47.53	4552.17	6.43	-6.46	-1.22	0.12

ARCO ALASKA, INC.
 WILDCAT
 AKMM930511:55-171-00009
 JULY 1993

KUVLUM #2 OCS-Y-0865-1
 KULLUK
 NORTH REFERENCE : TRUE NORTH
 SHORT COLLAR METHOD
 MAG. FIELD STRENGTH (NT) : 57558
 DIP ANGLE : 81.01
 TOTAL CORRECTION : 31.55

MEASURED DEPTH	ANGLE DEGREE	DIRECTION DEGREE	VERTICAL DEPTH	LATITUDE FEET	DEPARTURE FEET	VERTICAL SECTION	DOG LEG SEVERITY
4645.97	0.38	54.53	4645.87	6.87	-5.93	-0.53	0.12
4739.78	0.37	51.88	4739.68	7.23	-5.44	0.08	0.04
4835.25	0.39	55.89	4835.15	7.60	-4.94	0.70	0.04
4926.63	0.40	58.01	4926.53	7.94	-4.42	1.32	0.00
5020.40	0.41	67.09	5020.30	8.24	-3.84	1.97	0.07
5116.55	0.61	67.27	5116.44	8.57	-3.05	2.79	0.21
5209.97	0.53	67.04	5209.86	8.93	-2.20	3.69	0.07
5305.49	0.64	77.51	5305.37	9.22	-1.27	4.60	0.16
5398.53	0.70	76.33	5398.41	9.46	-0.20	5.59	0.06
5493.57	0.70	79.49	5493.44	9.71	0.93	6.64	0.04
5582.97	0.93	77.13	5582.83	9.97	2.17	7.78	0.26
5678.24	1.09	93.97	5678.09	10.08	3.82	9.16	0.35
5773.01	1.19	95.63	5772.84	9.92	5.71	10.56	0.11
5867.25	1.24	86.34	5867.06	9.88	7.70	12.12	0.21
5963.31	1.34	85.98	5963.09	10.03	9.86	13.93	0.10
6057.33	1.30	89.19	6057.09	10.12	12.02	15.70	0.09
6155.89	1.38	88.44	6155.62	10.17	14.33	17.56	0.08
6246.52	1.40	90.58	6246.22	10.19	16.52	19.31	0.06
6343.21	1.42	88.65	6342.88	10.20	18.90	21.21	0.05
6437.02	1.44	96.52	6436.66	10.10	21.24	23.00	0.21
6530.52	1.40	95.36	6530.13	9.86	23.54	24.68	0.05
6625.49	1.25	90.26	6625.08	9.75	25.72	26.34	0.20
6717.99	1.13	90.62	6717.56	9.73	27.64	27.86	0.12
6811.52	1.11	86.25	6811.07	9.78	29.47	29.34	0.09
6908.43	0.89	88.57	6907.97	9.86	31.15	30.72	0.23
7001.41	0.70	87.03	7000.94	9.91	32.43	31.77	0.20
7094.07	0.65	71.73	7093.59	10.10	33.49	32.73	0.20
7191.10	0.67	75.26	7190.62	10.42	34.56	33.77	0.04
7289.93	0.66	79.87	7289.44	10.66	35.68	34.81	0.05
7384.33	0.57	83.08	7383.83	10.82	36.68	35.69	0.09
7479.16	0.35	68.42	7478.66	10.98	37.41	36.37	0.26
7576.54	0.46	53.07	7576.04	11.32	38.00	37.05	0.16
7667.12	0.62	62.88	7666.61	11.76	38.73	37.89	0.20
7764.12	0.42	53.59	7763.61	12.22	39.48	38.77	0.23
7855.86	0.51	50.80	7855.35	12.67	40.06	39.51	0.09
7948.98	0.40	63.86	7948.46	13.07	40.68	40.24	0.15
8044.80	0.49	55.09	8044.28	13.46	41.32	40.98	0.12
8135.91	0.46	52.84	8135.39	13.90	41.93	41.74	0.04
8235.49	0.50	38.54	8234.96	14.48	42.51	42.55	0.12
8327.87	0.58	21.77	8327.34	15.23	42.94	43.35	0.19

ARCO ALASKA, INC.
 WILDCAT
 AKMM930511:55-171-00009
 JULY 1993

KUVLUM #2 OCS-Y-0865-1
 KULLUK
 NORTH REFERENCE : TRUE NORTH
 SHORT COLLAR METHOD
 MAG. FIELD STRENGTH (NT) : 57558
 DIP ANGLE : 81.01
 TOTAL CORRECTION : 31.55

MEASURED DEPTH	ANGLE DEGREE	DIRECTION DEGREE	VERTICAL DEPTH	LATITUDE FEET	DEPARTURE FEET	VERTICAL SECTION	DOG LEG SEVERITY
8422.68	0.63	30.47	8422.14	16.13	43.38	44.25	0.11
8516.08	0.63	38.17	8515.53	16.98	43.96	45.22	0.08
8611.27	0.63	51.31	8610.72	17.72	44.69	46.25	0.15
8705.56	0.70	47.75	8705.00	18.43	45.52	47.34	0.08
8801.41	0.77	43.45	8800.84	19.29	46.40	48.56	0.08
8988.40	0.68	26.79	8987.82	21.18	47.76	50.79	0.12
9176.72	0.67	26.31	9176.13	23.16	48.74	52.78	0.00
9365.32	1.02	36.50	9364.71	25.49	50.23	55.38	0.20
9478.52	1.00	41.74	9477.89	27.04	51.49	57.32	0.09
9574.08	1.00	34.65	9573.43	28.35	52.52	58.93	0.13
9671.24	1.30	58.34	9670.57	29.62	53.94	60.83	0.57
9862.12	1.41	62.09	9861.40	31.86	57.85	65.30	0.08
9954.39	1.43	58.84	9953.64	32.99	59.84	67.56	0.09
10049.37	1.06	61.01	10048.60	34.02	61.63	69.61	0.40
10239.79	0.97	70.43	10238.99	35.42	64.68	72.88	0.10
10332.67	1.45	65.20	10331.85	36.17	66.49	74.77	0.53
10519.48	1.54	31.86	10518.60	39.30	69.96	79.43	0.46
10617.34	1.78	31.43	10616.42	41.71	71.45	82.08	0.25
10713.17	2.10	34.71	10712.19	44.43	73.22	85.15	0.35
10803.90	2.43	27.34	10802.85	47.51	75.06	88.47	0.48
10895.52	3.02	27.19	10894.36	51.38	77.05	92.41	0.64
10993.30	3.48	25.72	10991.99	56.34	79.52	97.39	0.48
11087.35	4.03	29.16	11085.84	61.80	82.36	102.96	0.63
11125.00	4.03	29.16	11123.40	64.10	83.65	105.39	0.05

CALCULATIONS BASED ON THE MINIMUM CURVATURE METHOD
 HORIZONTAL DISPLACEMENT AT A DEPTH OF 11125.0 FEET
 IS 105.4 FEET ALONG N 52 DEG 32 MIN E

RELATIVE TO WELL HEAD

VERTICAL SECTION RELATIVE TO WELL HEAD
 VERTICAL SECTION COMPUTED ALONG 52.54 DEG
 A DECLINATION OF 31.55 HAS BEEN APPLIED

Arco Alaska
 COOK INLET
 930818 :50-733-20450
 OCTOBER 1993

SOUTH COOK INLET #3
 ROWAN Gilbert Rowe
 NORTH REFERENCE : GRID NORTH
 SHORT COLLAR METHOD
 MAG. FIELD STRENGTH (NT) : 50600
 DIP ANGLE : 60.00
 TOTAL CORRECTION : 0.00

MEASURED DEPTH (feet)	INCLIN (degree)	AZIMUTH (degree)	VERTICAL DEPTH (feet)	LATITUDE (N/S,+/-) (feet)	DEPARTURE (E/W,+/-) (feet)	VERTICAL SECTION (feet)	DOG LEG SEVERITY (dg/100f)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1168.26	0.57	322.73	1168.24	4.64	-3.53	2.01	0.05
1261.74	0.41	333.21	1261.72	5.31	-3.96	2.34	0.20
1356.74	0.34	76.06	1356.72	5.68	-3.84	2.72	0.62
1452.70	0.08	101.51	1452.67	5.73	-3.50	2.95	0.29
1548.29	0.31	267.17	1548.26	5.71	-3.69	2.82	0.40
1641.68	0.13	327.24	1641.65	5.78	-3.99	2.72	0.28
1733.95	0.22	329.85	1733.92	6.02	-4.14	2.85	0.10
1830.39	0.20	31.05	1830.36	6.33	-4.14	3.10	0.22
1924.83	0.18	17.28	1924.80	6.61	-4.01	3.41	0.05
2022.13	0.09	22.18	2022.10	6.82	-3.94	3.63	0.09
2115.36	0.27	50.38	2115.33	7.03	-3.74	3.91	0.21
2212.57	0.19	67.27	2212.54	7.24	-3.42	4.25	0.11
2307.50	0.32	64.32	2307.47	7.41	-3.04	4.61	0.14
2401.75	0.25	160.42	2401.72	7.33	-2.73	4.71	0.46
2495.45	0.32	26.24	2495.42	7.37	-2.54	4.84	0.56
2590.19	0.36	52.74	2590.16	7.79	-2.19	5.39	0.17
2689.37	0.33	131.61	2689.34	7.79	-1.72	5.64	0.45
2781.30	0.55	43.63	2781.26	7.93	-1.22	6.03	0.68
2874.98	0.41	21.61	2874.94	8.57	-0.79	6.79	0.24
2968.18	0.33	38.28	2968.14	9.08	-0.50	7.38	0.14
3061.97	0.27	51.92	3061.93	9.43	-0.16	7.86	0.09
3152.98	0.21	69.15	3152.94	9.62	0.17	8.20	0.09
3242.33	0.14	40.00	3242.29	9.77	0.39	8.44	0.12
3336.89	0.25	62.39	3336.85	9.95	0.65	8.73	0.13
3430.55	0.12	62.79	3430.51	10.09	0.92	9.00	0.13
3473.83	0.25	54.91	3473.78	10.17	1.04	9.12	0.30
3563.50	0.23	70.29	3563.45	10.34	1.36	9.45	0.07
3676.01	0.22	101.19	3675.96	10.37	1.78	9.70	0.10
3707.84	0.22	12.97	3707.79	10.42	1.86	9.78	0.96
3802.62	0.19	63.10	3802.57	10.67	2.04	10.09	0.19
3897.24	0.32	63.42	3897.19	10.86	2.42	10.45	0.14
3988.52	0.48	3.65	3988.47	11.36	2.68	11.01	0.46
4083.75	0.45	106.74	4083.70	11.65	3.06	11.47	0.77
4179.16	0.51	217.53	4179.11	11.21	3.16	11.15	0.83
4274.97	0.60	25.09	4274.91	11.32	3.11	11.22	1.15
4367.75	0.51	335.18	4367.69	12.13	3.14	11.92	0.51
4461.12	0.41	29.76	4461.06	12.80	3.14	12.47	0.46

4553.01	0.44	6.42	4552.95	13.44	3.34	13.12	0.19
4646.62	0.30	83.77	4646.55	13.82	3.62	13.59	0.50
4739.28	0.31	347.11	4739.21	14.09	3.80	13.92	0.49
4835.65	0.34	336.31	4835.58	14.60	3.63	14.26	0.07
4929.53	0.33	347.63	4929.46	15.12	3.46	14.60	0.07
5023.80	0.24	358.70	5023.73	15.59	3.40	14.96	0.11
5113.83	0.25	256.66	5113.76	15.73	3.20	14.98	0.43
5210.65	0.35	347.19	5210.58	15.97	2.93	15.03	0.45
5304.72	0.31	327.06	5304.65	16.47	2.73	15.34	0.12
5399.64	0.19	15.68	5399.57	16.84	2.63	15.60	0.25
5493.87	0.15	328.32	5493.79	17.09	2.60	15.80	0.15
5585.79	0.23	286.16	5585.71	17.24	2.37	15.80	0.16
5683.08	0.19	350.41	5683.00	17.45	2.16	15.87	0.23
5777.47	0.21	53.01	5777.39	17.71	2.27	16.14	0.22
5870.88	0.27	74.87	5870.80	17.87	2.62	16.47	0.11
5964.10	0.28	60.60	5964.02	18.04	3.03	16.83	0.07
6060.56	0.40	18.10	6060.48	18.48	3.35	17.37	0.28
6153.23	0.49	21.54	6153.15	19.16	3.59	18.08	0.09
6250.88	0.55	59.34	6250.79	19.79	4.15	18.91	0.35
6344.96	0.43	55.87	6344.87	20.22	4.83	19.64	0.12
6438.75	0.48	35.79	6438.66	20.74	5.35	20.36	0.18
6533.91	0.66	44.77	6533.81	21.45	5.98	21.30	0.21
6628.07	0.78	52.54	6627.96	22.23	6.87	22.43	0.16
6721.85	0.76	57.76	6721.74	22.95	7.90	23.59	0.07
6816.40	0.67	65.09	6816.28	23.52	8.93	24.62	0.14
6910.53	0.57	55.66	6910.40	24.01	9.81	25.52	0.15
7005.88	0.71	57.18	7005.75	24.60	10.70	26.49	0.14
7101.23	0.89	43.49	7101.09	25.45	11.71	27.75	0.27
7289.67	0.96	56.75	7289.50	27.38	14.03	30.62	0.12
7384.20	1.09	33.23	7384.02	28.56	15.18	32.24	0.46
7479.40	1.28	33.65	7479.20	30.21	16.27	34.21	0.20
7572.76	1.67	35.42	7572.53	32.19	17.64	36.62	0.42
7664.78	1.86	35.42	7664.50	34.50	19.29	39.46	0.21
7763.66	1.94	40.49	7763.33	37.09	21.30	42.72	0.18
7856.37	2.16	48.02	7855.98	39.45	23.62	45.96	0.37
7951.11	2.18	46.41	7950.65	41.88	26.25	49.42	0.07
8000.00	2.18	46.41	7999.51	43.16	27.60	51.23	0.00

CALCULATIONS BASED ON THE MINIMUM CURVATURE METHOD

HORIZONTAL DISPLACEMENT AT A DEPTH OF 8000.0 FEET
IS 51.2 FEET ALONG N 32 DEG 36 MIN E
RELATIVE TO WELL HEAD

VERTICAL SECTION RELATIVE TO WELL HEAD
VERTICAL SECTION COMPUTED ALONG 32.59 DEG

SHOW EVALUATION REPORTS

This section of the report contains copies of show evaluation reports for Kuvlum No. 2 and Kuvlum No. 3. These reports are based on chromatography evaluations of gases retrieved from mud samples injected into Sperry-Sun's Steam Still apparatus; consequently, interpretations made on each report reflect this procedure. Show reports are not always included in the well report analysis because of restricted information requirements placed on some wildcat wells. They do offer some insight of fluid content on potential producing zones of good permeability; however, they are often inadequate on tight zones or when gas samples are taken while coring.

10

See attachment regarding SPE-AIME, B.O. Pixler referencing hydrocarbon ratio evaluations.

sperry-sun LOGGING SYSTEMS

DRILLING SERVICES
A Baroid Company

Show Report 1 Part B
 Depth Interval 6470 to 6500
 True Vert. Depth _____ to _____
 Prepared by TOM MANSFIELD
 Delivered to _____
 Date 8/13/93 Time 06:00 A.M.

Operator ARCO ALASKA INC.
 Well Name KUVLUM #2
 Location BEAUFORT SEA, ALASKA

ZONE PRODUCTION	<input type="checkbox"/> GAS	<input type="checkbox"/> OIL	<input type="checkbox"/> WATER	<input checked="" type="checkbox"/> NON-PRODUCIBLE HYDROCARBONS
	CONTACT DEPTH			
Gas/Oil _____ ft.		Gas/Water _____ ft.		Oil/Water _____ ft.

5	DEPTH	6475	ft.	GAS	<input type="checkbox"/> %	units	122	MUD CHLORIDES (ppm)	17000
FLOWLINE ppm		SUCTION ppm		=		SHOW ppm			
(Steam Still ppm's in 1000's)									
C 1	5,850	-	1,140	=	4,710	HYDROCARBON RATIOS			
C 2	57	-	4	=	53	C ₁ / C ₂ = 89			
C 3	22	-		=	22	C ₁ / C ₃ = 214			
C 4	21	-		=	21	C ₁ / C ₄ = 224			
C 5	7	-		=	7	C ₁ / C ₅ = 673			

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

6	DEPTH		ft.	GAS	<input type="checkbox"/> %	units		MUD CHLORIDES (ppm)	
FLOWLINE ppm		SUCTION ppm		=		SHOW ppm			
(Steam Still ppm's in 1000's)									
C 1		-		=		HYDROCARBON RATIOS			
C 2		-		=		C ₁ / C ₂ =			
C 3		-		=		C ₁ / C ₃ =			
C 4		-		=		C ₁ / C ₄ =			
C 5		-		=		C ₁ / C ₅ =			

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

LITHOLOGY

SAND-CLEAR, LIGHT GRAY, OCCASIONAL BLACK TO BROWN, VERY FINE GRAIN, OCCASIONAL FINE GRAIN, ANGULAR TO SUB ANGULAR, MODERATELY SORTED, PREDOMINATELY QUARTZ GRAINS, OCCASIONAL LITHIC FRAGMENT, SILTY CLAY MATRIX MATERIAL.

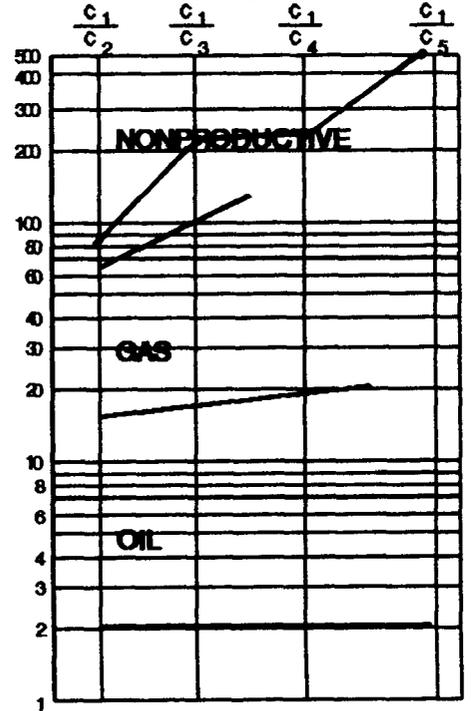
SHOW EVALUATION

LESS THAN 5% DULL ORANGE TO ORANGE FLUORESCENCE, TRACE YELLOW/GREEN FLUORESCENCE, FAIR YELLOW CUT FLUORESCENCE IN PART, NO ODOR, NO STAIN, SILTY CLAY MATRIX MATERIAL WITH POOR VISIBLE POROSITY.

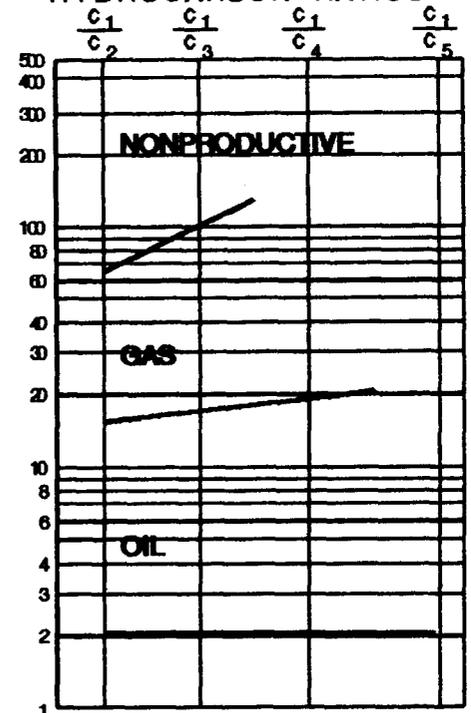
REMARKS

POOR SHOW

HYDROCARBON RATIOS



HYDROCARBON RATIOS



sperry-sun LOGGING SYSTEMS

DRILLING SERVICES
A Baroid Company

Show Report 2 Part B
Depth Interval 6663 to 6672
True Vert. Depth _____ to _____
Prepared by TOM MANSFIELD
Delivered to _____
Date 8/13/93 Time 22:30

Operator ARCO ALASKA INC.
Well Name KUYLUM #2
Location BEAUFORT SEA, AK

ZONE PRODUCTION	<input checked="" type="checkbox"/> GAS	<input type="checkbox"/> OIL	<input type="checkbox"/> WATER	<input type="checkbox"/> NON-PRODUCIBLE HYDROCARBONS
CONTACT DEPTH	Gas/Oil _____ ft.	Gas/Water _____ ft.	Oil/Water _____ ft.	

5	DEPTH <u>6665</u> ft.	GAS <input checked="" type="checkbox"/> % units <u>506</u>	MUD CHLORIDES (ppm) <u>17000</u>
	FLOWLINE ppm	SUCTION ppm	SHOW ppm
	(Steam Still ppm's in 1000's)		
C 1	<u>23,800</u>	<u>1,380</u>	<u>22,420</u>
C 2	<u>362</u>	<u>17</u>	<u>345</u>
C 3	<u>324</u>	<u>11</u>	<u>313</u>
C 4	<u>211</u>	<u>10</u>	<u>201</u>
C 5	<u>207</u>	<u>7</u>	<u>200</u>
	HYDROCARBON RATIOS		
	C ₁ / C ₂ = <u>65</u>		
	C ₁ / C ₃ = <u>72</u>		
	C ₁ / C ₄ = <u>112</u>		
	C ₁ / C ₅ = <u>112</u>		
PRODUCTION ANALYSIS	<input type="checkbox"/> GAS	<input type="checkbox"/> OIL	<input type="checkbox"/> WATER
	<input type="checkbox"/> NON-PRODUCIBLE HYDROCARBONS		

6	DEPTH <u>6675</u> ft.	GAS <input checked="" type="checkbox"/> % units <u>472</u>	MUD CHLORIDES (ppm) <u>17000</u>
	FLOWLINE ppm	SUCTION ppm	SHOW ppm
	(Steam Still ppm's in 1000's)		
C 1	<u>10,900</u>	<u>1,380</u>	<u>9,520</u>
C 2	<u>134</u>	<u>17</u>	<u>117</u>
C 3	<u>100</u>	<u>11</u>	<u>89</u>
C 4	<u>64</u>	<u>10</u>	<u>54</u>
C 5	<u>59</u>	<u>7</u>	<u>52</u>
	HYDROCARBON RATIOS		
	C ₁ / C ₂ = <u>81</u>		
	C ₁ / C ₃ = <u>107</u>		
	C ₁ / C ₄ = <u>176</u>		
	C ₁ / C ₅ = <u>183</u>		
PRODUCTION ANALYSIS	<input type="checkbox"/> GAS	<input type="checkbox"/> OIL	<input type="checkbox"/> WATER
	<input checked="" type="checkbox"/> NON-PRODUCIBLE HYDROCARBONS		

LITHOLOGY

SAND-CLEAR, TAN, LIGHT GRAY, BLACK IN PART. SILT-VERY FINE GRAIN, SUB ANGULAR TO SUB ROUND, PREDOMINATELY SUB ROUNDED POOR TO MODERATELY SORTED, UNCONSOLIDATED, CLAY MATRIX, 80-90% QUARTZ, 10-20% LITHIC GRAINS.

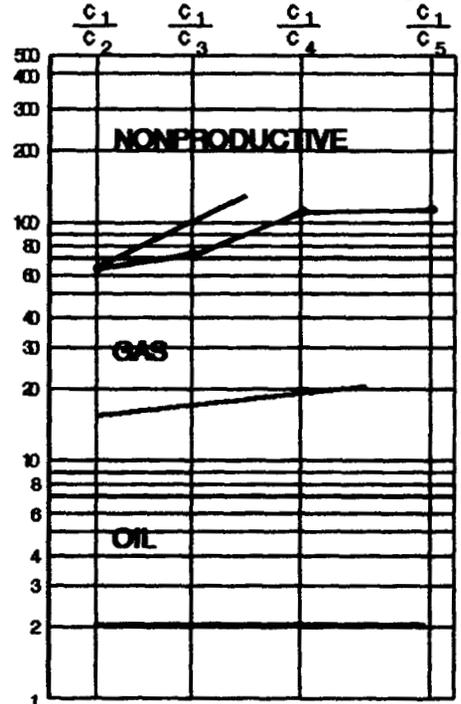
SHOW EVALUATION

MEDIUM TO BRIGHT GREEN/GOLD FLUORESCENCE ON 50% OF SURFACE, FAIR SLOW YELLOW CUT FLUORESCENCE, GOOD YELLOW/WHITE RESIDUAL RING CUT FLUORESCENCE. FAINT TO FAIR OIL ODOR, NO VISIBLE OIL STAINING, CLAY MATRIX, APPEARS LOW IN POROSITY. FLUORESCENCE INTENSITY FADING SOMEWHAT WITH TIME.

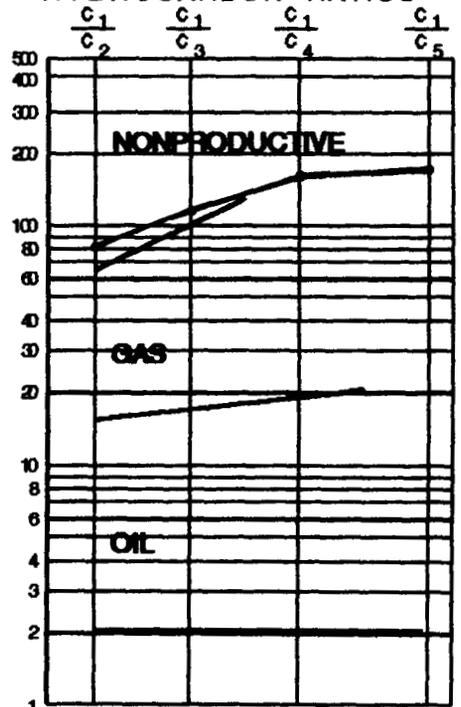
REMARKS

GOOD RESISTIVITY READINGS (10 AVG.) FROM 6665-6670. RATIO ANALYSIS INDICATES THAT THIS ZONE CONTAINS GAS. FAIR TO GOOD SHOW RATING FOR GAS/GAS CONDENSATE.

HYDROCARBON RATIOS



HYDROCARBON RATIOS



sperry-sun LOGGING SYSTEMS

DRILLING SERVICES
A Baroid Company

Show Report 3 Part B
Depth Interval 6698 to 6720
True Vert. Depth _____ to _____
Prepared by MANSFIELD/PATTON
Delivered to _____
Date 8/13/93 Time 22:30

Operator ARCO ALASKA INC.
Well Name KUVLUM #2
Location BEAUFORT SEA, AK

ZONE PRODUCTION	<input checked="" type="checkbox"/> GAS	<input type="checkbox"/> OIL	<input type="checkbox"/> WATER	<input type="checkbox"/> NON-PRODUCIBLE HYDROCARBONS
CONTACT DEPTH	Gas/Oil _____ ft.	Gas/Water _____ ft.	Oil/Water _____ ft.	

5	DEPTH <u>6700</u> ft.	GAS <input type="checkbox"/> %	<input checked="" type="checkbox"/> units	<u>523</u>	MUD CHLORIDES (ppm)	<u>17000</u>
	FLOWLINE ppm	SUCTION ppm	=	SHOW ppm	HYDROCARBON RATIOS	
	(Steam Still ppm's in 1000's)				$C_1 / C_2 =$ <u>73</u>	
C 1	<u>45,500</u>	<u>1,380</u>	=	<u>44,120</u>	$C_1 / C_3 =$ <u>114</u>	
C 2	<u>620</u>	<u>17</u>	=	<u>603</u>	$C_1 / C_4 =$ <u>169</u>	
C 3	<u>398</u>	<u>11</u>	=	<u>387</u>	$C_1 / C_5 =$ <u>174</u>	
C 4	<u>271</u>	<u>10</u>	=	<u>261</u>		
C 5	<u>260</u>	<u>7</u>	=	<u>253</u>		

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

6	DEPTH <u>6710</u> ft.	GAS <input type="checkbox"/> %	<input checked="" type="checkbox"/> units	<u>504</u>	MUD CHLORIDES (ppm)	<u>17000</u>
	FLOWLINE ppm	SUCTION ppm	=	SHOW ppm	HYDROCARBON RATIOS	
	(Steam Still ppm's in 1000's)				$C_1 / C_2 =$ <u>68</u>	
C 1	<u>33,800</u>	<u>1,380</u>	=	<u>32,420</u>	$C_1 / C_3 =$ <u>96</u>	
C 2	<u>495</u>	<u>17</u>	=	<u>478</u>	$C_1 / C_4 =$ <u>127</u>	
C 3	<u>350</u>	<u>11</u>	=	<u>339</u>	$C_1 / C_5 =$ <u>129</u>	
C 4	<u>265</u>	<u>10</u>	=	<u>255</u>		
C 5	<u>258</u>	<u>7</u>	=	<u>251</u>		

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

LITHOLOGY

SAND-DARK GRAY, BLACK, CLEAR, TRANSLUCENT, MEDIUM GRAY, VERY FINE TO MEDIUM GRAIN, PREDOMINATELY MEDIUM GRAIN, OCCASIONALLY COARSE TO VERY COARSE GRAIN, SUB ANGULAR TO WELL ROUNDED, PREDOMINATELY SUB ANGULAR, POOR TO MODERATELY SORTED, UNCONSOLIDATED, SILTY CLAY MATRIX, 60-70% CHERT & LITHIC FRAGMENTS, 30-40% QUARTZ.

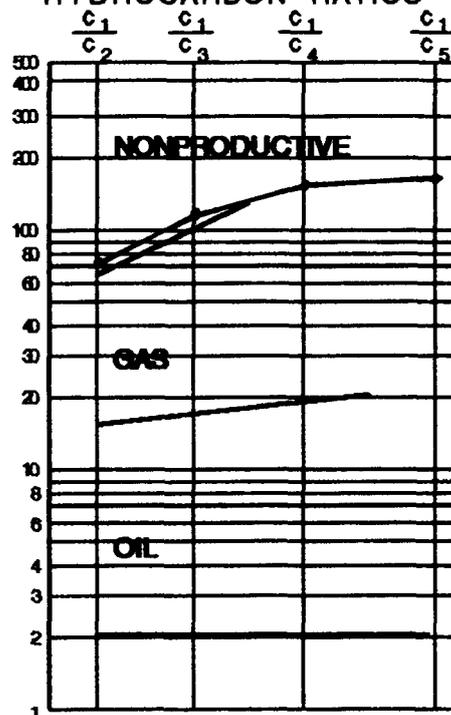
SHOW EVALUATION

50-70% MEDIUM TO BRIGHT GREEN/GOLD FLUORESCENCE ON SAMPLE SURFACE, GOOD FAST STREAMING MILKY WHITE/YELLOW CUT FLUORESCENCE, GOOD WHITE/YELLOW RESIDUAL RING CUT FLUORESCENCE, FAIR OIL ODOR, SLIGHT TRACE OF TAN TO LIGHT BROWN OIL STAIN. FLOURESCENSE INTENSITY FADING WITH TIME IN THE 6700 AND 6710 SAMPLES.

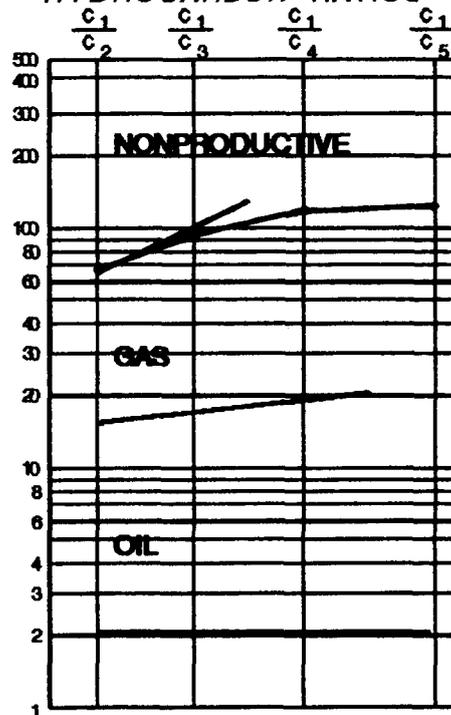
REMARKS

RESISTIVITY READINGS AVERAGING 7-8 IN THIS INTERVAL WHICH IS SOMEWHAT LOW FOR A VERY GOOD SHOW RATING. RATIO ANALYSIS INDICATES THAT THE ZONE IS PREDOMINATELY GAS BEARING OR POSSIBLY TIGHT. GOOD OVERALL SHOW RATING FOR GAS/GAS CONDENSATE.

HYDROCARBON RATIOS



HYDROCARBON RATIOS



sperry-sun LOGGING SYSTEMS

DRILLING SERVICES

A Baroid Company

Operator ARCO ALASKA INC.
 Well Name KUVLUM #2
 Location BEAUFORT SEA, AK

Show Report 4 Part B
 Depth Interval 6721 to 6729
 True Vert. Depth _____ to _____
 Prepared by MANSFIELD/PATTON
 Delivered to _____
 Date 8/13/93 Time 24:00

ZONE PRODUCTION	<input checked="" type="checkbox"/> GAS	<input type="checkbox"/> OIL	<input type="checkbox"/> WATER	<input type="checkbox"/> NON-PRODUCIBLE HYDROCARBONS
CONTACT DEPTH	Gas/Oil _____ ft.	Gas/Water _____ ft.	Oil/Water _____ ft.	

5	DEPTH	6525	ft.	GAS	<input checked="" type="checkbox"/> %	MUD CHLORIDES (ppm)	17000
					<input checked="" type="checkbox"/> units		
	FLOWLINE ppm	SUCTION ppm	=	SHOW ppm	HYDROCARBON RATIOS		
	(Steam Still ppm's in 1000's)				$C_1 / C_2 =$	61	
C 1	15,500	1,380	=	14,120	$C_1 / C_3 =$	77	
C 2	250	17	=	233	$C_1 / C_4 =$	98	
C 3	194	11	=	183	$C_1 / C_5 =$	99	
C 4	154	10	=	144			
C 5	150	7	=	143			

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

6	DEPTH	6729	ft.	GAS	<input checked="" type="checkbox"/> %	MUD CHLORIDES (ppm)	17000
					<input checked="" type="checkbox"/> units		
	FLOWLINE ppm	SUCTION ppm	=	SHOW ppm	HYDROCARBON RATIOS		
	(Steam Still ppm's in 1000's)				$C_1 / C_2 =$	57	
C 1	8,400	1,380	=	7,020	$C_1 / C_3 =$	68	
C 2	141	17	=	124	$C_1 / C_4 =$	83	
C 3	114	11	=	103	$C_1 / C_5 =$	78	
C 4	95	10	=	85			
C 5	97	7	=	90			

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

LITHOLOGY

SAND-DARK GRAY, BLACK, CLEAR, TRANSLUCENT, MEDIUM GRAY, FINE TO MEDIUM GRAIN, OCCASIONAL COARSE GRAIN TO SMALL PEBBLE SIZE, SUB ANGULAR TO WELL ROUNDED, POOR TO MODERATELY SORTED, UNCONSOLIDATED SILTY CLAY MATRIX, 60-70% CHERT AND LITHIC FRAGMENTS, 30-40% QUARTZ, OCCASIONAL CALCITE, TRACE PYRITE.

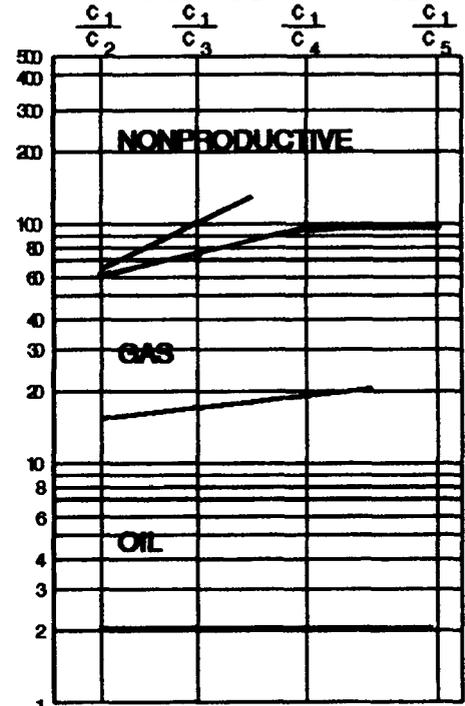
SHOW EVALUATION

60-70% MEDIUM TO BRIGHT GREEN/GOLD FLUORESCENCE ON SAMPLE SURFACE, GOOD FAST STREAMING MILKY WHITE/YELLOW CUT FLUORESCENCE, GOOD YELLOW/GOLD RESIDUAL RING CUT FLUORESCENCE, FAIR OIL ODOR, TRACE OF TAN TO LIGHT BROWN OIL STAIN.

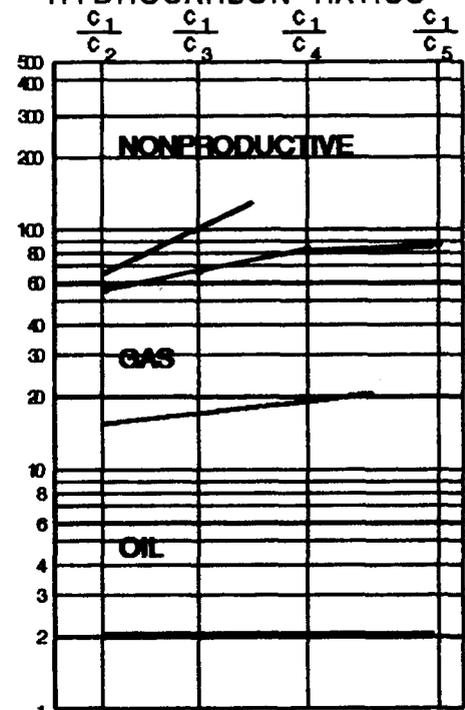
REMARKS

RESISTIVITY READINGS INCREASED IN THIS INTERVAL TO 15+. C1/C2 RATIOS ARE STILL IN THE GAS RANGE BUT ARE DECREASING WITH DEPTH. GOOD OVERALL SHOW RATING FOR GAS/GAS CONDENSATE.

HYDROCARBON RATIOS



HYDROCARBON RATIOS



sperry-sun LOGGING SYSTEMS

DRILLING SERVICES A Baroid Company

Show Report 5 Part B
 Depth Interval 7095 to 7115
 True Vert. Depth 7095 to 7115
 Prepared by TOM MANSFIELD
 Delivered to _____
 Date AUG 15.93 Time 23:00

Operator ARCO ALASKA INC.
 Well Name KUVLUM #2
 Location BEAUFORT SEA, AK

ZONE PRODUCTION	<input checked="" type="checkbox"/> GAS	<input type="checkbox"/> OIL	<input type="checkbox"/> WATER	<input type="checkbox"/> NON-PRODUCIBLE HYDROCARBONS
	CONTACT DEPTH		CONTACT DEPTH	
Gas/Oil _____ ft.		Gas/Water _____ ft.		Oil/Water _____ ft.

5	DEPTH	7100	ft.	GAS	<input checked="" type="checkbox"/>	%	units	258	MUD CHLORIDES (ppm)	17000
	FLOWLINE ppm		SUCTION ppm	=	SHOW ppm					
	(Steam Still ppm's in 1000's)									
C 1	15,800	-	1,570	=	14,230	HYDROCARBON RATIOS				
C 2	326	-	46	=	280	$C_1 / C_2 = 51$				
C 3	216	-	70	=	146	$C_1 / C_3 = 97$				
C 4	212	-	78	=	134	$C_1 / C_4 = 106$				
C 5	205	-	83	=	122	$C_1 / C_5 = 117$				

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

6	DEPTH	7110	ft.	GAS	<input checked="" type="checkbox"/>	%	units	268	MUD CHLORIDES (ppm)	17000
	FLOWLINE ppm		SUCTION ppm	=	SHOW ppm					
	(Steam Still ppm's in 1000's)									
C 1	10,800	-	1,570	=	9,230	HYDROCARBON RATIOS				
C 2	210	-	46	=	164	$C_1 / C_2 = 56$				
C 3	180	-	70	=	90	$C_1 / C_3 = 103$				
C 4	153	-	78	=	75	$C_1 / C_4 = 123$				
C 5	152	-	83	=	69	$C_1 / C_5 = 134$				

PRODUCTION ANALYSIS GAS OIL WATER NON-PRODUCIBLE HYDROCARBONS

LITHOLOGY

SAND-BLACK, M TO DARK GRAY, CLEAR, TRANSLUCENT, WHITE, FINE TO COARSE GRAIN, PREDOMINATELY COARSE GRAIN, ANGULAR TO SUB ANGULAR, POORLY SORTED, UNSCONSOLIDATED, TRACE CALCITE CEMENT (ONLY IN PART), 80% LITHIC FRAGMENTS, 20% QUARTZ, 10% DULL ORANGE MINERAL FLUORESCENCE.

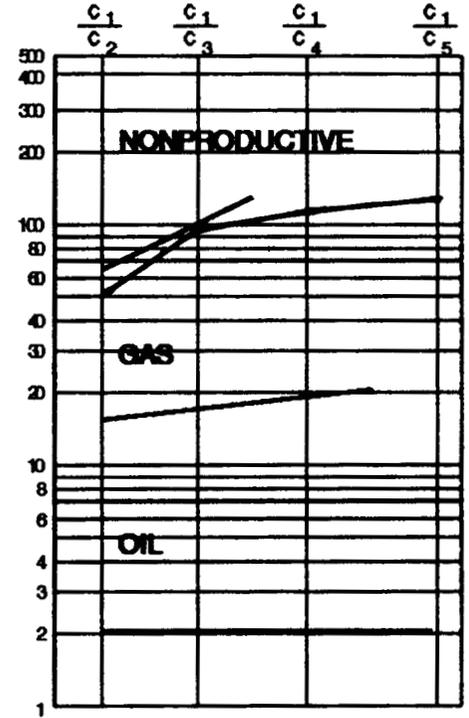
SHOW EVALUATION

10% BRIGHT YELLOW/WHITE SAMPLE FLUORESCENCE, VERY SLOW POOR WHITE CUT FLUORESCENCE, NO RESIDUAL CUT FLUORESCENCE. NO STAIN.

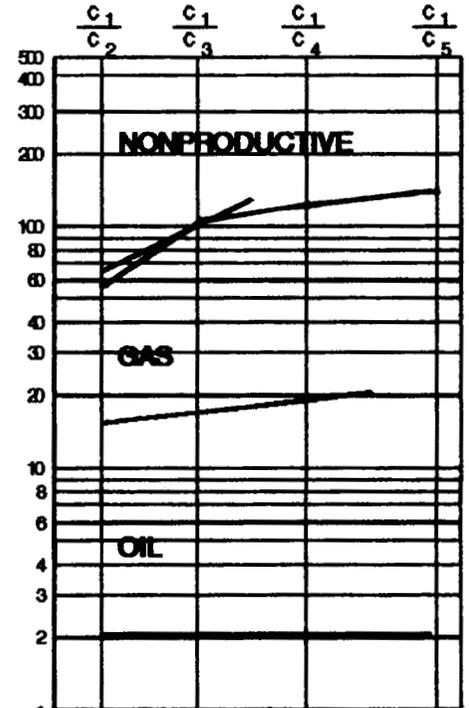
REMARKS

RESISTIVITY READINGS AVERAGED 7-8 FOR THIS INTERVAL. RATIO ANALYSIS INDICATES THAT THIS ZONE CONTAINS GAS. FAIR OVERALL SHOW RATING FOR GAS.

HYDROCARBON RATIOS



HYDROCARBON RATIOS





Formation Evaluation by Analysis of Hydrocarbon Ratios

B. O. Pixler, SPE-AIME, Baroid Div. National Lead Co.

Introduction

Mud logging was first offered commercially in Aug., 1939. This logging method quickly gained favor among many operators because the type of fluid in the formation could be determined within minutes after the formation was drilled. The presence and magnitude of the methane show was and is the most important factor in mud log interpretation. However this magnitude in some instances was improperly understood, and as a consequence some operators still do not use mud logging, even though the early technique frequently made the difference between a successful well and an abandoned hole. Both the "hot wire" log of gas combustibles in the sample and the percent-of-gas log obtained with the conventional gas trap and the gas chromatograph indicate only that the reservoir in question contains hydrocarbons. These methods do not necessarily indicate the quantitative amounts of the various hydrocarbons in the mud.

The addition of a new Steam Still-Reflux gas sampling system to gas chromatography enables accurate determination of the composition of the mud gas sample. A knowledge of gas composition makes it possible to establish the relationship of methane to the heavier hydrocarbon shows. An awareness of this relationship led to a new, additional mud log interpretative technique that permits relating the quantitative amounts of methane (C_1), ethane (C_2), propane (C_3), butane (C_4), and pentane (C_5) to in-place reservoir fluid content.

A long-accepted premise is that as formations are drilled, the drilling mud filtrate partially flushes the formation fluid ahead of the bit. It was generally thought that the formations were flushed to an irreducible minimum — generally considered to be about 30 percent of in-place fluid. Experience in mud logging, however, has shown that this rarely happens. This partial flushing does not prevent mud logging from successfully determining productive or non-productive formations. Experienced logging engineers, in possession of quantitative gas analyses, make interpretations that take into account the flushing that results in rocks of various permeabilities, the effect of overbalanced mud weight and the effect of initial filtrate loss.

Method

Ordinarily, when formation cuttings are drilled they retain much of the formation pore fluid. This fluid is released to the mud column as the cuttings travel up the annulus. Most of the formation fluid in the cuttings will be "produced" into the drilling mud during the top 500 ft of hole travel. Conventionally, a mud sample is diverted to a mechanically operated gas trap to obtain a sample of the gas in the mud. The efficiency of this trap is from 15 to 70 percent, depending upon the gel strength of the mud, the amount of mud flowing through the trap and the rotation speed of the trap impeller. The magnitude of the conventional

The ratio of methane to the heavier hydrocarbon components — ethane, propane, butane, and pentane — is indicative of gas, oil and water productive potential. The Steam Still-Reflux Unit, used in conjunction with mud logs and gas chromatographs yields a quantitative analysis from which this ratio can be plotted.

gas show is, therefore, quantitative only to the air-gas sample obtained. The sample is accurately analyzed by the gas chromatograph; but, because the sample furnished by the conventional gas trap represents only a fraction of the gas present in the mud, and because that fraction is not representative of the total gases in the mud, the results are still only qualitative.

When the Steam Still-Reflux Unit is used to obtain the gas sample, the gas sample will represent almost 100 percent of the hydrocarbon fractions C_1 through C_5 that were in the mud sample. This enables the chromatograph analysis to be related quantitatively to the mud, and the readings to be reported as parts per million of each hydrocarbon vapor (C_1 through C_5) to mud volume.

Because the cuttings from a particular formation "produce" the gas they contain into the drilling mud, it was reasonable to assume that this same formation, if completed, would produce gases of a similar composition. This assumption led to a comparison of ppm Logs of hydrocarbon vapors with similar data from producing wells. Plots were made of the ratio of methane to each of the heavier hydrocarbons from many analyses of wellhead samples. These plots were compared with plots, made from ppm Logs, of gas in mud. Both groups of plots showed definite patterns between (1) the magnitude of the ratios of methane to each of the heavier hydrocarbons, and (2) the slope of the lines of the plotted ratios. These, in turn, indicate productive potential and reservoir permeability.

The Steam Still-Reflux Unit consists of a small steam boiler, mud-injection port, mud-steam mixing chamber, Reflux-Condensing Unit and a gas-extraction port. Five ml of mud are injected into the purged mud-steam mixing chamber. The mud is rolled with 2,000 to 4,000 volumes of steam. The hydrocarbons (C_1 through C_5) extracted from the mud are collected

at the Reflux-Condensing Unit, withdrawn with a syringe, diluted to the standard chromatograph sample size and injected into the chromatograph for analysis. The Reflux-Condensing Unit removes only the lighter paraffin series hydrocarbons from the mud sample tested. For example, if the mud contains diesel oil, the more complex hydrocarbons — C_6 and above — condense and drop back into the mud-steam mixing chamber. Therefore, regardless of whether the fluid phase of the mud is oil or water, the gas sample analyzed contains only the light fractions through C_5 , and the analysis is representative of the formation gas.

The full importance of determining formation gas composition has not always been apparent. At first it was observed that if the magnitude of butane in the mud was greater than the magnitude of either propane or ethane, the zone in question would produce water and hydrocarbons. Later, the ratios of methane to each of the heavier hydrocarbon components were plotted on semilog paper. Hydrocarbon ratio plots obtained from ppm Logs and available data from wellhead gas sample analyses were compared. The comparison of the plots from ppm Logs and wellhead gas analysis data showed a striking correlation. The correlation demonstrated that ppm Logs made with Steam Still-Reflux samples could be interpreted in terms of in-place formation content.

The magnitude of the methane-to-ethane ratio determines if the reservoir contains gas or oil or if it is nonproductive. The slope of the line of the ratio plot of C_1/C_2 , C_1/C_3 , C_1/C_4 , and C_1/C_5 indicates whether the reservoir will produce hydrocarbons or hydrocarbons and water. Positive line slopes indicate production; negative slopes indicate water-bearing formations. An undersaturated reservoir may show a negative slope, but such occurrences are rare. The ratio plots may not be definitive for low permeability zones, but unusually steep plots indicate tight zones.

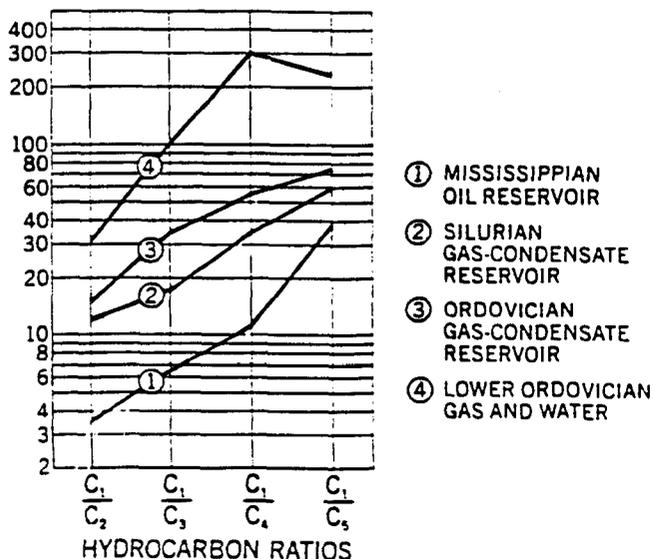


Fig. 1—Hydrocarbon ratio plots obtained from wellhead sample analyses data, limestone reservoirs, Rocky Mountain area.

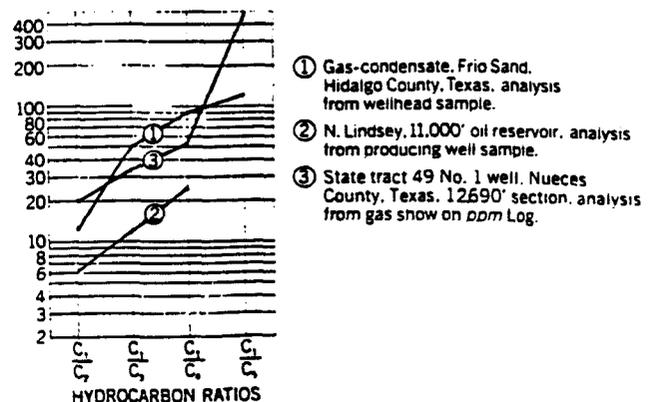


Fig. 2—Hydrocarbon ratio plots, productive reservoirs, South Texas.

A ratio of C_1/C_2 between 2 and 15 indicates oil. A ratio of C_1/C_2 between 15 and 65 indicates gas. The lower the C_1/C_2 ratio, the richer the gas or the lower the oil gravity. If the ratio of C_1/C_2 is below about 2 or above about 65 the zone is nonproductive.

Field Examples

Fig. 1 shows average hydrocarbon ratio plots from limestone reservoirs in the Rocky Mountain area. Plot 1 is derived from analyses of gases from Mississippian oil-producing reservoirs. The C_1/C_2 ratio is 3.5. The slope of the line is positive and not steep. Plot 2 was obtained from analyses of gases from wells producing gas-condensate from the Silurian. The C_1/C_2 ratio is 12; the line slope is again positive and not steep. Plot 3 is from gas-condensate wells producing from the Ordovician. The C_1/C_2 ratio is 15 and, again, the slope of the line is not steep; all three plots show slopes favorable for production. Plot 4 shows ratios obtained from an analysis of gas from the Lower Ordovician, which produced gas and water. The plot shows a negative slope of the section from the C_1/C_2 ratio to the C_1/C_5 ratio. Many tests have verified the fact that if a ratio plot shows a negative slope, the zone in question is water-bearing.

Fig. 2 shows plotted hydrocarbon ratios for productive reservoirs in South Texas. Plot 1 was made from an analysis of a wellhead sample of gas-condensate produced from a Frio sand, Hidalgo County. The production is rich in liquid hydrocarbons as indicated by the low C_1/C_2 ratio. Plot 2 is from an analysis of a wellhead gas sample from an 11,000-ft oil reservoir, North Lindsey field. The pentane was not reported, but the low C_1/C_2 ratio indicates oil production. Plot 3 was obtained from a gas show at 12,690 ft on the ppm Log of the State Tract 49 No. 1 Well, Nueces County, Tex. Formation tests resulted in gas production.

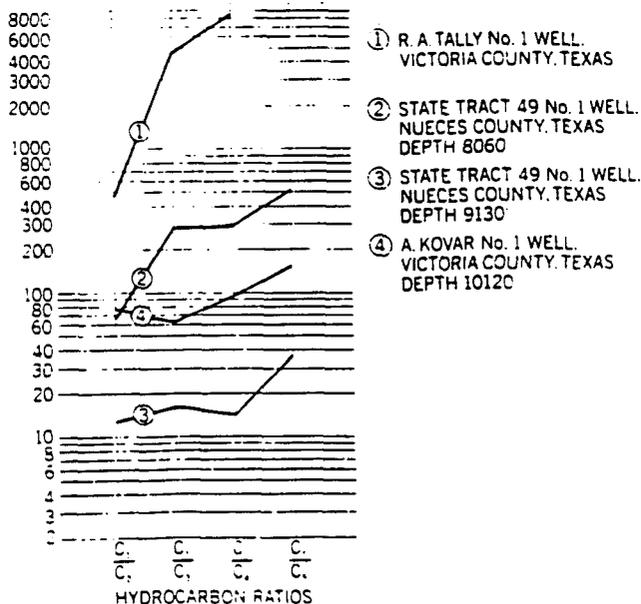


Fig. 3—Hydrocarbon ratio plots, nonproductive reservoirs, South Texas—analyses from gas shows on ppm Logs.

Experience shows that if the C_1/C_2 ratio is above 65 the zone is too tight for commercial production. Fig. 3 shows the ratio plots obtained from ppm Logs on Texas Gulf Coast wells that were nonproductive in the zones of interest. Plot 1 is from the ppm Log of the R. A. Tally No. 1 Well, Victoria County, Tex. The C_1/C_2 ratio was 470. The zone was tested extensively but it was a low permeability reservoir that could not be commercially completed. Plots 2 and 3 are from the State Tract 49 No. 1 Well, Nueces County, Tex. Plot 2 was from a sand encountered at about 8,060 ft. The relatively high ratios of C_1/C_2 , C_1/C_3 , C_1/C_4 , and C_1/C_5 indicated that the zone was nonproductive because of the low permeability. This was subsequently verified by testing. Plot 3 was obtained from a sand at 9,130 ft. The negative slope of the ratio plot, C_1/C_2 to C_1/C_3 , indicated that the zone was water-bearing. Subsequent formation tests showed water and non-commercial amounts of gas.

Plot 4 was obtained from the ppm Log of the Kovar No. 1 Well, Victoria County, Tex. The sand encountered from which the plot was made is at 10,120 ft. The gas show appeared to be good, but a negative slope of the C_1/C_3 ratio to the C_1/C_4 ratio was positive identification of a water-bearing formation.

Evaluation Technique

It is apparent that with this evaluation system, potential production can be accurately predicted. The only significant time lapse between penetration of the formation and evaluation of its productive possibilities is the time required to pump the mud from the bottom of the hole to the surface and analyze it by the Steam Still-Reflex and Chromatograph method. Fig. 4 shows the evaluation technique, which may be described as follows.

First, record the net increase of each gas component over the background gas; next, plot the ratios

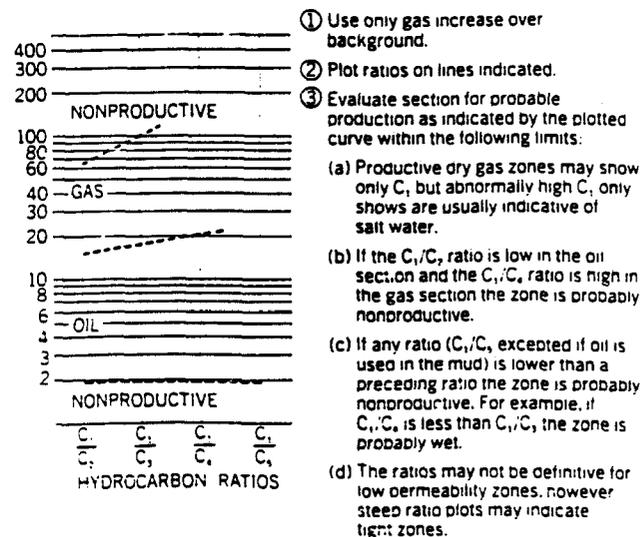


Fig. 4—ppm Log and report form for evaluation of show.

C_1/C_2 , C_1/C_3 , C_1/C_4 , C_1/C_5 on the ratio lines as indicated. Then evaluate, within the following limits, the section in question for probable production as indicated by the plotted curve:

1. Productive dry gas zones may show only C_1 , but abnormally high shows of C_1 only are usually indicative of salt water.

2. If the C_1/C_2 ratio is low in the oil section and the C_1/C_3 ratio is high in the gas section the zone is probably nonproductive.

3. If any ratio (C_1/C_3 excepted if oil is used in the mud) is lower than a preceding ratio, the zone is probably nonproductive. For example, if C_1/C_4 is less than C_1/C_3 , the zone is probably water-bearing.

4. The ratios may not be definitive for low permeability zones; however, steep ratio plots may indicate tight zones.

Application

The ppm Log is only one of many tools that are ordinarily used for formation evaluation. But in many instances, the ppm Log has furnished the vital information necessary to make the final decision on a well. One well drilled in inland waters of Louisiana had

what appeared on the ppm Log to be a good sand body, but the ppm Log showed only a nominal increase in gas. After the sand was penetrated and the well deepened, hole trouble was encountered. No other information of interest was available on the sand. The cost of the side-tracking to investigate the sand was sizable. Tight hole conditions and the low magnitude of the gas show indicated that the sand had good permeability and that possibly formation hydrocarbons had been flushed ahead of the bit. A plot of the hydrocarbon ratios indicated oil production. Therefore, at considerable expense, the sand was investigated and a new oil field was found.

An interesting well recently drilled in St. Martin Parish, La., was the No. 1 St. Martin Bank and Trust located on the southeast flank of the Anse La Butte Dome. A good sand encountered at about 8,000 ft showed oil, but the negative slope of the ratio plot indicated that the sand was water-bearing. The well was deepened to approximately 9,600 ft. One of the partners, a successful independent with a talent for finding oil by "feel" and by prudent use of the latest technology, decided that the formations in which the well was being drilled were tilted to almost vertical.

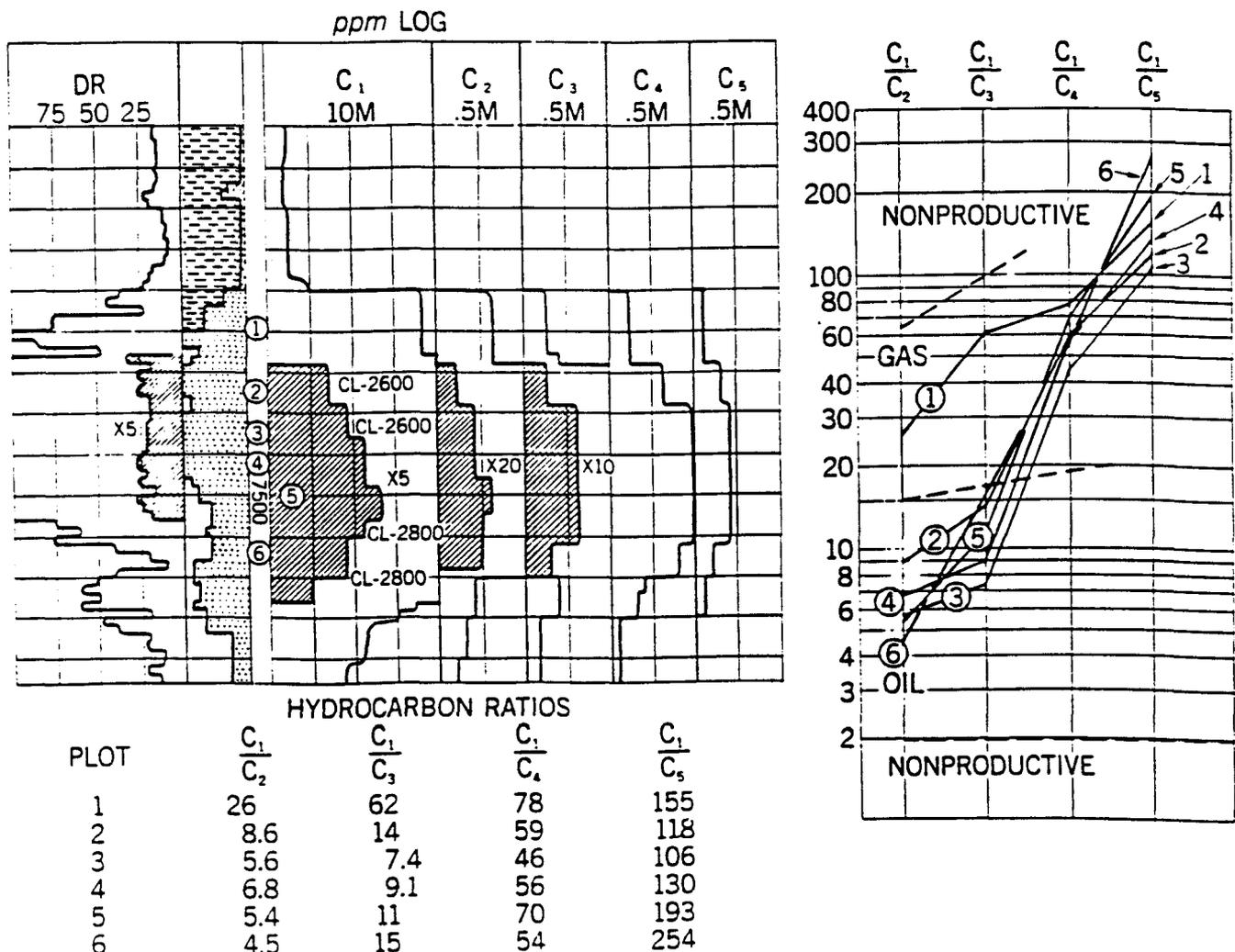


Fig. 5—ppm Log and hydrocarbon ratio plots. No. 1 St. Martin Bank and Trust Well, St. Martin Parish, La.

On his recommendaion the well was plugged back to about 7,000 ft and sidetracked. The sand that was drilled at 8,000 ft in the first hole was encountered in the directional hole at approximately 7,400 ft and the entire sand was hydrocarbon saturated.

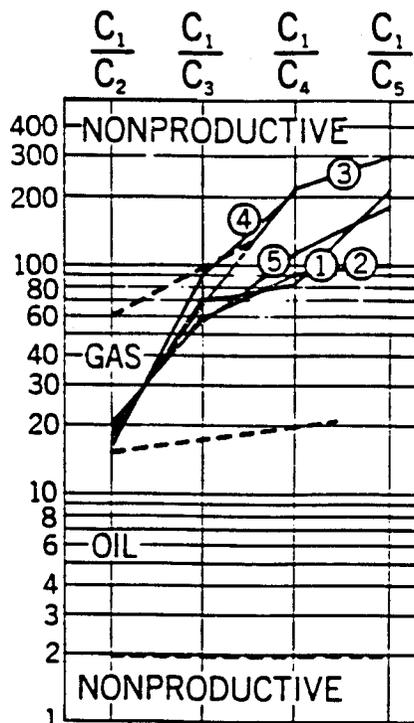
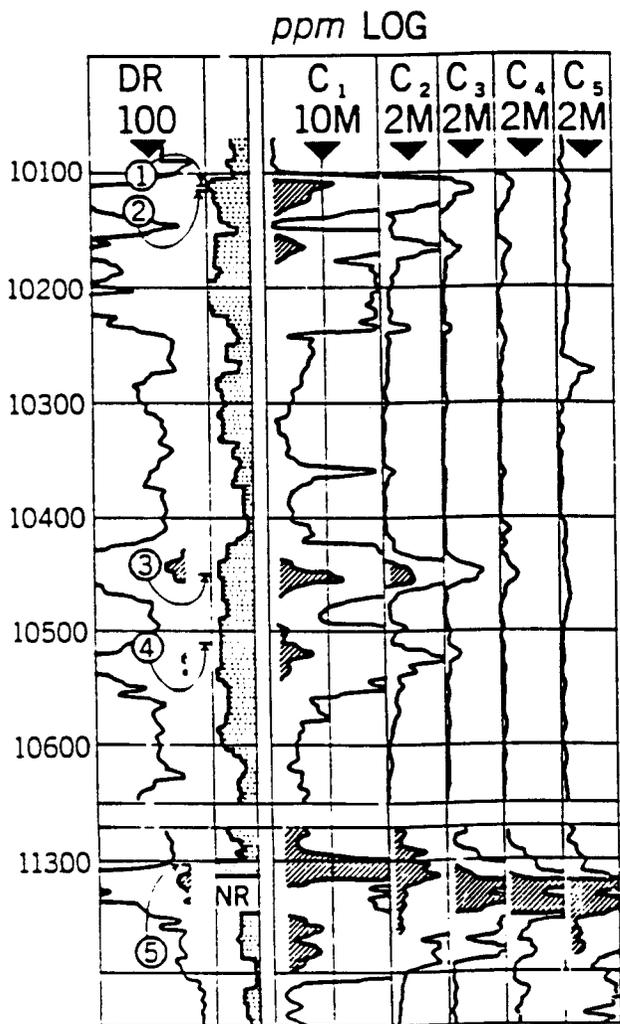
The ppm Log and the ratio plots from the sand in the sidetrack hole are shown in Fig. 5. Table 1 shows the mud gas components related to percent of total gas. In actual practice the ppm gas shows obtained from the ppm Log are not converted to percent of total gas; but note the general decrease in percent methane in the lower section of the sand compared with that in the upper section. The magnitude of the gas show in the straight hole and in the sidetrack hole was significant. An accurate determination, however, of the composition of the gas in both cases led to correct conclusions on the potential productivity of the sand at the different depths in each hole. Note that the ratio Plot 1 at the top of the sand indicates a gas cap. As shown in Table 1, the gas was 93.1 percent methane. Subsequent plots indicated that production would be oil. In each of these cases the C_1/C_2 ratio was less than 9. The lowest ratio, 4.5, is shown in Plot 6, which was made from the show at

TABLE 1—MUD GAS COMPONENTS, PERCENT OF TOTAL GAS

Depth (ft)	C_1	C_2	C_3	C_4	C_5
7,460	93.1	3.6	1.5	1.2	0.6
7,475	82.4	9.6	5.9	1.4	0.7
7,485	74.4	13.3	10.0	1.6	0.7
7,490	78.0	11.4	8.6	1.4	0.6
7,500	77.0	14.3	7.2	1.1	0.4
7,515	76.1	17.1	5.1	1.4	0.3

the bottom of the sand.

Another example of the application of the ppm Log is No. 1 State Tract 198 Well, Aransas County, Tex. Many sands were encountered showing the presence of hydrocarbons. The logging crew submitted more than 60 ratio plots to the operator during the drilling of the well. In almost all instances subsequent information verified the logging engineers' predictions of probable productivity based on the ratio plots. Fig. 6 shows a section of the ppm Log and the ratio plots for this well. The gas composition relating the percent of each gas component to the total gas is shown in Table 2. Gas condensate production is indi-



HYDROCARBON RATIOS

PLOT	$\frac{C_1}{C_2}$	$\frac{C_1}{C_3}$	$\frac{C_1}{C_4}$	$\frac{C_1}{C_5}$
1	18	71	84	230
2	20	61	92	102
3	19.5	78	233	310
4	16	93	232	∞
5	19.3	58	115	185

Fig. 6—ppm Log and hydrocarbon ratio plots. No. 1 State Tract 198 Well, Aransas County, Tex.

TABLE 2—MUD GAS COMPOSITION, PERCENT OF TOTAL GAS

Depth (ft)	C ₁	C ₂	C ₃	C ₄	C ₅
10,110	92.0	5.2	1.3	1.1	0.4
10,115	92.0	4.6	1.5	1.0	0.9
10,450	93.3	4.8	1.2	0.4	0.3
10,520	92.8	5.8	1.0	0.4	0.0
11,305	92.3	4.8	1.6	0.8	0.5

cated by the ppm Log and ratio plots as shown. The zones are tight marine deposits — especially the 10,520-ft zone. Plot 4 has the steepest line slope; pentane was not present. The slope of Plot 3 is steep. Plots 2 and 5 show more favorable (less steep) line slopes. The electric log and subsequent formation tests made of each zone indicated probable production. The well was completed as a gas condensate producer in the 11,300-ft section, which is the section plotted as No. 5.

Conclusions

Only qualitative shows of hydrocarbons in the mud can be derived from conventional mud logs. If chromatography is used, only a general indication of in-place gas composition is obtainable. Such hydrocarbon shows may be reported as units of gas or percent hydrocarbons or parts per million of gas in the air-gas mixture tested. Only the presence in relative amounts, not the actual quantity, of hydrocar-

bons in mud is indicated, and other supplemental information may be necessary to evaluate the formation in terms of potential productivity. However, if the composition of the gas sample obtained from the mud is representative of the in-place formation gas, then the gas analysis is accurate. The use of the Steam Still-Reflux Unit makes possible a report of formation gas composition on the ppm Log. Meaningful ratio plots of gas composition can then be made. Even though many factors affect the amount of reservoir fluid released to the drilling mud, reservoir potential productive capabilities can be determined by a study of the ratio of methane to each of the heavier hydrocarbon components. The hydrocarbon ratio plot is a unique technique and provides the operator with new information for evaluating productive possibilities of exploratory wells.

Computer programs involving percent gas in mud (ppm Log) and gas composition are being used in special cases to determine reservoir potential production. The use of computers in mud log interpretation, although new, will contribute significantly towards a better application of the data shown on the ppm Log.

JPT

Original manuscript received in Society of Petroleum Engineers office Aug. 5, 1968. Revised manuscript received March 5, 1969. Paper (SPE 2254) was presented at SPE 43rd Annual Fall Meeting held in Houston, Tex., Sept. 29-Oct. 2, 1968. © Copyright 1969 American Institute of Mining, Metallurgical, and Petroleum Engineers, Inc.

sperry-sun
DRILLING SERVICES *LOGGING SYSTEMS*
 A Baroid Company

DEPTH 296
 OPERATION DRLG
 FOOTAGE 71

No. 1
 DATE Jul 29 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0-1</u>	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>NA</u>	LITHOLOGY <u>NA</u>	SAMPLE DEPTH _____	TRIP CHLORIDES _____	LAG DOWN DP _____	LAG OFF BOTTOM <u>NA</u>	DRILL RATE ft/hr <u>5.2</u>	CORRECTED 'D' EXP. _____	SHALE DENSITY g/cc _____	EWR Res. _____
BACKGROUND CONNECTION TRIP _____	FLOWLINE TEMP <u>NA</u> degrees F											

FORMATION PRESSURE DATA

	CASING	BOTTOM HOLE	OPEN HOLE
PORE PRESSURE	_____ psi _____ ppg	<u>131</u> psi <u>8.5</u> ppg	_____ psi _____ ppg _____ ft
FRACTURE PRESSURE	<u>NA</u> psi _____ ppg	_____ psi _____ ppg	_____ psi _____ ppg _____ ft
ECD	_____ psi _____ ppg	<u>132</u> psi <u>8.6</u> ppg	_____ psi _____ ppg _____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME _____	BIT NO. <u>1</u>	PUMPS 1. <u>ID 1600</u> 2. <u>1D</u>
TYPE <u>SEA WATER</u>	TYPE <u>ATXG1</u>	SIZE inches <u>7.5x12</u> <u>7.5x12</u>
WEIGHT IN <u>8.5</u>	IADC CODE _____	CAPACITY gal/stk <u>6.54</u> <u>6.54</u>
FUNNEL VIS. _____	SIZE <u>26</u>	PUMP RATE stks/min <u>81</u> <u>80</u>
PV/YP _____	JETS <u>3-21.1-22</u>	FLOW RATE gal/min <u>530</u> <u>523</u>
GELS _____	DEPTH OUT _____	PRESSURE psi _____ <u>1490</u>
pH _____	ROT HRS. <u>14.7</u>	PD SURF / DS psi _____ <u>193</u>
FILT/CAKE API _____	FOOTAGE <u>67</u>	ANN / BIT psi _____ <u>0</u>
HP-HT _____	AVG ft/hr <u>5.2</u>	JET VELOCITY ft/sec _____ <u>246</u>
Pm _____	GRADE _____	JET IMPACT lbs _____ <u>1149</u>
Pf/Mf _____	HOLE DEV. _____	BIT HP _____ <u>988</u>
CHLORIDES ppm _____	COST/FT _____	HP RATIO / HP/IN2 _____ <u>.4 hp/in2</u>
CALCIUM ppm _____	RPM <u>140</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS _____	WOB <u>35</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>9.5X26</u>	<u>71</u>	<u>.636</u>	<u>40</u>	<u>378</u>	<u>14</u>
<u>5X26</u>	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	
	DP	HWDP	DC		
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>9.5</u>	_____	_____
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	_____
CAP-bbls/ft	_____	<u>.0087</u>	<u>.0080</u>	_____	_____
DISP-bbls/ft	_____	<u>.0181</u>	<u>.0707</u>	_____	_____
LENGTH-ft	_____	<u>193</u>	<u>103</u>	_____	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>195</u>	_____	_____

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

RIG UP TO RUN 30' CSG. RUN 30' CSG AND LOCK INTO PGB. PU 26' BIT. BHA AND MUD MOTOR. DRILL AND WASH CSG TO 296'. NO RISER.

GAS LIFT SYSTEM INSTALLED. BACKGROUND GAS 0-1 UNIT.

ADT DON WALTERS

sperry-sun *LOGGING SYSTEMS*

DRILLING SERVICES
A Baroid Company

DEPTH 915
OPERATION DRLG
FOOTAGE 619

No. 2
DATE Jul 30 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>5</u>	MAX GAS (units) <u>8</u>	AT DEPTH (feet) _____	SURVEY DATA <u>NA</u>	LITHOLOGY <u>NA</u>	DRILL RATE ft/hr <u>65</u>
BACKGROUND CONNECTION TRIP _____	LAG DOWN DP _____	LAG OFF BOTTOM <u>NA</u>	SAMPLE DEPTH _____	TRIP CHLORIDES _____	CORRECTED 'D' EXP. _____
FLOWLINE TEMP <u>NA</u> degrees F					SHALE DENSITY g/cc _____
					EWR Res. _____

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>133</u> psi	<u>8.5</u> ppg	<u>404</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>NA</u> psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg
ECD	<u>135</u> psi	<u>8.64</u> ppg	<u>419</u> psi	<u>8.8</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME _____	BIT NO. <u>1</u>	PUMPS <u>1</u> ID1600 <u>2</u> ID1600
TYPE <u>SEA WATER</u>	TYPE <u>ATXG1</u>	SIZE inches <u>7.5x12</u> <u>7.5x12</u>
WEIGHT IN <u>8.5</u>	IADC CODE _____	CAPACITY gal/stk <u>6.54</u> <u>6.54</u>
FUNNEL VIS. _____	SIZE <u>26</u>	PUMP RATE stks/min <u>80</u> <u>80</u>
PV/YP _____	JETS <u>3-21.1-22</u>	FLOW RATE gal/min <u>523</u> <u>523</u>
GELS _____	DEPTH OUT _____	PRESSURE psi _____
pH _____	ROT HRS. <u>33.4</u>	PD SURF / DS psi <u>176/991</u>
FILT/CAKE API _____	FOOTAGE <u>705</u>	ANN / BIT psi <u>1/416</u>
HP-HT _____	AVG ft/hr <u>20.6</u>	JET VELOCITY ft/sec <u>234</u>
P _m _____	GRADE _____	JET IMPACT lbs <u>1040</u>
PI/Mf _____	HOLE DEV. _____	BIT HP <u>245</u>
CHLORIDES ppm _____	COST/FT _____	HP RATIO / HP/IN2 <u>.5 hp/in2</u>
CALCIUM ppm _____	RPM <u>107</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS _____	WOB <u>22</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>9.5X26</u>	<u>690</u>	<u>.636</u>	<u>42</u>	<u>390</u>	<u>14</u>
<u>5X26</u>	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING:		
	DP	HWDP	DC	DEPTH		
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>9.5</u>	<u>301</u>	_____	_____
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>30</u>	_____	_____
CAP-bbls/ft	_____	<u>.0087</u>	<u>.0080</u>	<u>28</u>	_____	_____
DISP-bbls/ft	_____	<u>.0181</u>	<u>.0707</u>	<u>.7616</u>	_____	_____
LENGTH-ft	_____	<u>587</u>	<u>103</u>	<u>90</u>	_____	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>195</u>	<u>310</u>	_____	_____

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

LAND 30' CSG AT 301'. UNLATCH FROM CASING AND DRILL AHEAD WITH 26" BIT AND MUD MOTOR TO 915'. MONITORING WELL VIA GAS LIFT TO SHALE SHAKERS. BACKGROUND GAS 4-6 UNITS. MAX GAS 8 UNITS.

ADT _____ DON WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 1030
 OPERATION DRLG
 FOOTAGE 115

NO. 3
 DATE Jul 31 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>5</u>	MAX GAS (units) <u>9</u>	AT DEPTH (feet) _____	SURVEY DATA <u>1030 1.5 Deg</u>
BACKGROUND CONNECTION TRIP _____	FLOWLINE TEMP <u>NA</u> degrees F	LITHOLOGY <u>NA</u>	SAMPLE DEPTH _____
		TRIP CHLORIDES _____	DRILL RATE ft/hr <u>30</u>
		LAG DOWN DP _____	CORRECTED 'D' EXP. _____
		LAG OFF BOTTOM <u>NA</u>	SHALE DENSITY g/cc _____
			EWR Res. _____

FORMATION PRESSURE DATA

CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE <u>133</u> psi	<u>8.5</u> ppg	<u>404</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE <u>NA</u> psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg
ECD _____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME _____	BIT NO. <u>1</u>	PUMPS <u>1.</u> <u>ID1600</u> <u>2.</u> <u>ID1600</u>
TYPE <u>SEA WATER</u>	TYPE <u>ATXG1</u>	SIZE inches <u>7.5x12</u> <u>7.5x12</u>
WEIGHT IN <u>8.5</u>	IADC CODE _____	CAPACITY gal/stk <u>6.54</u> <u>6.54</u>
FUNNEL VIS. _____	SIZE <u>26</u>	PUMP RATE stks/min _____
PV/YP _____	JETS <u>3-21.1-22</u>	FLOW RATE gal/min _____
GELS _____	DEPTH OUT <u>1030</u>	PRESSURE psi <u>STATIC</u>
pH _____	ROT HRS. <u>36.3</u>	PD SURF / DS psi _____
FILT/CAKE API _____	FOOTAGE <u>819</u>	ANN / BIT psi _____
HP-HT _____	AVG ft/hr <u>22.5</u>	JET VELOCITY ft/sec _____
P _m _____	GRADE _____	JET IMPACT lbs _____
P _f /M _f _____	HOLE DEV. <u>1.5</u>	BIT HP _____
CHLORIDES ppm _____	COST/FT <u>1028</u>	HP RATIO / HP/IN2 _____
CALCIUM ppm _____	RPM <u>111</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS _____	WOB <u>21</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>20X30</u>	<u>101</u>	<u>.4857</u>	_____	_____	_____
<u>20X26</u>	<u>704</u>	<u>.2681</u>	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____
_____	_____	_____	_____	_____	_____

PIPE DATA

	DRILL STRING				CASING:			
	DP	HWDP	DC		DEPTH			
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>9.5</u>	_____	<u>301</u>	<u>1017</u>	_____	_____
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>30</u>	<u>20</u>	_____	_____
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>28</u>	<u>18.75</u>	_____	_____
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0707</u>	_____	<u>.7616</u>	<u>.3408</u>	_____	_____
LENGTH-ft	_____	_____	_____	_____	<u>90</u>	<u>805</u>	_____	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>195</u>	_____	<u>310</u>	<u>133</u>	_____	_____

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

DRILL AHEAD WITH 26" BIT AND MUD MOTOR TO 1030'. PUMP SWEEP. DROP SURVEY. SHORT TRIP TO 375'. RIH. CIRC HOLE UNTIL AIRFILT CLEAN. DISPLACE HOLE WITH 9.9 ppg MUD. POOH. RIG UP TO RUN 20" CSG. RUN 19 JTS OF 133 LB/FT 20" CSG. LAND CSG AT 1017'. CMT 20 AND 30 INCH CASING TO MUD LINE.

ADT _____ DON WALTERS

sperry-sun *LOGGING SYSTEMS*
DRILLING SERVICES
 A Baroid Company

DEPTH 1030
 OPERATION RIG BOPS
 FOOTAGE 0

NO. 4
 DATE Aug 1 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) _____	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>1030 1.5 Deg</u>
BACKGROUND _____	CONNECTION _____	TRIP _____	LITHOLOGY <u>NA</u>
FLOWLINE TEMP <u>NA</u> degrees F	DRILL RATE ft/hr _____	CORRECTED 'D' EXP. _____	SAMPLE DEPTH _____
	SHALE DENSITY g/cc _____	EWR Res. _____	TRIP CHLORIDES _____
			LAG DOWN DP _____
			LAG OFF BOTTOM <u>NA</u>

FORMATION PRESSURE DATA

CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>450</u> psi <u>8.5</u> ppg	<u>455</u> psi <u>8.5</u> ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ ft
FRACTURE PRESSURE	<u>632</u> psi <u>11.8 est</u> ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ ft
ECD	_____ psi _____ ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2400 31 JUL 93</u>	BIT NO. <u>1</u>	PUMPS 1. <u>ID1600</u> 2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>ATXG1</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE _____	CAPACITY gal/stk <u>4.91</u> <u>4.91</u>
FUNNEL VIS. <u>90</u>	SIZE <u>26</u>	PUMP RATE stks/min _____
PV/YP <u>28/19</u>	JETS <u>3-21,1-22</u>	FLOW RATE gal/min _____
GELS <u>4/8</u>	DEPTH OUT <u>1030</u>	PRESSURE psi <u>STATIC</u>
pH <u>9.5</u>	ROT HRS. <u>36.3</u>	PD SURF / DS psi _____
FILT/CAKE API <u>5/1</u>	FOOTAGE <u>819</u>	ANN / BIT psi _____
HP-HT _____	AVG ft/hr <u>22.5</u>	JET VELOCITY ft/sec _____
P _m <u>1.8</u>	GRADE _____	JET IMPACT lbs _____
P _f /M _f <u>.5/1.8</u>	HOLE DEV. <u>1.5</u>	BIT HP _____
CHLORIDES ppm <u>17500</u>	COST/FT <u>1028</u>	HP RATIO / HP/IN2 _____
CALCIUM ppm <u>1560</u>	RPM <u>111</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>0/6.4/93.6</u>	WOB <u>21</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBL
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____
_____	_____	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING:			
	DP	HWDP	DC	DEPTH	301	1018	_____
OD-inches	<u>5.0</u>	<u>5.0</u>	_____	30	<u>20</u>	_____	_____
ID-inches	<u>4.276</u>	<u>3.0</u>	_____	28	<u>18.75</u>	_____	_____
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	_____	.7616	<u>.3408</u>	_____	_____
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	_____	90	<u>793</u>	_____	_____
LENGTH-ft	_____	_____	_____	310	<u>133</u>	_____	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	_____			_____	_____

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

FINISH CEMENTING 20" CSG TO MUD LINE. WOC. TEST IBOP VALVE. TEST CHOKE MANIFOLD. RIG UP TO RUN BOP STACK.

ADT DON WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 1040
 OPERATION TRIP
 FOOTAGE 10

NO. 5
 DATE Aug 2 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR ARCO ALASKA, INC. WELL NAME KUVLUM NO. 2 FIELD/BLOCK OCS BLK 672
 CONTRACTOR CANMAR RIG NAME KULLUK AREA BEAUFORT SEA
 START DATE Jul 28 93 LOC. OFFSHORE STATE ALASKA

LOGGING DATA

AVG GAS (units)	MAX GAS (units)	AT DEPTH (feet)	SURVEY DATA	<u>1030 1.5 Deg</u>	
			LITHOLOGY	<u>100% CLAY</u>	
BACKGROUND CONNECTION TRIP			SAMPLE DEPTH	<u>1040</u>	
			TRIP CHLORIDES		DRILL RATE ft/hr
			LAG DOWN DP		CORRECTED 'D' EXP.
FLOWLINE TEMP	<u>NA</u>	degrees F	LAG OFF BOTTOM	<u>NA</u>	SHALE DENSITY g/cc
					EWR Res.

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>450</u> psi	<u>8.5</u> ppg	<u>500</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg _____ ft
FRACTURE PRESSURE	<u>697</u> psi	<u>12.9</u> ppg	_____ psi	_____ ppg	_____ psi	_____ ppg _____ ft
ECD	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg _____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME	<u>2400 1 AUG 93</u>	BIT NO.	<u>3</u>	<u>2</u>	PUMPS	<u>1. ID1600</u>	<u>2. ID1600</u>
TYPE	<u>GENERIC #2</u>	TYPE	<u>FDTG</u>	<u>SS33SGJ4</u>	SIZE inches	<u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN	<u>9.8</u>	IADC CODE			CAPACITY gal/stk	<u>4.91</u>	<u>4.91</u>
FUNNEL VIS.	<u>50</u>	SIZE	<u>12.5</u>	<u>17.5</u>	PUMP RATE stks/min		
PV/YP	<u>19/26</u>	JETS	<u>3x14.1-10</u>	<u>3-18.1-11</u>	FLOW RATE gal/min		
GELS	<u>5/8</u>	DEPTH OUT		<u>1040</u>	PRESSURE psi	<u>STATIC</u>	
pH	<u>9.9</u>	ROT HRS.		<u>2.8</u>	PD SURF / DS psi		
FILT/CAKE API	<u>4.8/1</u>	FOOTAGE		<u>10</u>	ANN / BIT psi		
HP-HT	<u>-</u>	AVG ft/hr		<u>3.6</u>	JET VELOCITY ft/sec		
Pm	<u>2.2</u>	GRADE			JET IMPACT lbs		
Pf/Mf	<u>.5/1.81.1/2.9</u>	HOLE DEV.		<u>1.5</u>	BIT HP		
CHLORIDES ppm	<u>17000</u>	COST/FT		<u>4019</u>	HP RATIO / HP/IN2		
CALCIUM ppm	<u>400</u>	RPM		<u>64</u>	REDUCED 1 _____ psi at _____ stk/min		
OIL/WATER/SOLIDS	<u>0/5.6/94.4</u>	WOB		<u>8</u>	RATE 2 _____ psi at _____ stk/min		
DAILY/CUM. COST							

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>8X12.5</u>		<u>.0836</u>			
<u>5X12.5</u>		<u>.1215</u>			
<u>5X17.5</u>		<u>.2733</u>			
<u>5X18.75</u>		<u>.3083</u>			
<u>5X20</u>		<u>.3644</u>			

PIPE DATA

	DRILL STRING			CASING:		
	DP	HWDP	DC	DEPTH		
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>301</u>	<u>1018</u>	
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>30</u>	<u>20</u>	
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>28</u>	<u>18.75</u>	
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>.7616</u>	<u>.3408</u>	
LENGTH-ft		<u>656</u>	<u>384</u>	<u>90</u>	<u>793</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	<u>310</u>	<u>133</u>	

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

RIG UP STACK AND DIVERTER. RUN STACK AND DIVERTER TO PBG. TEST STACK. RIH AND TEST CASING TO 2200 psi. POOH. PICK UP BHA AND 17.5' BIT. RIH. TAG CMT AT 993'. DRILL CMT TO 1008'. CHANGE HOLE OVER TO 9.8 ppg GENERIC #2 MUD. DRILL CMT. SHOE AND 10' OF NEW HOLE. PERFORM LEAK OFF TEST-170 psi-12.9 ppg. POOH. LAY DOWN BHA AND 17.5' BIT. PICK UP NEW BHA. MWD TOOL AND 12.25' BIT NO. 3.

ADT DON WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 2275
 OPERATION DRILL
 FOOTAGE 1225

NO. 6
 DATE Aug 3 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>14</u>	MAX GAS (units) <u>28</u>	AT DEPTH (feet) <u>1185</u>	SURVEY DATA <u>.24 Deg at 2210'</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>0</u>	FLOWLINE TEMP <u>33</u> degrees F	LITHOLOGY <u>90 % CLAY 10% SAND</u>
			SAMPLE DEPTH <u>2200</u>
			TRIP CHLORIDES _____
			LAG DOWN DP <u>252 stks</u>
			LAG OFF BOTTOM <u>4015 stks</u>
			DRILL RATE ft/hr <u>100</u>
			CORRECTED 'D' EXP. <u>0.79</u>
			SHALE DENSITY g/cc _____
			EWR Res. <u>2</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>450</u> psi	<u>8.5</u> ppg	<u>1010</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>697</u> psi	<u>12.9</u> ppg	_____ psi	_____ ppg	_____ psi	_____ ppg
ECD	<u>524</u> psi	<u>9.9</u> ppg	<u>1175</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2400 1 AUG 93</u>	BIT NO. <u>3</u>	PUMPS 1. <u>ID1600</u> 2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTG</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE _____	CAPACITY gal/stk <u>4.91</u> <u>4.91</u>
FUNNEL VIS. <u>50</u>	SIZE <u>12.5</u>	PUMP RATE stks/min <u>68</u> <u>68</u>
PV/YP <u>24/21</u>	JETS <u>3x14.1-10</u>	FLOW RATE gal/min <u>334</u> <u>334</u>
GELS <u>4/5</u>	DEPTH OUT _____	PRESSURE psi <u>2040</u>
pH <u>9.6</u>	ROT HRS. <u>14.4</u>	PD SURF / DS psi <u>93/862</u>
FILT/CAKE API <u>4.6/1</u>	FOOTAGE <u>1235</u>	ANN / BIT psi <u>11/1436</u>
HP-HT _____	AVG ft/hr <u>85</u>	JET VELOCITY ft/sec <u>405</u>
P _m <u>1.3</u>	GRADE _____	JET IMPACT lbs <u>1368</u>
P _f /M _f <u>.8/1.7</u>	HOLE DEV. <u>.24</u>	BIT HP <u>558</u>
CHLORIDES ppm <u>16000</u>	COST/FT _____	HP RATIO / HP/IN2 <u>4.7hp/in2</u>
CALCIUM ppm <u>840</u>	RPM <u>125</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>0/6.3/93.7</u>	WOB <u>9</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

	LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
8X12.5	<u>384</u>	<u>.0836</u>	<u>191</u>	<u>319</u>	<u>34</u>
5X12.5	<u>851</u>	<u>.1215</u>	<u>131</u>	<u>261</u>	<u>104</u>
5X17.5	<u>22</u>	<u>.2733</u>	<u>58</u>	<u>213</u>	<u>6</u>
5X18.75	<u>853</u>	<u>.3083</u>	<u>50</u>	<u>223</u>	<u>270</u>
5X20	<u>165</u>	<u>.3644</u>	<u>44</u>	<u>216</u>	<u>60</u>

PIPE DATA

	DRILL STRING			CASING:			
	DP	HWDP	DC	DEPTH	301	1018	
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>		<u>30</u>	<u>20</u>	
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>28</u>	<u>18.75</u>	
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>		<u>.7616</u>	<u>.3408</u>	
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>				
LENGTH-ft	<u>1170</u>	<u>656</u>	<u>384</u>		<u>90</u>	<u>793</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>		<u>310</u>	<u>133</u>	

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

RUN IN HOLE WITH 12.25" BIT NO. 3. DRILL AHEAD THRU CLAY/SAND WHILE CONTROL DRILLING AT 100ft/hr TO 2275'. NO APPARENT HOLE PROBLEMS.

ADT DON WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 3545
 OPERATION DRILL
 FOOTAGE 1280

No. 7
 DATE Aug 4 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>16</u>	MAX GAS (units) <u>27</u>	AT DEPTH (feet) <u>2315</u>	SURVEY DATA <u>.40 at 3441'</u>	LITHOLOGY <u>60 % CLAY 40% SILTSTONE</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>61</u>	FLOWLINE TEMP <u>34</u> degrees F	SAMPLE DEPTH <u>3440</u>	TRIP CHLORIDES _____
			LAG DOWN DP <u>445 stks</u>	DRILL RATE ft/hr <u>103</u>
			LAG OFF BOTTOM <u>5420 stks</u>	CORRECTED 'D' EXP. <u>1.10</u>
				SHALE DENSITY g/cc _____
				EWR Res. <u>2</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>450</u> psi	<u>8.5</u> ppg	<u>1601</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>697</u> psi	<u>12.9</u> ppg	<u>2577</u> psi	<u>14</u> ppg	_____ psi	_____ ppg
ECD	<u>529</u> psi	<u>10.0</u> ppg	<u>1840</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2400 3 AUG 93</u>	BIT NO. <u>3</u>	PUMPS <u>1.</u> <u>ID1600</u>	<u>2.</u> <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTG</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE _____	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>54</u>	SIZE <u>12.5</u>	PUMP RATE stks/min <u>72</u>	<u>71</u>
PV/YP <u>27/23</u>	JETS <u>3x14,1-10</u>	FLOW RATE gal/min <u>353</u>	<u>349</u>
GELS <u>3/5</u>	DEPTH OUT _____	PRESSURE psi _____	<u>2390</u>
pH <u>9.5</u>	ROT HRS. <u>28.6</u>	PD SURF / DS psi _____	<u>103/1139</u>
FILT/CAKE API <u>4/1</u>	FOOTAGE <u>2505</u>	ANN / BIT psi _____	<u>20/1599</u>
HP+HT _____	AVG ft/hr <u>85</u>	JET VELOCITY ft/sec _____	<u>427</u>
P _m <u>1.3/1</u>	GRADE _____	JET IMPACT lbs _____	<u>1524</u>
Pf/Mf <u>.6/1.5</u>	HOLE DEV. <u>.40</u>	BIT HP _____	<u>656</u>
CHLORIDES ppm <u>16000</u>	COST/FT _____	HP RATIO / HP/IN2 _____	<u>5.6hp/in2</u>
CALCIUM ppm <u>1200</u>	RPM <u>118</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>0/8/92</u>	WOB <u>30</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____			

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>8X12.5</u>	<u>384</u>	<u>.0836</u>	<u>200</u>	<u>339</u>	<u>34</u>
<u>5X12.5</u>	<u>2121</u>	<u>.1215</u>	<u>138</u>	<u>277</u>	<u>257</u>
<u>5X17.5</u>	<u>22</u>	<u>.2733</u>	<u>61</u>	<u>225</u>	<u>6</u>
<u>5X18.75</u>	<u>853</u>	<u>.3083</u>	<u>53</u>	<u>236</u>	<u>270</u>
<u>5X20</u>	<u>165</u>	<u>.3644</u>	<u>46</u>	<u>228</u>	<u>60</u>

PIPE DATA

	DRILL STRING			CASING:			
	DP	HWDP	DC	DEPTH	301	1018	
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>		<u>30</u>	<u>20</u>	
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>28</u>	<u>18.75</u>	
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>		<u>.7616</u>	<u>.3408</u>	
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>				
LENGTH-ft	<u>2503</u>	<u>656</u>	<u>384</u>		<u>90</u>	<u>793</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>		<u>310</u>	<u>133</u>	

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

DRILL AHEAD THRU CLAY/SAND TO 2430'. CIRC OUT. SHORT TRIP TO SHOE. FLOW CHECK EVERY 10 STANDS. HOLE PULLED TIGHT AT 1786'.
 RIH. REAM FROM 1729-1761'. WASH TO BOTTOM FROM 2380'. NO FILL. CBU AFTER TRIP. MAX GAS 61u. DRILL AHEAD TO 3545'. NO APPARENT PROBLEMS.

ADT DON WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 4005
 OPERATION CIRC
 FOOTAGE 460

NO. 8
 DATE Aug 5 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR ARCO ALASKA, INC. WELL NAME KUVLUM NO. 2 FIELD/BLOCK OCS BLK 672
 CONTRACTOR CANMAR RIG NAME KULLUK AREA BEAUFORT SEA
 START DATE Jul 28 93 LOC. OFFSHORE STATE ALASKA

LOGGING DATA

AVG GAS (units)	MAX GAS (units)	AT DEPTH (feet)	SURVEY DATA	<u>.39 at 3977</u>
BACKGROUND CONNECTION TRIP	<u>16</u>	<u>39</u>	LITHOLOGY	<u>60 % CLAY 30% SILTSTONE 10% SAND</u>
FLOWLINE TEMP		<u>3775</u>	SAMPLE DEPTH	<u>4005</u>
			TRIP CHLORIDES	
			LAG DOWN DP	
			LAG OFF BOTTOM	
			DRILL RATE ft/hr	
			CORRECTED 'D' EXP.	
			SHALE DENSITY g/cc	
			EWR Res.	

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE
PORE PRESSURE	<u>450</u> psi	<u>8.5</u> ppG	<u>1601</u> psi	<u>8.7</u> ppG	_____ psi _____ ppG _____ ft
FRACTURE PRESSURE	<u>697</u> psi	<u>12.9</u> ppG	<u>2577</u> psi	<u>14</u> ppG	_____ psi _____ ppG _____ ft
ECD	_____ psi	_____ ppG	_____ psi	_____ ppG	_____ psi _____ ppG _____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME	<u>2400 4 AUG 93</u>	BIT NO.	<u>3</u>	PUMPS	1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE	<u>GENERIC #2</u>	TYPE	<u>FDTG</u>	SIZE inches	<u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN	<u>9.8</u>	IADC CODE		CAPACITY gal/stk	<u>4.91</u>	<u>4.91</u>
FUNNEL VIS.	<u>52</u>	SIZE	<u>12.5</u>	PUMP RATE stks/min		
PV/YP	<u>24/22</u>	JETS	<u>3x14.1-10</u>	FLOW RATE gal/min		
GELS	<u>3/5</u>	DEPTH OUT	<u>4005</u>	PRESSURE psi		
pH	<u>9.5</u>	ROT HRS.	<u>33.7</u>	PD SURF / DS psi		
FILT/CAKE API	<u>4.2/1</u>	FOOTAGE	<u>2966</u>	ANN / BIT psi		
HP-HT		AVG ft/hr	<u>88</u>	JET VELOCITY ft/sec		
P _m	<u>1.8</u>	GRADE		JET IMPACT lbs		
Pf/Mf	<u>.6/1.9</u>	HOLE DEV.	<u>.39</u>	BIT HP		
CHLORIDES ppm	<u>16000</u>	COST/FT	<u>311</u>	HP RATIO / HP/IN2		
CALCIUM ppm	<u>800</u>	RPM	<u>122</u>	REDUCED 1 _____ psi at _____ stk/min		
OIL/WATER/SOLIDS	<u>0/92.2/7.8</u>	WOB	<u>14</u>	RATE 2 _____ psi at _____ stk/min		
DAILY/CUM. COST						

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
5X20	<u>165</u>	<u>.3644</u>			
5X18.75	<u>853</u>	<u>.3083</u>			
5X17.5	<u>22</u>	<u>.2733</u>			
5X12.5	<u>2121</u>	<u>.1215</u>			
8X12.5	<u>384</u>	<u>.0836</u>			

PIPE DATA

	DRILL STRING			CASING:		
	DP	HWDP	DC	DEPTH	301	1018
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>		<u>30</u>	<u>20</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>28</u>	<u>18.75</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>		<u>.7616</u>	<u>.3408</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>			
LENGTH-ft	<u>2503</u>	<u>656</u>	<u>384</u>		<u>90</u>	<u>793</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>		<u>310</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

DRILL AHEAD THRU CLAY/SILTSTONE/SAND TO 4005'. CIRC OUT. POOH. PUMP AND BACK REAM FROM 3651' TO 1016'. MAX OVERPULL 60 K.
 LAY DOWN MWD TOOL. RIH. CBU. MAX GAS 85u. CIRC AND CONDITION HOLE. POOH FOR E LOGS.

ADT _____ DON WALTERS

sperry-sun **LOGGING SYSTEMS**
 DRILLING SERVICES
 A Baroid Company

DEPTH 4005
 OPERATION E-LOG
 FOOTAGE 0

No. 9
 DATE Aug 6 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR ARCO ALASKA, INC. WELL NAME KUVLUM NO. 2 FIELD/BLOCK OCS BLK 672 NR6-4
 CONTRACTOR CANMAR RIG NAME KULLUK AREA BEAUFORT SEA
 START DATE Jul 28 93 LOC. OFFSHORE STATE ALASKA

LOGGING DATA

AVG GAS (units)	MAX GAS (units)	AT DEPTH (feet)	SURVEY DATA	<u>.39 at 3977</u>	
BACKGROUND	CONNECTION	TRIP	LITHOLOGY	<u>60 % CLAY 30% SILTSTONE 10% SAND</u>	
FLOWLINE TEMP	<u>0</u>	<u>0</u>	SAMPLE DEPTH	<u>4005</u>	
	<u>85</u>	<u>4005</u>	TRIP CHLORIDES	<u>NA</u>	
	<u>NA</u>	<u>degrees F</u>	LAG DOWN DP	<u>520</u>	
			LAG OFF BOTTOM	<u>5900</u>	
			DRILL RATE ft/hr	<u>NA</u>	
			CORRECTED 'D' EXP.	<u>NA</u>	
			SHALE DENSITY g/cc	<u>NA</u>	
			EWR Res.	<u>NA</u>	

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>450</u>	psi	<u>8.5</u>	ppg	<u>1601</u>	psi
FRACTURE PRESSURE	<u>697</u>	psi	<u>12.9</u>	ppg	<u>2577</u>	psi
ECD		psi		ppg		psi

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME	<u>2400 AUG 5 93</u>	BIT NO.	<u>3</u>	PUMPS	<u>1. ID1600</u>	<u>2. ID1600</u>
TYPE	<u>GENERIC #2</u>	TYPE	<u>FDTG</u>	SIZE inches	<u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN	<u>9.8</u>	IADC CODE		CAPACITY gal/stk	<u>4.91</u>	<u>4.91</u>
FUNNEL VIS.	<u>52</u>	SIZE	<u>12.5</u>	PUMP RATE stks/min		
PV/YP	<u>24/22</u>	JETS	<u>3x14.1-10</u>	FLOW RATE gal/min		
GELS	<u>3/5</u>	DEPTH OUT	<u>4005</u>	PRESSURE psi	<u>STATIC PAST</u>	
pH	<u>9.5</u>	ROT HRS.	<u>33.7</u>	PD SURF / DS psi	<u>24 HRS</u>	
FILT/CAKE API	<u>3.8/1</u>	FOOTAGE	<u>2966</u>	ANN / BIT psi		
HP-HT		AVG ft/hr	<u>88</u>	JET VELOCITY ft/sec		
Pm	<u>1.8</u>	GRADE		JET IMPACT lbs		
Pf/Mf	<u>.8/1.9</u>	HOLE DEV.	<u>.39</u>	BIT HP		
CHLORIDES ppm	<u>16000</u>	COST/FT	<u>311</u>	HP RATIO / HP/IN2		
CALCIUM ppm	<u>200</u>	RPM	<u>122</u>	REDUCED 1	psi at	stk/min
OIL/WATER/SOLIDS	<u>0/92.2/7.8</u>	WOB	<u>14</u>	RATE 2	psi at	stk/min
DAILY/CUM. COST						

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>165</u>	<u>.3644</u>			
<u>5X18.75</u>	<u>853</u>	<u>.3083</u>			
<u>5X17.5</u>	<u>22</u>	<u>.2733</u>			
<u>5X12.5</u>	<u>2121</u>	<u>.1215</u>			
<u>8X12.5</u>	<u>384</u>	<u>.0836</u>			

PIPE DATA

	DRILL STRING			CASING: DEPTH		
	DP	HWDP	DC	301	1018	
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>30</u>	<u>20</u>	
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>28</u>	<u>18.75</u>	
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.7616</u>	<u>.3408</u>	
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>			
LENGTH-ft	<u>2503</u>	<u>656</u>	<u>384</u>	<u>90</u>	<u>793</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	<u>310</u>	<u>133</u>	

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 800 JETS 4-14'S ft/mi = NA sec/std

POOH FOR E-LOGS. HOLE PULLED WITHOUT EXCESS DRAG. RIG UP SCHLUMBERGER. RUN ELECTRIC LOGS.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 2905
 OPERATION OPEN HOLE
 FOOTAGE 1887

No. 10
 DATE Aug 7 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>5-10</u>	MAX GAS (units) <u>22</u>	AT DEPTH (feet) <u>2360</u>	SURVEY DATA <u>.39 at 3977</u>	LITHOLOGY <u>60 % CLAY 30% SILTSTONE 10% SAND</u>
BACKGROUND CONNECTION TRIP <u>0</u>	TRIP CHLORIDES <u>NA</u>	LAG DOWN DP <u>375</u>	LAG OFF BOTTOM <u>7100</u>	SAMPLE DEPTH <u>4005</u>
FLOWLINE TEMP <u>NA</u> degrees F	DRILL RATE ft/hr <u>375</u>	CORRECTED 'D' EXP. <u>.66</u>	SHALE DENSITY g/cc <u>-</u>	EWR Res. <u>-</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>450</u> psi	<u>8.5</u> ppG	<u>1601</u> psi	<u>8.7</u> ppG	_____ psi	_____ ppG
FRACTURE PRESSURE	<u>697</u> psi	<u>12.9</u> ppG	<u>3020</u> psi	<u>14.5</u> ppG	_____ psi	_____ ppG
ECD	<u>518</u> psi	<u>9.8</u> ppG	_____ psi	_____ ppG	_____ psi	_____ ppG

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 6 93</u>	BIT NO. <u>3</u>	RR3	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTC</u>	<u>FDTC/H.O.</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE _____	_____	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>65</u>	SIZE <u>12.25</u>	<u>12.25/17.5</u>	PUMP RATE stks/min <u>115</u>	<u>115</u>
PV/YP <u>26/30</u>	JETS <u>3x14.1-10</u>	<u>TFA:1.44</u>	FLOW RATE gal/min <u>1132</u>	_____
GELS <u>3/6</u>	DEPTH OUT <u>4005</u>	<u>NA</u>	PRESSURE psi <u>2200</u>	_____
pH <u>9.2</u>	ROT HRS. <u>33.7</u>	<u>4.2</u>	PD SURF / DS psi <u>100/1545</u>	_____
FILT/CAKE API <u>4.2 - 1/32</u>	FOOTAGE <u>2966</u>	<u>1887</u>	ANN / BIT psi <u>5/550</u>	_____
HP-HT _____	AVG ft/hr <u>88</u>	<u>449</u>	JET VELOCITY ft/sec <u>250</u>	_____
P _m <u>1.3</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u>1440</u>	_____
Pf/Mf <u>.5/1.6</u>	HOLE DEV. <u>.39</u>	_____	BIT HP <u>365</u>	_____
CHLORIDES ppm <u>16000</u>	COST/FT <u>311</u>	<u>NA</u>	HP RATIO / HP/IN2 <u>28% - 1.5/IN2</u>	_____
CALCIUM ppm <u>600</u>	RPM <u>122</u>	<u>150</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>0/91.7/8.3</u>	WOB <u>14</u>	<u>10-20</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____	_____	_____	_____	_____

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>165</u>	<u>.3644</u>	<u>74</u>	<u>241</u>	_____
<u>5X18.75</u>	<u>853</u>	<u>.3083</u>	<u>85</u>	<u>249</u>	_____
<u>5X17.5</u>	<u>1587</u>	<u>.2733</u>	<u>99</u>	<u>238</u>	_____
<u>5X12.25</u>	_____	<u>.1215</u>	_____	_____	_____
<u>8X17.5</u>	<u>300</u>	<u>.2354</u>	<u>115</u>	<u>263</u>	_____

PIPE DATA

	DRILL STRING			CASING:			
	DP	HWDP	DC	DEPTH			
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>301</u>	<u>1018</u>	_____	_____
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>30</u>	<u>20</u>	_____	_____
CAP-bbbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.7616</u>	<u>.3408</u>	_____	_____
DISP-bbbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	_____	_____	_____	_____
LENGTH-ft	<u>2179</u>	<u>426</u>	<u>300</u>	<u>90</u>	<u>793</u>	_____	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	<u>310</u>	<u>133</u>	_____	_____

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM _____ JETS _____ ft/mi = _____ sec/std

RUN ELECTRIC LOGS. MAKE UP NEW BOTTOM HOLE ASSEMBLY RR BIT 3 AND A 17.5' HOLE OPENER. RIH TO BOTTOM OF 20" CASING.

OPEN HOLE TO 17.5' FOR NEXT CASING RUN. GOOD PENETRATION RATES WHILE REAMING.

ADT _____ J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 4005
 OPERATION CIRCULATE
 FOOTAGE 1100

No. 11
 DATE Aug 8 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>5</u>	MAX GAS (units) <u>28</u>	AT DEPTH (feet) <u>3850</u>	SURVEY DATA <u>.39 at 3977</u>	LITHOLOGY <u>60% CLAY 30% SILTSTONE 10% SAND</u>
BACKGROUND CONNECTION TRIP <u>0</u>	TRIP <u>60</u>	AT DEPTH <u>4005</u>	SAMPLE DEPTH <u>4005</u>	TRIP CHLORIDES <u>550</u>
FLOWLINE TEMP <u>48</u> degrees F			LAG DOWN DP <u>9700</u>	LAG OFF BOTTOM <u>9700</u>
			DRILL RATE ft/hr <u>140</u>	CORRECTED 'D' EXP. <u>90</u>
				SHALE DENSITY g/cc <u>-</u>
				EWR Res. <u>-</u>

FORMATION PRESSURE DATA

CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE <u>450</u> psi	<u>8.5</u> ppG	<u>1601</u> psi	<u>8.7</u> ppG	<u>-</u> psi	<u>-</u> ppG
FRACTURE PRESSURE <u>697</u> psi	<u>12.9</u> ppG	<u>3020</u> psi	<u>14.5</u> ppG	<u>-</u> psi	<u>-</u> ppG
ECD <u>518</u> psi	<u>9.84</u> ppG	<u>2051</u> psi	<u>9.85</u> ppG	<u>-</u> psi	<u>-</u> ppG

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 7 93</u>	BIT NO. <u>3</u>	RR3	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTC</u>	<u>FDTC/H.O.</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE <u>-</u>		CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>52</u>	SIZE <u>12.25</u>	<u>12.25/17.5</u>	PUMP RATE stks/min <u>115</u>	<u>115</u>
PV/YP <u>24/26</u>	JETS <u>3x14.1-10</u>	<u>TFA:1.44</u>	FLOW RATE gal/min <u>1132</u>	
GELS <u>3/4</u>	DEPTH OUT <u>4005</u>	<u>4005</u>	PRESSURE psi <u>2475</u>	
pH <u>9.3</u>	ROT HRS. <u>33.7</u>	<u>10.1</u>	PD SURF / DS psi <u>100/1815</u>	
FILT/CAKE API <u>5.2 - 1/32</u>	FOOTAGE <u>2966</u>	<u>2987</u>	ANN / BIT psi <u>10/550</u>	
HP-HT <u>-</u>	AVG ft/hr <u>88</u>	<u>294</u>	JET VELOCITY ft/sec <u>250</u>	
P _m <u>1.2</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u>1440</u>	
P _f /M _f <u>.4/1.6</u>	HOLE DEV. <u>.39</u>		BIT HP <u>365</u>	
CHLORIDES ppm <u>16000</u>	COST/FT <u>311</u>	<u>NA</u>	HP RATIO / HP/IN2 <u>28% - 1.5/IN2</u>	
CALCIUM ppm <u>680</u>	RPM <u>122</u>	<u>145</u>	REDUCED 1 <u>-</u> psi at <u>-</u> stk/min	
OIL/WATER/SOLIDS <u>0/91.7/8.3</u>	WOB <u>14</u>	<u>10-20</u>	RATE 2 <u>-</u> psi at <u>-</u> stk/min	
DAILY/CUM. COST <u>-</u>				

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>171</u>	<u>.3644</u>	<u>74</u>	<u>221</u>	<u>-</u>
<u>5X18.75</u>	<u>847</u>	<u>.3083</u>	<u>85</u>	<u>229</u>	<u>-</u>
<u>5X17.5</u>	<u>2687</u>	<u>.2733</u>	<u>99</u>	<u>218</u>	<u>-</u>
<u>5X12.25</u>	<u>-</u>	<u>.1215</u>	<u>-</u>	<u>-</u>	<u>-</u>
<u>8X17.5</u>	<u>300</u>	<u>.2354</u>	<u>115</u>	<u>243</u>	<u>-</u>

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches <u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>8</u>	<u>171</u>	<u>301</u>	<u>1018</u>	<u>-</u>
ID-inches <u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>2.875</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>-</u>
CAP-bbls/ft <u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.0076</u>	<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>-</u>
DISP-bbls/ft <u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>.0545</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>-</u>
LENGTH-ft <u>3279</u>	<u>426</u>	<u>300</u>	<u>300</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>-</u>
WEIGHT-lbs/ft <u>19.5</u>	<u>49</u>	<u>149</u>	<u>149</u>	<u>170.5</u>	<u>95</u>	<u>812</u>	<u>-</u>
					<u>310</u>	<u>133</u>	<u>-</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM - JETS - 13 3/8" CSG 160 ft/mi = 15 sec/std

OPEN HOLE TO 17.5' TO 4005'. CBU. SHORT TRIP TO SHOE. TIGHT HOLE CONDITIONS NOTED ON THE WAY OUT WITH THE HOLE TRYING TO SWAB. BACK REAM TO KEEP FROM SWABBING. WASH AND REAM TO BOTTOM. GAS FROM BOTTOM ON SHORT TRIP = 60 UNITS.

CIRCULATE AND CONDITION HOLE FOR RUNNING CASING.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 4005
 OPERATION CEMENT
 FOOTAGE 0

No. 12
 DATE Aug 9 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARGO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>5</u>	MAX GAS (units) <u>10</u>	AT DEPTH (feet) <u>4005</u>	SURVEY DATA <u>.39 at 3977</u>	LITHOLOGY <u>60% CLAY 30% SILTSTONE 10% SAND</u>	SAMPLE DEPTH <u>4005</u>	DRILL RATE ft/hr <u>NA</u>
BACKGROUND CONNECTION TRIP <u>0</u>	TRIP <u>10</u>	LAG DOWN DP <u>4905</u>	LAG OFF BOTTOM <u>4850</u>	CORRECTED 'D' EXP. <u>NA</u>	SHALE DENSITY g/cc <u>-</u>	EWR Res. <u>-</u>
FLOWLINE TEMP <u>48</u> degrees F						

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>450</u> psi	<u>8.5</u> ppg	<u>1601</u> psi	<u>8.7</u> ppg	<u> </u> psi	<u> </u> ppg
FRACTURE PRESSURE	<u>697</u> psi	<u>12.9</u> ppg	<u>3020</u> psi	<u>14.5</u> ppg	<u> </u> psi	<u> </u> ppg
ECD	<u>524</u> psi	<u>9.9</u> ppg	<u>2082</u> psi	<u>10.0</u> ppg	<u> </u> psi	<u> </u> ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 8 93</u>	BIT NO. <u>3</u>	RR3	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTC</u>	<u>FDTC/H.O.</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE <u> </u>		CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>50</u>	SIZE <u>12.25</u>	<u>12.25/17.5</u>	PUMP RATE stks/min <u>87</u>	
PV/YP <u>23/21</u>	JETS <u>3x14.1-10</u>	<u>TFA:1.44</u>	FLOW RATE gal/min <u>427</u>	
GELS <u>3/4</u>	DEPTH OUT <u>4005</u>	<u>4005</u>	PRESSURE psi <u>410</u>	
pH <u>9.4</u>	ROT HRS. <u>33.7</u>	<u>10.1</u>	PD SURF / DS psi <u>50/355</u>	
FILT/CAKE API <u>3.8 - 1/32</u>	FOOTAGE <u>2966</u>	<u>2987</u>	ANN / BIT psi <u>5/-</u>	
HP-HT <u> </u>	AVG ft/hr <u>88</u>	<u>294</u>	JET VELOCITY ft/sec <u> </u>	
Pm <u>1.2</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u> </u>	
PF/Mf <u>.4/1.4</u>	HOLE DEV. <u>.39</u>		BIT HP <u> </u>	
CHLORIDES ppm <u>16000</u>	COST/FT <u>311</u>	<u>NA</u>	HP RATIO / HP/IN2 <u> </u>	
CALCIUM ppm <u>640</u>	RPM <u>122</u>	<u>145</u>	REDUCED 1 <u> </u> psi at <u> </u> stk/min	
OIL/WATER/SOLIDS <u>0/91.7/8.3</u>	WOB <u>14</u>	<u>10-20</u>	RATE 2 <u> </u> psi at <u> </u> stk/min	
DAILY/CUM. COST <u> </u>				

ANNULAR DATA

	LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>171</u>	<u>.3644</u>	<u>28</u>	<u>268</u>	<u> </u>
<u>13.375/18.75</u>	<u>847</u>	<u>.2038</u>	<u>61</u>	<u>367</u>	<u> </u>
<u>13.375/17.5</u>	<u>2959</u>	<u>.1238</u>	<u>82</u>	<u>371</u>	<u> </u>

PIPE DATA

	DRILL STRING			CASING: RISER COND. SURF.				
	DP	HWDP	DC	DEPTH	171	301	1018	3977
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>18.75</u>	<u>12.415</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>	<u>12.415</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>	<u>.024</u>
LENGTH-ft	<u> </u>	<u> </u>	<u> </u>	<u>170.5</u>	<u>95</u>	<u>812</u>	<u>3771</u>	<u>3771</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	<u>310</u>	<u>310</u>	<u>133</u>	<u>68</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 9.6 GPM 600 JETS 2-14,1-13 (OR 4-12'S) ft/mi = 15 sec/std
 POOH. RIG UP FOR RUNNING CASING. RUN AND LAND 68 LB/FT - 13 3/8" CASING TO 3977'. CIRCULATE TO CONDITION HOLE BEFORE
 CEMENTING. GOOD RETURNS NOTED WHILE RUNNING CASING. MAX GAS FROM BOTTOMS UP = 10 UNITS. PUMP AND DISPLACE APP. 480 BBL
 OF CEMENT AND SPACER.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 4005
 OPERATION RIH
 FOOTAGE 0

NO. 13
 DATE Aug 10 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) _____	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>.39 at 3977</u>
BACKGROUND <u>0</u>	CONNECTION <u>0</u>	TRIP <u>10</u>	LITHOLOGY <u>60% CLAY 30% SILTSTONE 10% SAND</u>
FLOWLINE TEMP <u>48</u> degrees F	SAMPLE DEPTH <u>4005</u>	TRIP CHLORIDES _____	DRILL RATE ft/hr <u>NA</u>
	LAG DOWN DP <u>570</u>	LAG OFF BOTTOM <u>4850</u>	CORRECTED 'D' EXP. <u>NA</u>
			SHALE DENSITY g/cc _____
			EWR Res. _____

FORMATION PRESSURE DATA

CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi <u>8.7</u> ppG	<u>1601</u> psi <u>8.7</u> ppG	_____ psi _____ ppG	_____ psi _____ ppG	_____ ft
FRACTURE PRESSURE	_____ psi <u>NA</u> ppG	<u>3020</u> psi <u>14.5</u> ppG	_____ psi _____ ppG	_____ psi _____ ppG	_____ ft
ECD	_____ psi _____ ppG	_____ psi _____ ppG	_____ psi _____ ppG	_____ psi _____ ppG	_____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 9 93</u>	BIT NO. <u>4</u>	RR3	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTC</u>	<u>FDTC/H.O.</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE _____	_____	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>51</u>	SIZE <u>12.25</u>	<u>12.25/17.5</u>	PUMP RATE stks/min _____	_____
PV/YP <u>15/17</u>	JETS <u>4-12'S</u>	<u>TFA:1.44</u>	FLOW RATE gal/min _____	_____
GELS <u>3/4</u>	DEPTH OUT _____	<u>4005</u>	PRESSURE psi _____	<u>STATIC</u>
pH <u>9.2</u>	ROT HRS. _____	<u>10.1</u>	PD SURF / DS psi _____	_____
FILT/CAKE API <u>3.0 - 1/32</u>	FOOTAGE _____	<u>2987</u>	ANN / BIT psi _____	_____
HP-HT _____	AVG ft/hr _____	<u>294</u>	JET VELOCITY ft/sec _____	_____
Pm <u>1.0</u>	GRADE _____	<u>INC</u>	JET IMPACT lbs _____	_____
Pf/Mf <u>.3/1.5</u>	HOLE DEV. _____	_____	BIT HP _____	_____
CHLORIDES ppm <u>16000</u>	COST/FT _____	<u>NA</u>	HP RATIO / HP/IN2 _____	_____
CALCIUM ppm <u>600</u>	RPM _____	<u>145</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>0/92/8</u>	WOB _____	<u>10-20</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	_____	_____	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	_____	<u>.1255</u>	_____	_____	_____
<u>8X13 3/8</u>	<u>DC-CSG</u>	_____	<u>.0876</u>	_____	_____	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	_____	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING				CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	_____	<u>171</u>	<u>301</u>	<u>1018</u>	<u>3977</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	_____	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	_____	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
LENGTH-ft	_____	<u>728</u>	<u>476</u>	_____	<u>170.5</u>	<u>95</u>	<u>812</u>	<u>3771</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	_____	_____	<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 9.6 GPM 600 JETS 2-14,1-13 (OR 4-12'S) _____ ft/mi = 15 sec/std

COMPLETE CEMENTING JOB. GOOD RETURNS NOTED WHILE CEMENTING. R/U SCHLUMBERGER. RUN VSP AND TEMPERATURE LOGS.

TEST BOP. MAKE UP NEW BIT AND BHA. RIH.

ADT J. PATTON

sperry-sun
DRILLING SERVICES *LOGGING SYSTEMS*
 A Baroid Company

DEPTH 5146
 OPERATION DRILLING
 FOOTAGE 1141

NO. 14
 DATE Aug 11 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>50</u>	MAX GAS (units) <u>229</u>	AT DEPTH (feet) <u>4585</u>	SURVEY DATA <u>.48 at 5043'</u>	LITHOLOGY <u>70 % CLAY 20% SILTSTONE 10% SAND</u>	SAMPLE DEPTH <u>5050</u>	TRIP CHLORIDES _____	DRILL RATE ft/hr <u>105</u>
BACKGROUND CONNECTION TRIP <u>105</u>	<u>229</u>	<u>4585</u>	LAG DOWN DP <u>685</u>	LAG OFF BOTTOM <u>5950</u>	CORRECTED 'D' EXP. <u>1.03</u>	SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>2.5</u>
FLOWLINE TEMP <u>80</u>	degrees F						

FORMATION PRESSURE DATA

CASING			BOTTOM HOLE			OPEN HOLE		
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>2382</u> psi	<u>8.9</u> ppg	_____ psi	_____ ppg	_____ ft	_____ ft
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>4094</u> psi	<u>15.3</u> ppg	_____ psi	_____ ppg	_____ ft	_____ ft
ECD	<u>2068</u> psi	<u>10.0</u> ppg	<u>2703</u> psi	<u>10.1</u> ppg	_____ psi	_____ ppg	_____ ft	_____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 10 93</u>	BIT NO. <u>4</u>	RR3	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTC</u>	<u>FDTC/H.O.</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8+</u>	IADC CODE _____		CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>58</u>	SIZE <u>12.25</u>	<u>12.25/17.5</u>	PUMP RATE stks/min <u>61</u>	<u>61</u>
PV/YP <u>19/19</u>	JETS <u>4-12'S</u>	<u>TFA:1.44</u>	FLOW RATE gal/min <u>600</u>	
GELS <u>3/4</u>	DEPTH OUT _____	<u>4005</u>	PRESSURE psi <u>2725</u>	
pH <u>9.9</u>	ROT HRS. <u>12.4</u>	<u>10.1</u>	PD SURF / DS psi <u>75/960</u>	
FILT/CAKE API <u>3.2 - 1/32</u>	FOOTAGE <u>1141</u>	<u>2987</u>	ANN / BIT psi <u>25/1865</u>	
HP-HT _____	AVG ft/hr <u>92</u>	<u>294</u>	JET VELOCITY ft/sec <u>435</u>	
P _m <u>1.0</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u>1325</u>	
Pf/Mf <u>.3/1.6</u>	HOLE DEV. <u>.48 @ 5043</u>		BIT HP <u>580</u>	
CHLORIDES ppm <u>17000</u>	COST/FT _____	<u>NA</u>	HP RATIO / HP/IN2 <u>61% - 5.0/IN2</u>	
CALCIUM ppm <u>860</u>	RPM <u>130</u>	<u>145</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>0/92/8</u>	WOB <u>25</u>	<u>10-20</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____				

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5X20 DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>39</u>	<u>210</u>	
<u>5X13 3/8 DP-CSG</u>	<u>728</u>	<u>.1255</u>	<u>114</u>	<u>265</u>	
<u>8X13 3/8 DC-CSG</u>	<u>3771</u>	<u>.0876</u>	<u>118</u>	<u>247</u>	
<u>8X12.25 DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>171</u>	<u>296</u>	

PIPE DATA

	DRILL STRING				CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>		<u>171</u>	<u>301</u>	<u>1018</u>	<u>3977</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>		<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>		<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
LENGTH-ft	<u>3970</u>	<u>728</u>	<u>476</u>		<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>		<u>170.5</u>	<u>95</u>	<u>812</u>	<u>3771</u>
						<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 600 JETS 2-14,1-13 (OR 4-12'S) _____ ft/mi = 15 sec/std

RIH WITH NB 4. TAG CEMENT AT 3889'. CBU. TEST CASING TO 3500 PSI. DRILL OUT CEMENT AND SHOE PLUS 10' OF NEW HOLE. CBU.

RUN EAK OFF TEST TO 14.9 PPG WITHOUT BREAKING DOWN FORMATION. DRILL AHEAD. CONNECTION GAS LOGGED BELOW 4300' AVERAGING

APP 50 UNITS OVER BACKGROUND. SLIGHT TREND NOTED ON PRESSURE PLOTS. RAISED PORE PRESSURE ESTIMATE TO 8.9 - 9.0 PPG.

DRILL AHEAD.

ADT _____ J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 5925
 OPERATION DRILLING
 FOOTAGE 779

No. 15
 DATE Aug 12 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>35</u>	MAX GAS (units) <u>250</u>	AT DEPTH (feet) <u>5220</u>	SURVEY DATA <u>1.19 at 5773'</u>	LITHOLOGY <u>60 % CLAY 30% SILTSTONE 10% SAND</u>
BACKGROUND CONNECTION TRIP <u>92</u>	TRIP <u>95</u>	LAG DOWN DP <u>805</u>	LAG OFF BOTTOM <u>6800</u>	DRILL RATE ft/hr <u>85</u>
FLOWLINE TEMP <u>94</u> degrees F				CORRECTED 'D' EXP. <u>1.18</u>
				SHALE DENSITY g/cc <u>NA</u>
				EWR Res. <u>2.5</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>2773</u> psi	<u>9.0</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>4837</u> psi	<u>15.7</u> ppg	_____ psi	_____ ppg
ECD	<u>2109</u> psi	<u>10.2</u> ppg	<u>3173</u> psi	<u>10.3</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 11 93</u>	BIT NO. <u>4</u>	RR3	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>FDTC</u>	<u>FDTC/H.O.</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.0</u>	IADC CODE _____		CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>55</u>	SIZE <u>12.25</u>	<u>12.25/17.5</u>	PUMP RATE stks/min <u>68</u>	<u>69</u>
PV/YP <u>20/23</u>	JETS <u>4-12'S</u>	<u>TFA:1.44</u>	FLOW RATE gal/min <u>670</u>	
GELS <u>3/6</u>	DEPTH OUT <u>4005</u>		PRESSURE psi <u>3450</u>	
pH <u>9.3</u>	ROT HRS. <u>21.4</u>	<u>10.1</u>	PD SURF / DS psi <u>100/1200</u>	
FILT/CAKE API <u>3.0 - 1/32</u>	FOOTAGE <u>1920</u>	<u>2987</u>	ANN / BIT psi <u>35/2115</u>	
HP-HT _____	AVG ft/hr <u>90</u>	<u>294</u>	JET VELOCITY ft/sec <u>487</u>	
Pm <u>.7</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u>1687</u>	
Pf/Mf <u>.15/1.4</u>	HOLE DEV. <u>1.19 @ 5773</u>		BIT HP <u>825</u>	
CHLORIDES ppm <u>17500</u>	COST/FT _____	<u>NA</u>	HP RATIO / HP/IN2 <u>61% - 7.0/IN2</u>	
CALCIUM ppm <u>680</u>	RPM <u>130</u>	<u>145</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>0/91.5/8.8</u>	WOB <u>45</u>	<u>10-20</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>44</u>	<u>246</u>	
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>127</u>	<u>302</u>	
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>1452</u>	<u>.1215</u>	<u>131</u>	<u>282</u>	
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>191</u>	<u>332</u>	

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>171</u>	<u>301</u>	<u>1018</u>	<u>3977</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
LENGTH-ft	<u>4721</u>	<u>728</u>	<u>476</u>	<u>170.5</u>	<u>95</u>	<u>812</u>	<u>3771</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>		<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.0 GPM 600 JETS 3-13,1-11 _____ ft/mi = 15 sec/std

CONTROL DRILL WITH BIT NO. 4. CONSISTANT CONECTION GAS READINGS AVERAGING ABOUT 50 UNITS ABOVE BACKGROUND.

DRILL TO 5525'. CBU. SHORT TRIP TO SHOE. HOLE TRYING TO SWAB WITH TIGHT HOLE ON THE WAY OUT. PUMP-BACKREAM OUT OFF THE HOLE. NO EXCESS DRAG NOTED ON WAY BACK IN. MAX GAS RECORDED WHILE DRILLING AHEAD AFTER GETTING BACK TO BOTTOM = 95 UNITS. DRILL AHEAD.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 6593
OPERATION POOH
FOOTAGE 668

NO. 16
DATE Aug 13 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>40</u>	MAX GAS (units) <u>125</u>	AT DEPTH (feet) <u>5220</u>	SURVEY DATA <u>1.40 at 6531'</u>
BACKGROUND CONNECTION TRIP FLOWLINE TEMP <u>94</u> degrees F	LITHOLOGY <u>80 % CLAY 20% SILTSTONE</u>	SAMPLE DEPTH <u>6580</u>	DRILL RATE ft/hr <u>45</u>
	TRIP CHLORIDES <u>905</u>	LAG DOWN DP <u>7250</u>	CORRECTED 'D' EXP. <u>1.32</u>
	LAG OFF BOTTOM <u>7250</u>	SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>3.5</u>

FORMATION PRESSURE DATA

CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi <u>8.7</u> ppg	<u>3120</u> psi <u>9.1</u> ppg			
FRACTURE PRESSURE	<u>3081</u> psi <u>14.9</u> ppg	<u>5383</u> psi <u>15.7</u> ppg			
ECD	<u>2109</u> psi <u>10.2</u> ppg	<u>3531</u> psi <u>10.3</u> ppg			

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 12 93</u>	BIT NO. <u>4</u>	RR3	PUMPS <u>1.</u> ID1600	ID1600
TYPE <u>GENERIC #2</u>	TYPE <u>FDTG</u>	FDTG/H.O.	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.0+</u>	IADC CODE		CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>59</u>	SIZE <u>12.25</u>	<u>12.25/17.5</u>	PUMP RATE stks/min <u>62</u>	<u>63</u>
PV/YP <u>22/28</u>	JETS <u>4-12'S</u>	TFA:1.44	FLOW RATE gal/min <u>615</u>	
GELS <u>5/9</u>	DEPTH OUT <u>6593</u>	<u>4005</u>	PRESSURE psi <u>3250</u>	
pH <u>9.1</u>	ROT HRS. <u>34.1</u>	<u>10.1</u>	PD SURF / DS psi <u>100/1320</u>	
FILT/CAKE API <u>2.7 - 1/32</u>	FOOTAGE <u>2588</u>	<u>2987</u>	ANN / BIT psi <u>50/1780</u>	
HP-HT	AVG ft/hr <u>76</u>	<u>294</u>	JET VELOCITY ft/sec <u>447</u>	
Pm <u>.5</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u>1422</u>	
Pf/Mf <u>.1/1.3</u>	HOLE DEV. <u>1.4 @ 6531</u>		BIT HP <u>640</u>	
CHLORIDES ppm <u>17000</u>	COST/FT <u>370</u>	<u>NA</u>	HP RATIO / HP/IN2 <u>55% - 5.4/IN2</u>	
CALCIUM ppm <u>920</u>	RPM <u>130</u>	<u>145</u>	REDUCED 1 <u>psi at stk/min</u>	
OIL/WATER/SOLIDS <u>0/91.5/8.5</u>	WOB <u>40</u>	<u>10-20</u>	RATE 2 <u>psi at stk/min</u>	
DAILY/CUM. COST				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>40</u>	<u>291</u>	
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>117</u>	<u>351</u>	
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>2139</u>	<u>.1215</u>	<u>121</u>	<u>327</u>	
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>175</u>	<u>380</u>	

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	
	DP	HWDP	DC				171	301
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>	
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>	
CAP-bbbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>	
DISP-bbbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>	
LENGTH-ft	<u>4721</u>	<u>728</u>	<u>476</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>		<u>310</u>	<u>133</u>	<u>68</u>	

REMARKS AND RECOMMENDATIONS

MW 10.0 GPM 600 JETS 3-13,1-11 ft/mi = 15 sec/std

DRILL AHEAD WITH BIT NO. 4. RAISE MUD WEIGHT TO 10.0 PPG TO STABILIZE HOLE CONDITIONS ON TRIPS. CONNECTION GAS AVERAGING ABOUT 50 UNITS ABOVE BACKGROUND. DRILL TO 6593'. CBU. POOH ON SLOW PENETRATION RATES AND BIT HOURS. SMALL SHOWS NOTED IN SANDS LOGGED DURING THE LAST 100' OF DRILLING. BACKREAM WHILE PULLING OUT OF THE HOLE.. AVERAGE GAS WHILE CIRCULATING IWAS 100 UNITS. MAX GAS RECORDED FOR PAST 24 HRS WAS 344 UNITS - ALSO LOGGED FROM BACKREAMING OUT OF THE HOLE.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 6729
 OPERATION RIH/CORE#1
 FOOTAGE 136

No. 17
 DATE Aug 14 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR	<u>ARCO ALASKA, INC.</u>	WELL NAME	<u>KUVLUM NO. 2</u>	FIELD/BLOCK	<u>OCS BLK 672 NR6-4</u>
CONTRACTOR	<u>CANMAR</u>	RIG NAME	<u>KULLUK</u>	AREA	<u>BEAUFORT SEA</u>
START DATE	<u>Jul 28 93</u>	LOC.	<u>OFFSHORE</u>	STATE	<u>ALASKA</u>

LOGGING DATA

AVG GAS (units)	<u>45</u>	MAX GAS (units)	<u>525</u>	AT DEPTH (feet)	<u>6700</u>	SURVEY DATA	<u>1.25 at 6625'</u>
BACKGROUND CONNECTION TRIP	<u>85</u>		<u>6562</u>		<u>6593</u>	LITHOLOGY	<u>30 % CLAY 30% SILTSTONE 40% SAND</u>
FLOWLINE TEMP	<u>88</u>					SAMPLE DEPTH	<u>6729</u>
						TRIP CHLORIDES	
						LAG DOWN DP	<u>940</u>
						LAG OFF BOTTOM	<u>7500</u>
						DRILL RATE ft/hr	<u>85</u>
						CORRECTED 'D' EXP.	<u>.72</u>
						SHALE DENSITY g/cc	<u>NA</u>
						EWR Res.	<u>15</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u>	psi	<u>8.7</u>	ppg	<u>3149</u>	psi
FRACTURE PRESSURE	<u>3081</u>	psi	<u>14.9</u>	ppg	<u>5494</u>	psi
ECD	<u>2109</u>	psi	<u>10.2</u>	ppg	<u>3569</u>	psi

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME	<u>24:00 AUG 13 93</u>	BIT NO.	<u>6</u>	<u>5</u>	PUMPS	<u>1.</u>	<u>ID1600</u>	<u>2.</u>	<u>ID1600</u>
TYPE	<u>GENERIC #2</u>	TYPE	<u>CB-1</u>	<u>DS-40 PDC</u>	SIZE inches	<u>6.5X12</u>	<u>6.5X12</u>		
WEIGHT IN	<u>10.0</u>	IADC CODE			CAPACITY gal/stk	<u>4.91</u>	<u>4.91</u>		
FUNNEL VIS.	<u>79</u>	SIZE	<u>8.5</u>	<u>12.25</u>	PUMP RATE stks/min	<u>71</u>	<u>71</u>		
PV/YP	<u>26/32</u>	JETS	<u>TFA: .7</u>	<u>2-14, 3-13</u>	FLOW RATE gal/min	<u>700</u>			
GELS	<u>5/10</u>	DEPTH OUT		<u>6729</u>	PRESSURE psi		<u>2650</u>		
pH	<u>9.0</u>	ROT HRS.		<u>1.8</u>	PD SURF / DS psi		<u>100/1600</u>		
FILT/CAKE API	<u>2.6 - 1/32</u>	FOOTAGE		<u>136</u>	ANN / BIT psi		<u>50/950</u>		
HP-HT		AVG ft/hr		<u>76</u>	JET VELOCITY ft/sec		<u>326</u>		
Pm	<u>.5</u>	GRADE		<u>INC</u>	JET IMPACT lbs		<u>1180</u>		
Pf/Mf	<u>.1/1.3</u>	HOLE DEV.			BIT HP		<u>387</u>		
CHLORIDES ppm	<u>17500</u>	COST/FT		<u>1360</u>	HP RATIO / HP/IN2		<u>36% - 3.3/IN2</u>		
CALCIUM ppm	<u>1040</u>	RPM		<u>130</u>	REDUCED 1		<u>psi at</u>	<u>stk/min</u>	
OIL/WATER/SOLIDS	<u>.5/90.5/9</u>	WOB		<u>5-10</u>	RATE 2		<u>psi at</u>	<u>stk/min</u>	
DAILY/CUM. COST									

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>46</u>	<u>314</u>	
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>133</u>	<u>380</u>	
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>2284</u>	<u>.1215</u>	<u>137</u>	<u>355</u>	
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>199</u>	<u>414</u>	

PIPE DATA

	DRILL STRING			CASING:	RISER	COND.	SURF.
	DP	HWDP	DC	DEPTH	171	301	1017
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>		<u>21.0</u>	<u>30</u>	<u>20</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20.0</u>	<u>28</u>	<u>18.75</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>		<u>.3887</u>	<u>.7616</u>	<u>.3408</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>		<u>NA</u>	<u>.113</u>	<u>.0479</u>
LENGTH-ft	<u>5525</u>	<u>728</u>	<u>476</u>		<u>170.5</u>	<u>95</u>	<u>811</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>			<u>310</u>	<u>133</u>
							<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.0 GPM 600 JETS 3-13,1-11 ft/mi = 15 sec/std

RIH WITH NB # 5. REAM LAST TWO STANDS TO BOTTOM. DRILL AHEAD. BREAK IN BIT WITH LOW WEIGHT ON BIT. DRILL AHEAD TO 6729'.
 CIRCULATE OUT HOLE VOLUME ON POTENTIAL SHOW INDICATED BY MWD TOOL. ZERO DISCHARGE DRILL CUTTINGS FROM ZONE OF INTEREST. MAX GAS FROM SAND FORMATION AT 6700' = 525 UNITS. CIRCULATE AND CONDITION HOLE FOR CORING. BACKGROUND GAS TO LESS THAN 50 UNITS. POOH. HOLE PULLED GOOD ON THIS TRIP. PICK UP CORE BARREL. RIH FOR CORE NO. 1.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 7205
 OPERATION DRILLING
 FOOTAGE 476

NO. 18
 DATE Aug 15 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>60</u>	MAX GAS (units) <u>464</u>	AT DEPTH (feet) <u>6755</u>	SURVEY DATA <u>.65 at 7094'</u>	LITHOLOGY <u>40 % CLAY 60% SILTSTONE</u>
BACKGROUND CONNECTION TRIP <u>90</u>	FLOWLINE TEMP <u>93</u> degrees F	TRIP CHLORIDES <u>998</u>	LAG DOWN DP <u>998</u>	LAG OFF BOTTOM <u>7950</u>
			DRILL RATE ft/hr <u>80</u>	CORRECTED 'D' EXP. <u>.75</u>
			SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>5</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>3372</u> psi	<u>9.0</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>5920</u> psi	<u>15.8</u> ppg	_____ psi	_____ ppg
ECD	<u>2151</u> psi	<u>10.3</u> ppg	<u>3896</u> psi	<u>10.4</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 14 93</u>	BIT NO. <u>CB-1</u>	RR5	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>RC-412</u>	<u>DS-40H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.1</u>	IADC CODE <u>CORE #1</u>	<u>PDC</u>	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>69</u>	SIZE <u>8.5</u>	<u>12.25</u>	PUMP RATE stks/min <u>71</u>	<u>70</u>
PV/YP <u>24/34</u>	JETS <u>TFA: .7</u>	<u>2-14, 3-13</u>	FLOW RATE gal/min <u>693</u>	
GELS <u>5/12</u>	DEPTH OUT <u>6732</u>	<u>NA</u>	PRESSURE psi <u>2650</u>	
pH <u>8.9</u>	ROT HRS. <u>.9</u>	<u>5.6</u>	PD SURF / DS psi <u>100/1610</u>	
FILT/CAKE API <u>3.0 - 1/32</u>	FOOTAGE <u>3</u>	<u>473</u>	ANN / BIT psi <u>70/940</u>	
HP-HT <u>6.8 @ 150</u>	AVG ft/hr <u>3.3</u>	<u>84</u>	JET VELOCITY ft/sec <u>322</u>	
Pm <u>.3</u>	GRADE _____	<u>INC</u>	JET IMPACT lbs <u>1170</u>	
Pf/Mf <u>.1/1.3</u>	HOLE DEV. _____		BIT HP <u>380</u>	
CHLORIDES ppm <u>17000</u>	COST/FT <u>NA</u>	<u>650</u>	HP RATIO / HP/IN2 <u>36% - 3.2/IN2</u>	
CALCIUM ppm <u>920</u>	RPM <u>60</u>	<u>130</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>TR/11/89</u>	WOB <u>10</u>	<u>5-10</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>45</u>	<u>334</u>	
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>132</u>	<u>396</u>	
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>2751</u>	<u>.1215</u>	<u>136</u>	<u>369</u>	
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>197</u>	<u>423</u>	

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	
	DP	HWDP	DC		171	301	1017	3978
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>		<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>		<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>		<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
LENGTH-ft	<u>6001</u>	<u>728</u>	<u>476</u>		<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>			<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.0 GPM 600 JETS 3-13,1-11 ft/mi = 15 sec/std

RIH FOR CORE NO. 1. ATTEMPT TO CORE. MAX TRIP GAS FROM BOTTOM = 246 UNITS. POOH AFTER PENETRATING 3 FEET OF HOLE.
 CORE BIT APPEARED TO BALL UP WITH CLAY. RR BIT NO. 5. DRILL AHEAD.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 7865
 OPERATION DRILLING
 FOOTAGE 660

NO. 19
 DATE Aug 16 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>40</u>	MAX GAS (units) <u>180</u>	AT DEPTH (feet) <u>7250</u>	SURVEY DATA <u>.65 at 7094'</u>	LITHOLOGY <u>40 % CLAY 60% SILTSTONE</u>
BACKGROUND CONNECTION <u>NA</u>	TRIP <u>625</u>	TRIP <u>7698</u>	SAMPLE DEPTH <u>7070</u>	TRIP CHLORIDES
FLOWLINE TEMP <u>91</u> degrees F			LAG DOWN DP <u>998</u>	LAG OFF BOTTOM <u>7950</u>
			DRILL RATE ft/hr <u>160</u>	CORRECTED 'D' EXP. <u>.78</u>
			SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>7</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>3844</u> psi	<u>9.4</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>6544</u> psi	<u>16</u> ppg	_____ psi	_____ ppg
ECD	<u>2151</u> psi	<u>10.3</u> ppg	<u>4212</u> psi	<u>10.3</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 15 93</u>	BIT NO. <u>CB-1</u>	<u>RR5</u>	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>RC-412</u>	<u>DS-40H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.0</u>	IADC CODE <u>CORE #1</u>	<u>PDC</u>	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>59</u>	SIZE <u>8.5</u>	<u>12.25</u>	PUMP RATE stks/min <u>72</u>	<u>71</u>
PV/YP <u>25/30</u>	JETS <u>TFA: .7</u>	<u>2-14, 3-13</u>	FLOW RATE gal/min <u>704</u>	
GELS <u>3/8</u>	DEPTH OUT <u>6732</u>		PRESSURE psi <u>2800</u>	
pH <u>8.6</u>	ROT HRS. <u>.9</u>	<u>12.1</u>	PD SURF / DS psi <u>100/1675</u>	
FILT/CAKE API <u>2.8 - 1/32</u>	FOOTAGE <u>3</u>	<u>1133</u>	ANN / BIT psi <u>65/960</u>	
HP-HT <u>6.0 @ 150</u>	AVG ft/hr <u>3.3</u>	<u>94</u>	JET VELOCITY ft/sec <u>328</u>	
Pm <u>.3</u>	GRADE <u>INC</u>		JET IMPACT lbs <u>1195</u>	
PI/MF <u>.1/1.3</u>	HOLE DEV. _____		BIT HP <u>395</u>	
CHLORIDES ppm <u>17500</u>	COST/FT <u>NA</u>	<u>596</u>	HP RATIO / HP/IN2 <u>33% - 3.3/IN2</u>	
CALCIUM ppm <u>880</u>	RPM <u>60</u>	<u>160</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>TR/9/91</u>	WOB <u>10</u>	<u>15</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>46</u>	<u>295</u>	
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>134</u>	<u>360</u>	
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>3411</u>	<u>.1215</u>	<u>138</u>	<u>336</u>	
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>201</u>	<u>393</u>	

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>171</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>
DISP-bbbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
LENGTH-ft	<u>6661</u>	<u>728</u>	<u>476</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>
					<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.0 GPM 700 JETS TFA: .68 ft/mi = 15 sec/std

DRILL AHEAD LOOKING FOR CORE POINT. PRESSURE TREND STARTING TO DEVELOP ON D-EXPONENT PLOT AT 7000'. INCREASE ROP APPROXIMATELY 50% BY ADDING WEIGHT ON BIT AND ADDITIONAL RPM BELOW 7500'. SLIGHT INCREASE IN GAS LOGGED FROM BOTTOMS UP ON CONNECTIONS. RAISED PORE PRESSURE ESTIMATE TO 9.4 PPG AT 7675'. DRILL TO 7698'. CBU. POOH TO SHOE. PUMP OUT OF THE HOLE ON STANDS 9,10,11, AND 12. REPAIR TOP DRIVE. RIH. DRILL AHEAD. BOTTOMS UP FROM TRIP = 625 UNITS.

ADT J. PATTON

sperry-sun LOGGING SYSTEMS

DRILLING SERVICES
A Baroid Company

DEPTH 9500
OPERATION POOH
FOOTAGE 1635

No. 20
DATE Aug 17 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>90</u>	MAX GAS (units) <u>1513</u>	AT DEPTH (feet) <u>9020</u>	SURVEY DATA <u>.80 @ 9376</u>
BACKGROUND CONNECTION TRIP	<u>165</u>	<u>9488</u>	LITHOLOGY <u>60 % CLAY 40% SILTSTONE TR SANDSTONE</u>
TRIP	<u>625</u>	<u>7698</u>	SAMPLE DEPTH <u>9500</u>
FLOWLINE TEMP <u>95</u> degrees F			TRIP CHLORIDES
			LAG DOWN DP <u>1345</u>
			LAG OFF BOTTOM <u>10450</u>
			DRILL RATE ft/hr <u>88</u>
			CORRECTED 'D' EXP. <u>.88</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>3.5</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE		
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>3844</u> psi	<u>9.7</u> ppg	_____ psi	_____ ppg	_____ ft
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>6544</u> psi	<u>16.2</u> ppg	_____ psi	_____ ppg	_____ ft
ECD	<u>2151</u> psi	<u>10.</u> ppg	<u>4212</u> psi	_____ ppg	_____ psi	_____ ppg	_____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 16 93</u>	BIT NO. <u>CB-1</u>	RR5	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>RC-412</u>	<u>DS-40H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.4+</u>	IADC CODE <u>CORE #1</u>	<u>PDC</u>	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>70</u>	SIZE <u>8.5</u>	<u>12.25</u>	PUMP RATE stks/min <u>69</u>	<u>70</u>
PV/YP <u>30/40</u>	JETS <u>TFA: .7</u>	<u>2-14, 3-13</u>	FLOW RATE gal/min <u>686</u>	
GELS <u>5/15</u>	DEPTH OUT <u>6732</u>	<u>9500</u>	PRESSURE psi <u>3600</u>	
pH <u>8.8</u>	ROT HRS. <u>.9</u>	<u>27.4</u>	PD SURF / DS psi <u>100/2450</u>	
FILT./CAKE API <u>2.9 - 1/32</u>	FOOTAGE <u>3</u>	<u>2768</u>	ANN / BIT psi <u>105/945</u>	
HP-HT <u>6.8 @ 150</u>	AVG ft/hr <u>3.3</u>	<u>101</u>	JET VELOCITY ft/sec <u>319</u>	
P _m <u>.3</u>	GRADE <u>INC</u>		JET IMPACT lbs <u>1179</u>	
Pf/Mf <u>.1/1.4</u>	HOLE DEV. _____		BIT HP <u>380</u>	
CHLORIDES ppm <u>17000</u>	COST/FT <u>NA</u>	<u>331</u>	HP RATIO / HP/IN2 <u>26% - 3.2/IN2</u>	
CALCIUM ppm <u>920</u>	RPM <u>60</u>	<u>160</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>TR/10.5/89.5</u>	WOB <u>10</u>	<u>14</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>45</u>	<u>361</u>	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>130</u>	<u>432</u>	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>5046</u>	<u>.1215</u>	<u>134</u>	<u>403</u>	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>195</u>	<u>466</u>	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	
OD-inches	DP <u>5.0</u>	HWDP <u>5.0</u>	DC <u>8</u>	<u>171</u>	<u>21.0</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>20.0</u>	<u>30</u>	<u>20</u>	<u>18.75</u>	<u>12.415</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>	
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>	
LENGTH-ft	<u>8296</u>	<u>728</u>	<u>476</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>		<u>310</u>	<u>133</u>	<u>68</u>	

REMARKS AND RECOMMENDATIONS

MW 10.4 GPM 650 JETS TFA: .68 _____ ft/mi = 15 sec/std

DRILL AHEAD WITH BIT NO. 5. SLIGHT INCREASE IN BACKGROUND GAS AND CONNECTION GAS LOGGED WITH INCREASING DEPTH. RAISED PORE PRESSURE ESTIMATE TO REFLECT TREND DEVELOPING ON D-EXPONENT AND RESISTIVITY PLOT. CURRENT ESTIMATE IS 9.7 PPG AT THIS DEPTH. THE MUD WEIGHT WAS RAISED IN TWO STAGES TO 10.4 PPG FOR ADDITIONAL OVERBALANCE. CBU AT 9500. POOH.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 9500
 OPERATION RIH
 FOOTAGE 0

NO. 21
 DATE Aug 18 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>350</u>	AT DEPTH (feet) <u>B.REM</u>	SURVEY DATA <u>.80 @ 9376</u>	LITHOLOGY <u>60% CLAY 40% SILTSTONE TR SANDSTONE</u>
BACKGROUND CONNECTION TRIP <u>0</u>	<u>165</u>	<u>9488</u>	SAMPLE DEPTH <u>9500</u>	TRIP CHLORIDES <u> </u>
FLOWLINE TEMP <u>80</u> degrees F			LAG DOWN DP <u>1345</u>	LAG OFF BOTTOM <u>10450</u>
			DRILL RATE ft/hr <u>88</u>	CORRECTED 'D' EXP. <u>.88</u>
			SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>3.5</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppG	<u>3844</u> psi	<u>9.7</u> ppG	_____ psi	_____ ppG
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppG	<u>6544</u> psi	<u>16.2</u> ppG	_____ psi	_____ ppG
ECD	<u>2151</u> psi	<u>10.6</u> ppG	<u>4212</u> psi	<u>10.6</u> ppG	_____ psi	_____ ppG

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 17 93</u>	BIT NO. <u>6</u>	RR5	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>DS-40H</u>	<u>DS-40H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.4</u>	IADC CODE <u>PDC</u>	<u>PDC</u>	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>68</u>	SIZE <u>12.25</u>	<u>12.25</u>	PUMP RATE stks/min <u>69</u>	<u>70</u>
PV/YP <u>23/35</u>	JETS <u>5-15</u>	<u>2-14, 3-13</u>	FLOW RATE gal/min <u>686</u>	
GELS <u>4/7</u>	DEPTH OUT _____	<u>9500</u>	PRESSURE psi _____	<u>3600</u>
pH <u>8.8</u>	ROT HRS. _____	<u>27.4</u>	PD SURF / DS psi _____	<u>100/2450</u>
FILT/CAKE API <u>2.9 - 1/32</u>	FOOTAGE _____	<u>2768</u>	ANN / BIT psi _____	<u>105/945</u>
HP-HT <u>6.8 @ 150</u>	AVG ft/hr _____	<u>101</u>	JET VELOCITY ft/sec _____	<u>319</u>
Pm <u>.3</u>	GRADE _____	<u>INC</u>	JET IMPACT lbs _____	<u>1179</u>
Pf/Mf <u>.1/1.5</u>	HOLE DEV. _____		BIT HP _____	<u>380</u>
CHLORIDES ppm <u>17500</u>	COST/FT _____	<u>331</u>	HP RATIO / HP/IN2 _____	<u>26% - 3.2/IN2</u>
CALCIUM ppm <u>920</u>	RPM _____	<u>160</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>TR/10/90</u>	WOB _____	<u>14</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>45</u>	<u>361</u>	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>130</u>	<u>432</u>	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>5046</u>	<u>.1215</u>	<u>134</u>	<u>403</u>	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>195</u>	<u>466</u>	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	
OD-inches	DP <u>5.0</u>	HWDP <u>5.0</u>	DC <u>8</u>		<u>171</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>		<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>		<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
LENGTH-ft	<u>8296</u>	<u>728</u>	<u>476</u>		<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>			<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.4 GPM 700 JETS TFA: .75 _____ ft/mi = 15 sec/std

PUMP OUT OF HOLE ON FIRST 20 STANDS. HOLE PULLED GOOD FOR THE REST OF THE WAY OUT. TEST BOP. PICK UP ADDITIONAL DRILL PIPE ON THE WAY BACK IN.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 10551
 OPERATION S. TRIP
 FOOTAGE 1051

NO. 22
 DATE Aug 19 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>50</u>	MAX GAS (units) <u>140</u>	AT DEPTH (feet) <u>9785</u>	SURVEY DATA <u>.80 @ 9376</u>
BACKGROUND CONNECTION TRIP <u>1541</u>	FLOWLINE TEMP <u>105</u> degrees F	LITHOLOGY <u>60% CLAY 40% SILTSTONE TR SANDSTONE</u>	SAMPLE DEPTH <u>9500</u>
TRIP CHLORIDES <u>1541</u>	LAG DOWN DP <u>1505</u>	DRILL RATE ft/hr <u>95</u>	TRIP CHLORIDES <u>1541</u>
LAG OFF BOTTOM <u>11750</u>	LAG OFF BOTTOM <u>11750</u>	CORRECTED 'D' EXP. <u>.81</u>	SHALE DENSITY g/cc <u>NA</u>
		EWR Res. <u>3.5</u>	

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>5432</u> psi	<u>9.9</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>9053</u> psi	<u>16.5</u> ppg	_____ psi	_____ ppg
ECD	<u>2113</u> psi	<u>10.7</u> ppg	<u>5870</u> psi	<u>10.6</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 18 93</u>	BIT NO. <u>6</u>	RR5 _____	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>DS-40H</u>	<u>DS-40H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.5</u>	IADC CODE <u>PDC</u>	<u>PDC</u>	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>64</u>	SIZE <u>12.25</u>	<u>12.25</u>	PUMP RATE stks/min <u>69</u>	<u>69</u>
PV/YP <u>26/34</u>	JETS <u>5-15</u>	<u>2-14, 3-13</u>	FLOW RATE gal/min <u>678</u>	_____
GELS <u>4/12</u>	DEPTH OUT <u>9500</u>	_____	PRESSURE psi <u>3200</u>	_____
pH <u>8.8</u>	ROT HRS. <u>11.6</u>	<u>27.4</u>	PD SURF / DS psi <u>100/2400</u>	_____
FILT/CAKE API <u>3.4 - 1/32</u>	FOOTAGE <u>1051</u>	<u>2768</u>	ANN / BIT psi <u>100/600</u>	_____
HP-HT <u>6.8 @ 150</u>	AVG ft/hr <u>90</u>	<u>101</u>	JET VELOCITY ft/sec <u>252</u>	_____
Pm <u>.45</u>	GRADE <u>INC</u>	<u>40% - 1/8</u>	JET IMPACT lbs <u>929</u>	_____
Pf/Mf <u>.25/1.5</u>	HOLE DEV. _____	_____	BIT HP <u>235</u>	_____
CHLORIDES ppm <u>17000</u>	COST/FT <u>503</u>	<u>331</u>	HP RATIO / HP/IN2 <u>19% - 2.0/IN2</u>	_____
CALCIUM ppm <u>920</u>	RPM <u>155</u>	<u>160</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>TR/10/90</u>	WOB <u>8-10</u>	<u>14</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	<u>44</u>	<u>321</u>	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	<u>129</u>	<u>385</u>	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>6098</u>	<u>.1215</u>	<u>133</u>	<u>359</u>	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>193</u>	<u>416</u>	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>171</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
LENGTH-ft	<u>9347</u>	<u>728</u>	<u>476</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	_____	<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.5 GPM 700 JETS TFA: .75 ft/mi = 15 sec/std

DRILL AHEAD WITH BIT NO. 6. MAX GAS FROM BOTTOM ON TRIP = 1543 UNITS. VERY GOOD PENETRATION RATES WITH NEW BIT.

RESISTIVITY DATA INDICATING INCREASING PORE PRESSURE GRADIENT CONTINUOUS TO ABOUT 10,000'. RAISED PORE PRESSURE ESTIMATE TO 9.9 PPG AT THIS DEPTH. TREND APPEARS TO STABILIZE BELOW 10,000'. DRILL TO 10551'. SHORT TRIP PAST 9,500' TO CONDITION THE HOLE.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 11125
OPERATION S. TRIP
FOOTAGE 574

No. 23
DATE Aug 20 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>40</u>	MAX GAS (units) <u>130</u>	AT DEPTH (feet) <u>10927</u>	SURVEY DATA <u>4.03 Deg at 11125'</u>	LITHOLOGY <u>40 % CLAY 60% SILTSTONE</u>	SAMPLE DEPTH <u>11125</u>	DRILL RATE ft/hr <u>20</u>
BACKGROUND CONNECTION TRIP <u>10</u>	TRIP <u>683</u>	TRIP <u>10551</u>	TRIP CHLORIDES	LAG DOWN DP	LAG OFF BOTTOM	CORRECTED 'D' EXP.
FLOWLINE TEMP _____	degrees F					SHALE DENSITY g/cc <u>NA</u>
						EWR Res.

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>5432</u> psi	<u>9.9</u> ppg	_____ psi	_____ ppg _____ ft
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>9053</u> psi	<u>16.5</u> ppg	_____ psi	_____ ppg _____ ft
ECD	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg _____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>24:00 AUG 19 93</u>	BIT NO. <u>6</u>	PUMPS <u>1.</u> <u>ID1600</u> <u>2.</u> <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>DS-40H</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>10.7</u>	IADC CODE <u>PDC</u>	CAPACITY gal/stk <u>4.91</u> <u>4.91</u>
FUNNEL VIS. <u>58</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____
PV/YP <u>27/34</u>	JETS <u>5-15</u>	FLOW RATE gal/min _____
GELS <u>3/9</u>	DEPTH OUT <u>11125</u>	PRESSURE psi _____
pH <u>8.6</u>	ROT HRS. <u>25.1</u>	PD SURF / DS psi _____
FILT/CAKE API <u>3.1 - 1/32</u>	FOOTAGE <u>1625</u>	ANN / BIT psi _____
HP-HT <u>6.0 @ 150</u>	AVG ft/hr <u>65</u>	JET VELOCITY ft/sec _____
P _m <u>.3</u>	GRADE _____	JET IMPACT lbs _____
P _f /M _i <u>.2/1.5</u>	HOLE DEV. <u>4.03</u>	BIT HP _____
CHLORIDES ppm <u>17000</u>	COST/FT <u>517</u>	HP RATIO / HP/IN2 _____
CALCIUM ppm <u>960</u>	RPM <u>152</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>TR/11.5/88.5</u>	WOB <u>11</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	_____	_____	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	_____	_____	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>6098</u>	<u>.1215</u>	_____	_____	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING: RISER COND. SURF.			
	DP	HWDP	DC	DEPTH			
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>171</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
LENGTH-ft	<u>9919</u>	<u>728</u>	<u>476</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>
					<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.5 GPM 700 JETS TFA: .75 _____ ft/mi = 15 sec/std

RIH AFTER SHORT TRIP. SHORT TRIP GAS = 683. DRILL AHEAD WITH BIT NO 6 THRU SILTSTONE/CLAY TO 11125'. SHORT TRIP TO SHOE TO CONDITION HOLE TO RUN E LOGS. HOLE PULLED TIGHT AT 10261-10071' AND 9057-8767'.

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 11125
 OPERATION E LOG
 FOOTAGE _____

NO. 24
 DATE Aug 21 93
 TIME 04.00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR ARCO ALASKA, INC. WELL NAME KUVLUM NO. 2 FIELD/BLOCK OCS BLK 672 NR6-4
 CONTRACTOR CANMAR RIG NAME KULLUK AREA BEAUFORT SEA
 START DATE Jul 28 93 LOC. OFFSHORE STATE ALASKA

LOGGING DATA

AVG MAX AT SURVEY DATA 4.03 Deg at 11125'
 GAS GAS DEPTH LITHOLOGY 40 % CLAY 60% SILTSTONE
 (units) (units) (feet) SAMPLE DEPTH 11125
 BACKGROUND NA TRIP CHLORIDES _____
 CONNECTION _____ LAG DOWN DP _____
 TRIP _____ 663 11125 LAG OFF BOTTOM _____
 FLOWLINE TEMP _____ degrees F DRILL RATE ft/hr _____
 CORRECTED 'D' EXP. _____
 SHALE DENSITY g/cc NA
 EWR Res. _____

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE									
PORE PRESSURE	1800	psi	8.7	ppg	5727	psi	9.9	ppg	_____	psi	_____	ppg	_____	ft
FRACTURE PRESSURE	3081	psi	14.9	ppg	9545	psi	16.5	ppg	_____	psi	_____	ppg	_____	ft
ECD	_____	psi	_____	ppg	_____	psi	_____	ppg	_____	psi	_____	ppg	_____	ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME	<u>1530 AUG 20 93</u>	BIT NO.	<u>6</u>	PUMPS	1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE	<u>GENERIC #2</u>	TYPE	<u>DS-40H</u>	SIZE inches	<u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN	<u>10.8</u>	IADC CODE	<u>PDC</u>	CAPACITY gal/stk	<u>4.91</u>	<u>4.91</u>
FUNNEL VIS.	<u>56</u>	SIZE	<u>12.25</u>	PUMP RATE stks/min	_____	_____
PV/YP	<u>28/36</u>	JETS	<u>5-15</u>	FLOW RATE gal/min	_____	_____
GELS	<u>3/13</u>	DEPTH OUT	<u>11125</u>	PRESSURE psi	<u>STATIC</u>	
pH	<u>8.5</u>	ROT HRS.	<u>25.1</u>	PD SURF / DS psi	_____	
FILT/CAKE API	<u>3.0 -1/32</u>	FOOTAGE	<u>1625</u>	ANN / BIT psi	_____	
HP-HT	<u>6.2 @ 150</u>	AVG ft/hr	<u>65</u>	JET VELOCITY ft/sec	_____	
P.m	<u>.3</u>	GRADE	<u>4-4-X-1/8</u>	JET IMPACT lbs	_____	
Pf.Mf	<u>.15/1.4</u>	HOLE DEV.	<u>4.03</u>	BIT HP	_____	
CHLORIDES ppm	<u>17000</u>	COST/FT	<u>517</u>	HP RATIO / HP/IN2	_____	
CALCIUM ppm	<u>920</u>	RPM	<u>152</u>	REDUCED 1	_____ psi at	_____ stk/min
OIL/WATER/SOLIDS	<u>TR/11.5/88.5</u>	WOB	<u>11</u>	RATE 2	_____ psi at	_____ stk/min
DAILY/CUM. COST	_____					

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	_____	_____	_____
<u>5X13 3/8</u>	<u>DP-C&G</u>	<u>3906</u>	<u>.1255</u>	_____	_____	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>6098</u>	<u>.1215</u>	_____	_____	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>171</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
LENGTH-ft	<u>9919</u>	<u>728</u>	<u>476</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	_____	<u>310</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.5 GPM 700 JETS TFA: .75 _____ ft/mi = 15 sec/std

RIH AFTER SHORT TRIP. SHORT TRIP GAS=663. CIRC AND CONDITION HOLE. POH FOR E LOGS. NO PROBLEMS PULLING PIPE. E LOG.

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

DEPTH 11125
 OPERATION E LOG
 FOOTAGE _____

No. 25
 DATE Aug 22 93
 TIME 04 00

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) _____	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>4.03 Deg at 11125'</u>
BACKGROUND _____	CONNECTION _____	TRIP _____	LITHOLOGY <u>40 % CLAY 60% SILTSTONE</u>
FLOWLINE TEMP _____ degrees F	SAMPLE DEPTH <u>11125</u>	TRIP CHLORIDES _____	DRILL RATE ft/hr _____
	LAG DOWN DP _____	LAG OFF BOTTOM _____	CORRECTED 'D' EXP. _____
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. _____

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>5727</u> psi	<u>9.9</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>9545</u> psi	<u>16.5</u> ppg	_____ psi	_____ ppg
ECD	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2100 21 AUG 93</u>	BIT NO. _____	6	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE _____	<u>D8-40H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.9</u>	IADC CODE _____	<u>PDC</u>	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>68</u>	SIZE _____	<u>12.25</u>	PUMP RATE stks/min _____	_____
PV/YP <u>28/37</u>	JETS _____	<u>5-15</u>	FLOW RATE gal/min _____	_____
GELS <u>3/12</u>	DEPTH OUT _____	<u>11125</u>	PRESSURE psi _____	<u>STATIC</u>
pH <u>8.5</u>	ROT HRS. _____	<u>25.1</u>	PD SURF / DS psi _____	_____
FILT/CAKE API <u>2.6/1</u>	FOOTAGE _____	<u>1625</u>	ANN / BIT psi _____	_____
HP-HT <u>7.0 @ 150</u>	AVG ft/hr _____	<u>85</u>	JET VELOCITY ft/sec _____	_____
P _m <u>.3</u>	GRADE _____	<u>4-4-X-1/8</u>	JET IMPACT lbs _____	_____
Pf/Mf <u>.15/1.4</u>	HOLE DEV. _____	<u>4.03</u>	BIT HP _____	_____
CHLORIDES ppm <u>17000</u>	COST/FT _____	<u>517</u>	HP RATIO / HP/IN2 _____	_____
CALCIUM ppm <u>940</u>	RPM _____	<u>152</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>TR/12/88</u>	WOB _____	<u>11</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	_____	_____	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	_____	_____	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>6098</u>	<u>.1215</u>	_____	_____	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	INT.
	DP	HWDP	DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	<u>171</u>	<u>21.0</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>20.0</u>	<u>30</u>	<u>20</u>	<u>18.75</u>	<u>12.415</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>	_____
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>	_____
LENGTH-ft	<u>9921</u>	<u>728</u>	<u>476</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	_____	<u>310</u>	<u>133</u>	<u>68</u>	_____

REMARKS AND RECOMMENDATIONS

MW 10.5 GPM 700 JETS TFA: .75 _____ ft/mi = 15 sec/std

E LOG, HOLE TAKING .5 BBLs/HR

ADT _____ D. WALTERS

sperry-sun **LOGGING SYSTEMS**
 DRILLING SERVICES
 A Baroid Company

DEPTH 11125
 OPERATION E LOG
 FOOTAGE _____

No. 27
 DATE Aug 24 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>NA</u>	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>4.03 Deg at 11125'</u>
BACKGROUND CONNECTION TRIP _____	FLOWLINE TEMP _____ degrees F	LITHOLOGY <u>40 % CLAY 60% SILTSTONE</u>	SAMPLE DEPTH <u>11125</u>
TRIP _____	LAG DOWN DP _____	TRIP CHLORIDES _____	DRILL RATE ft/hr _____
LAG OFF BOTTOM _____	SHALE DENSITY g/cc <u>NA</u>	LAG OFF BOTTOM _____	CORRECTED 'D' EXP. _____
	EWR Res. _____		

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>5727</u> psi	<u>9.9</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>9545</u> psi	<u>16.5</u> ppg	_____ psi	_____ ppg
ECD	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>1900 22 AUG 93</u>	BIT NO. <u>6</u>	PUMPS 1. <u>ID1600</u>	2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>D8-40H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.9</u>	IADC CODE _____	CAPACITY gal/stk <u>4.91</u>	<u>4.91</u>
FUNNEL VIS. <u>68</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____	_____
PV/YP <u>28/33</u>	JETS _____	FLOW RATE gal/min _____	_____
GELS <u>3/14</u>	DEPTH OUT <u>11125</u>	PRESSURE psi _____	<u>STATIC</u>
pH <u>8.5</u>	ROT HRS. _____	PD SURF / DS psi _____	_____
FILT/CAKE API <u>2.8/1</u>	FOOTAGE <u>1625</u>	ANN / BIT psi _____	_____
HP+HT <u>8.6 @ 150</u>	AVG ft/hr _____	JET VELOCITY ft/sec _____	_____
P _m <u>.3</u>	GRADE <u>4-4-X-1/8</u>	JET IMPACT lbs _____	_____
Pf/Mf <u>.15/1.4</u>	HOLE DEV. <u>4.03</u>	BIT HP _____	_____
CHLORIDES ppm <u>17000</u>	COST/FT <u>517</u>	HP RATIO / HP/IN2 _____	_____
CALCIUM ppm <u>960</u>	RPM <u>152</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>TR/12/88</u>	WOB <u>11</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____			

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20 DP-RISER</u>	<u>171</u>	<u>.3644</u>	_____	_____	_____
<u>5X13 3/8 DP-CSG</u>	<u>3906</u>	<u>.1255</u>	_____	_____	_____
<u>5X12.25 DP-HOLE</u>	<u>6098</u>	<u>.1215</u>	_____	_____	_____
<u>8X12.25 DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING				CASING: DEPTH	RISER	COND.	SURF.	INT.
OD-inches	<u>5.0</u>	<u>5.0</u>	_____	<u>8</u>	<u>171</u>	<u>21.0</u>	<u>30</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	_____	<u>2.875</u>	<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	_____	<u>.0076</u>	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>	_____
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	_____	<u>.0545</u>	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>	_____
LENGTH-ft	<u>9921</u>	<u>728</u>	_____	<u>476</u>	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	_____	<u>149</u>	_____	<u>310</u>	<u>133</u>	<u>68</u>	_____

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____	ft/mi = _____	sec/std _____
E LOG. LOST 70 BBLs MUD TO HOLE IN 56 HRS. RIH FOR CLEANOUT RUN. HOLE TIGHT AT 10837'. WASH TO BOTTOM. CBU. TRIP GAS=1469.		
POOH FOR MORE E LOGS.		
ADT _____ D. WALTERS		

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 11125
 OPERATION E LOG
 FOOTAGE _____

NO. 28
 DATE Aug 25 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM NO. 2</u>	FIELD/BLOCK <u>OCS BLK 672 NR6-4</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Jul 28 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>NA</u>	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>4.03 Deg at 11125'</u>
BACKGROUND CONNECTION _____	TRIP _____	TRIP CHLORIDES _____	LITHOLOGY <u>40 % CLAY 60% SILTSTONE</u>
TRIP _____	LAG DOWN DP _____	LAG OFF BOTTOM _____	SAMPLE DEPTH <u>11125</u>
FLOWLINE TEMP _____ degrees F	DRILL RATE ft/hr _____	CORRECTED 'D' EXP. _____	SHALE DENSITY g/cc <u>NA</u>
	EWR Res. _____		

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>5727</u> psi	<u>9.9</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>9545</u> psi	<u>16.5</u> ppg	_____ psi	_____ ppg
ECD	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>1900 24 AUG 93</u>	BIT NO. <u>6</u>	PUMPS 1. <u>ID1600</u> 2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>D8-40H</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>10.9</u>	IADC CODE _____	CAPACITY gal/stk <u>4.91</u> <u>4.91</u>
FUNNEL VIS. <u>68</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____
PV/YP <u>28/32</u>	JETS <u>5-15</u>	FLOW RATE gal/min _____
GELS <u>3/14</u>	DEPTH OUT <u>11125</u>	PRESSURE psi <u>STATIC</u>
pH <u>8.5</u>	ROT HRS. <u>25.1</u>	PD SURF / DS psi _____
FILT/CAKE API <u>2.8/1</u>	FOOTAGE <u>1625</u>	ANN / BIT psi _____
HP-HT <u>8.8 @ 150</u>	AVG ft/hr <u>85</u>	JET VELOCITY ft/sec _____
P _m <u>.3</u>	GRADE <u>4-4-X-1/8</u>	JET IMPACT lbs _____
Pf/Mf <u>.15/1.4</u>	HOLE DEV. <u>4.03</u>	BIT HP _____
CHLORIDES ppm <u>17000</u>	COST/FT _____	HP RATIO / HP/IN2 _____
CALCIUM ppm <u>960</u>	RPM <u>152</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>TR/12/88</u>	WOB <u>11</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	_____	_____	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	_____	_____	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>6098</u>	<u>.1215</u>	_____	_____	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING				CASING: DEPTH	RISER	COND.	SURF.	INT.
	DP	HWDP	DC						
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	_____	<u>171</u>	<u>301</u>	<u>1017</u>	<u>3978</u>	
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>	
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	_____	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>	
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	_____	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>	
LENGTH-ft	<u>9921</u>	<u>728</u>	<u>476</u>	_____	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	_____	_____	<u>310</u>	<u>133</u>	<u>68</u>	

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____	ft/mi = _____ sec/std
<u>E LOG. LOST 15 BBLs MUD TO HOLE IN 20 HRS.</u>	
ADT _____	D. WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 11125
 OPERATION CIRC
 FOOTAGE _____

NO. 29
 DATE Aug 26 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR ARCO ALASKA, INC. WELL NAME KUVLUM NO. 2 FIELD/BLOCK OCS BLK 672 NR6-4
 CONTRACTOR CANMAR RIG NAME KULLUK AREA BEAUFORT SEA
 START DATE Jul 28 93 LOC. OFFSHORE STATE ALASKA

LOGGING DATA

AVG GAS (units) <u>NA</u>	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>4.03 Deg at 11125'</u>	LITHOLOGY <u>40 % CLAY 60% SILTSTONE</u>	SAMPLE DEPTH <u>11125</u>	DRILL RATE ft/hr _____
BACKGROUND CONNECTION TRIP _____	FLOWLINE TEMP _____ degrees F	TRIP CHLORIDES _____	LAG DOWN DP _____	LAG OFF BOTTOM _____	CORRECTED 'D' EXP. _____	SHALE DENSITY g/cc <u>NA</u>
			EWR Res. _____			

FORMATION PRESSURE DATA

CASING			BOTTOM HOLE			OPEN HOLE		
PORE PRESSURE	<u>1800</u> psi	<u>8.7</u> ppg	<u>5727</u> psi	<u>9.9</u> ppg	_____ psi	_____ ppg	_____ ft	_____ ft
FRACTURE PRESSURE	<u>3081</u> psi	<u>14.9</u> ppg	<u>9545</u> psi	<u>16.5</u> ppg	_____ psi	_____ ppg	_____ ft	_____ ft
ECD	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ ft	_____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>1900 24 AUG 93</u>	BIT NO. <u>6</u>	PUMPS 1. <u>ID1600</u> 2. <u>ID1600</u>
TYPE <u>GENERIC #2</u>	TYPE <u>D8-40H</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>10.9</u>	IADC CODE _____	CAPACITY gal/stk <u>4.91</u> <u>4.91</u>
FUNNEL VIS. <u>68</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____
PV/YP <u>28/32</u>	JETS <u>5-15</u>	FLOW RATE gal/min _____
GELS <u>3/14</u>	DEPTH OUT <u>11125</u>	PRESSURE psi _____
pH <u>8.5</u>	ROT HRS. <u>25.1</u>	PD SURF / DS psi _____
FILT/CAKE API <u>2.8/1</u>	FOOTAGE <u>1625</u>	ANN / BIT psi _____
HPHT <u>8.8 @ 150</u>	AVG ft/hr <u>85</u>	JET VELOCITY ft/sec _____
P _m <u>.3</u>	GRADE <u>4-4-X-1/8</u>	JET IMPACT lbs _____
Pf/Mf <u>.15/1.4</u>	HOLE DEV. <u>4.03</u>	BIT HP _____
CHLORIDES ppm <u>17000</u>	COST/FT _____	HP RATIO / HP/IN2 _____
CALCIUM ppm <u>960</u>	RPM <u>152</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>TR/12/88</u>	WOB <u>11</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5X20</u>	<u>DP-RISER</u>	<u>171</u>	<u>.3644</u>	_____	_____	_____
<u>5X13 3/8</u>	<u>DP-CSG</u>	<u>3906</u>	<u>.1255</u>	_____	_____	_____
<u>5X12.25</u>	<u>DP-HOLE</u>	<u>6098</u>	<u>.1215</u>	_____	_____	_____
<u>8X12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	INT.
	DP	HWDP	DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8</u>	_____	<u>171</u>	<u>301</u>	<u>1017</u>	<u>3978</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>21.0</u>	<u>30</u>	<u>20</u>	<u>13.375</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0076</u>	_____	<u>20.0</u>	<u>28</u>	<u>18.75</u>	<u>12.415</u>
DISP-bbls/ft	<u>.0075</u>	<u>.0181</u>	<u>.0545</u>	_____	<u>.3887</u>	<u>.7616</u>	<u>.3408</u>	<u>.1498</u>
LENGTH-ft	<u>9921</u>	<u>728</u>	<u>476</u>	_____	<u>NA</u>	<u>.113</u>	<u>.0479</u>	<u>.024</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>149</u>	_____	<u>170.5</u>	<u>95</u>	<u>811</u>	<u>3772</u>
					<u>310</u>	<u>133</u>	<u>68</u>	

REMARKS AND RECOMMENDATIONS

MW _____ GPM _____ JETS _____ ft/mi = _____ sec/std

E LOG. LOGGING TOOL STUCK AT 6200'. TRIP IN HOLE STRIPPING OVER WIRELINE TO RECOVER FISH. RECOVER FISH. POOH. RIH FOR CLEANOUT RUN. CIRCULATE AND CONDITION HOLE.

ADT D. WALTERS

sperry-sun *LOGGING SYSTEMS*
 DRILLING SERVICES
 A Baroid Company

DEPTH 405
 OPERATION DRILLING
 FOOTAGE 189

NO. 1
 DATE Sep 10 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>2</u>	AT DEPTH (feet) _____	SURVEY DATA <u>NA</u>	LITHOLOGY <u>NA</u>	SAMPLE DEPTH _____	TRIP CHLORIDES _____	LAG DOWN DP <u>25</u>	LAG OFF BOTTOM <u>NA</u>	DRILL RATE ft/hr <u>45</u>	CORRECTED 'D' EXP. <u>.91</u>	SHALE DENSITY g/cc _____	EWR Res. _____
BACKGROUND CONNECTION <u>0</u>	TRIP <u>0</u>	FLOWLINE TEMP <u>39</u> degrees F										

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>137</u> psi	<u>8.5</u> ppg	<u>179</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>NA</u> psi	<u>NA</u> ppg	<u>200</u> psi	<u>9.5</u> ppg	_____ psi	_____ ppg
ECD	<u>137</u> psi	<u>8.5</u> ppg	<u>179</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>00:00 9/9/93</u>	BIT NO. <u>1</u>	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>SWEEP STORAGE</u>	TYPE <u>ATXG1</u>	SIZE inches <u>7.5X12</u>	<u>7.5X12</u>
WEIGHT IN <u>8.8</u>	IADC CODE _____	CAPACITY gal/stk <u>6.54</u>	<u>6.54</u>
FUNNEL VIS. <u>70</u>	SIZE <u>26'</u>	PUMP RATE stks/min <u>77</u>	<u>77</u>
PV/YP <u>16/16</u>	JETS <u>3-21,1-22</u>	FLOW RATE gal/min <u>1007</u>	_____
GELS <u>12/28</u>	DEPTH OUT _____	PRESSURE psi _____	<u>1300</u>
pH <u>9.0</u>	ROT HRS. <u>14.6</u>	PD SURF / DS psi _____	<u>100/790</u>
FILT/CAKE API _____	FOOTAGE <u>189</u>	ANN / BIT psi _____	<u>0/410</u>
HP-HT _____	AVG ft/hr <u>12.9</u>	JET VELOCITY ft/sec _____	<u>232</u>
Pm _____	GRADE <u>INC</u>	JET IMPACT lbs _____	<u>1024</u>
Pf/Mf <u>.15/.3</u>	HOLE DEV. _____	BIT HP _____	<u>240</u>
CHLORIDES ppm <u>650</u>	COST/FT <u>226</u>	HP RATIO / HP/IN2 _____	<u>30% - .5/IN2</u>
CALCIUM ppm <u>400</u>	RPM <u>160 (CALC)</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS _____	WOB <u>2/10</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____			

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 27</u> DP-CSG	<u>93</u>	<u>.6842</u>	<u>34</u>	<u>NA</u>	_____
<u>5 X 26</u> DP-HOLE	_____	<u>.6326</u>	_____	_____	_____
<u>9.0 x 27</u>	<u>6</u>	<u>.5905</u>	<u>36</u>	_____	_____
<u>9.0 X 26</u> DC-HOLE	<u>96</u>	<u>.5692</u>	<u>41</u>	_____	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.
	DP	HWDP	DC			
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>9.5</u>	<u>21</u>	<u>30</u>	_____
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>20</u>	<u>27</u>	_____
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	<u>.3887</u>	<u>.7085</u>	_____
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0707</u>	_____	<u>.113</u>	_____
LENGTH-ft	_____	<u>303</u>	<u>102</u>	_____	_____	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>195</u>	_____	<u>450</u>	_____

REMARKS AND RECOMMENDATIONS

MW 8.5 GPM _____ JETS _____ ft/mi = _____ sec/std

ON LOCATION 8-30-93. DRILL PILOT HOLE WITH 26' PILOT BIT TO 230'. DRILL 24' GLORY HOLE FROM THE MUD LINE AT 172' TO 211'. LAND 24' PROTECTIVE CAISSON INSIDE OF GLORY HOLE. CONTINUE DRILLING WITH GLORY HOLE BIT WHILE WASHING DOWN CASSION TO 216'. LAND GUIDE BASE. RIH WITH 30' CONDUCTOR CSG IN CONJUNCTION WITH BIT NO. 1 AND MUD MOTOR. JET DRILL CASING. LAND 30' CASING AT 309'. DRILL AHEAD WITH BIT NO. 1.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 1040
 OPERATION R/U F/20'
 FOOTAGE 635

No. 2
 DATE Sep 11 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>3</u>	AT DEPTH (feet) <u>510</u>	SURVEY DATA <u>NA</u>	LITHOLOGY <u>NA</u>	SAMPLE DEPTH _____	TRIP CHLORIDES _____	DRILL RATE ft/hr <u>50</u>
BACKGROUND CONNECTION TRIP <u>0</u>	LAG DOWN DP <u>70</u>	LAG OFF BOTTOM <u>NA</u>	CORRECTED 'D' EXP. <u>.74</u>	SHALE DENSITY g/cc <u>NA</u>	EWR Res. _____		
FLOWLINE TEMP <u>33</u> degrees F							

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>137</u> psi	<u>8.5</u> ppg	<u>460</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>NA</u> psi	<u>NA</u> ppg	<u>660</u> psi	<u>12.2</u> ppg	_____ psi	_____ ppg
ECD	<u>137</u> psi	<u>8.5</u> ppg	<u>460</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>00:00 9/10/93</u>	BIT NO. <u>1</u>	PUMPS <u>1</u> ID-1600	<u>2</u> ID-1600
TYPE <u>DISPLACED MUD</u>	TYPE <u>ATXG1</u>	SIZE inches <u>7.5X12</u>	<u>7.5X12</u>
WEIGHT IN <u>9.6</u>	IADC CODE _____	CAPACITY gal/stk <u>6.54</u>	<u>6.54</u>
FUNNEL VIS. <u>58</u>	SIZE <u>26'</u>	PUMP RATE stks/min <u>71</u>	<u>71</u>
PV/YP <u>16/18</u>	JETS <u>3-21,1-22</u>	FLOW RATE gal/min <u>927</u>	
GELS <u>6/14</u>	DEPTH OUT <u>1040</u>	PRESSURE psi <u>1450</u>	
pH <u>9.5</u>	ROT HRS. <u>26.7</u>	PD SURF / DS psi <u>100/1000</u>	
FILT/CAKE API <u>13.0</u>	FOOTAGE <u>824</u>	ANN / BIT psi <u>0/350</u>	
HP-HT _____	AVG ft/hr <u>30.7</u>	JET VELOCITY ft/sec <u>215</u>	
P _m <u>-.4</u>	GRADE _____	JET IMPACT lbs <u>875</u>	
P _f /M _f <u>.2/5</u>	HOLE DEV. _____	BIT HP <u>190</u>	
CHLORIDES ppm <u>14000</u>	COST/FT <u>88</u>	HP RATIO / HP/IN2 <u>24% - .4/IN2</u>	
CALCIUM ppm <u>560</u>	RPM <u>165 (CALC)</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS _____	WOB <u>10</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____			

ANNULAR DATA

	LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5 X 27</u> DP-CSG	<u>93</u>	<u>.6842</u>	<u>32</u>	<u>NA</u>	
<u>5 X 26</u> DP-HOLE	<u>722</u>	<u>.6326</u>	<u>35</u>		
<u>9.0 x 27</u>		<u>.5905</u>			
<u>9.0 X 26</u> DC-HOLE	<u>102</u>	<u>.5692</u>	<u>38</u>		

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.
	DP	HWDP	DC			
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>9.5</u>		<u>21</u>	<u>30</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20</u>	<u>27</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>		<u>.3887</u>	<u>.7085</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0707</u>			<u>.113</u>
LENGTH-ft	<u>217</u>	<u>721</u>	<u>102</u>			<u>100</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>195</u>			<u>450</u>

REMARKS AND RECOMMENDATIONS

MW 8.7 GPM _____ JETS _____ ft/mi = _____ sec/std

DRILL AHEAD WITH BIT NO. 1 OCCASIONALLY PUMPING HIGH VIS SWEEPS TO CLEAN THE HOLE. SAND FORMATION INTERPRETED FROM NORMALIZED ROP DATA BETWEEN 770' - 990'. DRILL TO 1040'. CIRCULATE OUT HOLE VOLUME. PUMP HIGH VIS SWEEP. SHORT TRIP TO 30' CASING. PUMP HIGH VIS SWEEP. DISPLACE HOLE WITH 9.6 PPG MUD. POOH. RIG TO RUN 20' CASING.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 1040
OPERATION RUN BOP
FOOTAGE 0

No. 3
DATE Sep 12 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>3</u>	AT DEPTH (feet) <u>510</u>	SURVEY DATA <u>NA</u>	LITHOLOGY <u>NA</u>	SAMPLE DEPTH _____	TRIP CHLORIDES _____	DRILL RATE ft/hr <u>50</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>0</u>	FLOWLINE TEMP <u>33</u> degrees F	LAG DOWN DP <u>77</u>	LAG OFF BOTTOM <u>2750</u>	CORRECTED 'D' EXP. <u>.74</u>	SHALE DENSITY g/cc <u>NA</u>	EWR Res. _____

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>137</u> psi	<u>8.5</u> ppg	<u>460</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>NA</u> psi	<u>NA</u> ppg	<u>660</u> psi	<u>12.2</u> ppg	_____ psi	_____ ppg
ECD	<u>137</u> psi	<u>8.5</u> ppg	<u>460</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>00:00 9/11/93</u>	BIT NO. <u>1</u>	PUMPS <u>1.</u> ID-1600	<u>2.</u> ID-1600
TYPE <u>MUD IN HOLE</u>	TYPE <u>ATXG1</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.6</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>58</u>	SIZE <u>26"</u>	PUMP RATE stks/min _____	_____
PV/YP <u>16/18</u>	JETS <u>3-21,1-22</u>	FLOW RATE gal/min _____	_____
GELS <u>0/14</u>	DEPTH OUT <u>1040</u>	PRESSURE psi <u>STATIC PAST</u>	_____
pH <u>9.5</u>	ROT HRS. <u>26.7</u>	PD SURF / DS psi <u>24 HRS</u>	_____
FILT/CAKE API <u>13.0</u>	FOOTAGE <u>824</u>	ANN / BIT psi _____	_____
HP-HT _____	AVG ft/hr <u>30.7</u>	JET VELOCITY ft/sec _____	_____
P _m <u>.4</u>	GRADE _____	JET IMPACT lbs _____	_____
P _f /M _f <u>.2/.5</u>	HOLE DEV. _____	BIT HP _____	_____
CHLORIDES ppm <u>14000</u>	COST/FT <u>88</u>	HP RATIO / HP/IN2 _____	_____
CALCIUM ppm <u>560</u>	RPM <u>165 (CALC)</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS _____	WOB <u>10</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____			

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5 X 20</u>	<u>DP-RISER</u>	_____	<u>.3644</u>	_____	<u>NA</u>	_____
<u>5 X 18.73</u>	<u>DP-CSG</u>	_____	<u>.3166</u>	_____	_____	_____
<u>5 X 12.25</u>	<u>DP-HOLE</u>	_____	<u>.1215</u>	_____	_____	_____
<u>8.0 X 18.73</u>	<u>DC-CSG</u>	_____	<u>.3265</u>	_____	_____	_____
<u>8.0 X 12.25</u>	<u>DC-HOLE</u>	_____	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING:			
	DP	HWDP	DC	DEPTH	RISER	COND.	SURF.
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>
LENGTH-ft	_____	<u>721</u>	_____	_____	<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.6 GPM 650 JETS 4-12'S 3000 PSI _____ ft/mi = _____ sec/std

RUN 20' - 133 LD/FT CASING. LAND CASING AT 1022'. CEMENT 20' & 30' AT THE SAME TIME. START RUNNING BOP STACK.

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 1040
 OPERATION SQUEEZE
 FOOTAGE 0

No. 4
 DATE Sep 13 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>0</u>	AT DEPTH (feet) <u>0</u>	SURVEY DATA <u>NA</u>	LITHOLOGY <u>NA</u>	SAMPLE DEPTH <u>0</u>	TRIP CHLORIDES <u>0</u>	DRILL RATE ft/hr <u>50</u>
BACKGROUND CONNECTION TRIP <u>0</u>	FLOWLINE TEMP <u>33</u> degrees F		LAG DOWN DP <u>77</u>	LAG OFF BOTTOM <u>2750</u>			CORRECTED 'D' EXP. <u>.74</u>
							SHALE DENSITY g/cc <u>NA</u>
							EWR Res. <u>0</u>

FORMATION PRESSURE DATA

	CASING	BOTTOM HOLE	OPEN HOLE
PORE PRESSURE	<u>137</u> psi <u>8.5</u> ppg	<u>460</u> psi <u>8.5</u> ppg	<u>0</u> psi <u>0</u> ppg
FRACTURE PRESSURE	<u>NA</u> psi <u>NA</u> ppg	<u>660</u> psi <u>12.2</u> ppg	<u>0</u> psi <u>0</u> ppg
ECD	<u>137</u> psi <u>8.5</u> ppg	<u>460</u> psi <u>8.5</u> ppg	<u>0</u> psi <u>0</u> ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>00:00 9/12/93</u>	BIT NO. <u>1</u>	2	PUMPS <u>1</u>	1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>MUD IN PITS</u>	TYPE <u>ATXG1</u>	<u>SS335GJ4</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>	
WEIGHT IN <u>9.8</u>	IADC CODE <u>0</u>		CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>	
FUNNEL VIS. <u>53</u>	SIZE <u>26"</u>	<u>17.5</u>	PUMP RATE stks/min <u>70</u>	<u>70</u>	
PV/YP <u>18/19</u>	JETS <u>3-21,1-22</u>	<u>3-18,1-11</u>	FLOW RATE gal/min <u>689</u>		
GELS <u>4/4</u>	DEPTH OUT <u>1040</u>		PRESSURE psi <u>1200</u>		
pH <u>9.0</u>	ROT HRS. <u>26.7</u>		PD SURF / DS psi <u>90/580</u>		
FILT/CAKE API <u>4.4</u>	FOOTAGE <u>824</u>		ANN / BIT psi <u>0/530</u>		
HPHT <u>0</u>	AVG ft/hr <u>30.7</u>		JET VELOCITY ft/sec <u>264</u>		
P _m <u>-.4</u>	GRADE <u>0</u>		JET IMPACT lbs <u>800</u>		
Pf/Mf <u>.2/6</u>	HOLE DEV. <u>0</u>		BIT HP <u>212</u>		
CHLORIDES ppm <u>18000</u>	COST/FT <u>88</u>		HP RATIO / HP/IN2 <u>24% - .9/IN2</u>		
CALCIUM ppm <u>1800</u>	RPM <u>165 (CALC)</u>		REDUCED 1 <u>0</u> psi at <u>0</u> stk/min		
OIL/WATER/SOLIDS <u>0</u>	WOB <u>10</u>		RATE 2 <u>0</u> psi at <u>0</u> stk/min		
DAILY/CUM. COST <u>0</u>					

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>45</u>	<u>0</u>	<u>0</u>
<u>5 X 18.73</u>	<u>DP-CSG</u>	<u>845</u>	<u>.3166</u>	<u>52</u>	<u>0</u>	<u>0</u>
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>0</u>	<u>.1215</u>	<u>0</u>	<u>0</u>	<u>0</u>
<u>8.0 X 18.73</u>	<u>DC-CSG</u>	<u>0</u>	<u>.3285</u>	<u>0</u>	<u>0</u>	<u>0</u>
<u>8.0 X 12.25</u>	<u>DC-HOLE</u>	<u>0</u>	<u>.0836</u>	<u>0</u>	<u>0</u>	<u>0</u>

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	<u>0</u>	<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>0</u>	<u>20</u>	<u>30</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	<u>0</u>	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	<u>0</u>	<u>0</u>	<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>0</u>	<u>721</u>	<u>0</u>	<u>0</u>	<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	<u>0</u>	<u>0</u>	<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.6 GPM 650 JETS 4-12'S 3000 PSI 0 ft/mi = 0 sec/std

LAND AND TEST BOP STACK. ATTEMPT TO TEST CASING - NO TEST. RIH WITH 17.5' BIT. WASH DOWN TO FLOAT/SHOE. POOH.

RIH WITH STINGER. STING IN AND SUEEZE WITH 83 BBL OF CEMENT. PULL 4 STANDS. CO.

ADT J. PATTON

sperry-sun
DRILLING SERVICES *LOGGING SYSTEMS*
 A Baroid Company

DEPTH 1645
 OPERATION DRILLING
 FOOTAGE 595

No. 5
 DATE Sep 14 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>25</u>	MAX GAS (units) <u>44</u>	AT DEPTH (feet) <u>1625</u>	SURVEY DATA <u>.31 DEG @ 1548'</u>	LITHOLOGY <u>50% SAND 30% CLAY 20% SILT</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>46</u>	FLOWLINE TEMP <u>41</u> degrees F	SAMPLE DEPTH <u>1470</u>	TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP <u>155</u>	LAG OFF BOTTOM <u>3325</u>
			DRILL RATE ft/hr <u>105</u>	CORRECTED 'D' EXP. <u>.80</u>
			SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>2</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>452</u> psi	<u>8.5</u> ppg	<u>727</u> psi	<u>8.5</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>760</u> psi	<u>14.3</u> ppg	<u>1112</u> psi	<u>13.0</u> ppg	_____ psi	_____ ppg
ECD	<u>531</u> psi	<u>10.0</u> ppg	<u>855</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>00:00 9/13/93</u>	BIT NO. <u>3</u>	<u>2</u>	PUMPS <u>1.</u> ID-1600	<u>2.</u> ID-1600
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	<u>6S33SGJ4</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.7+</u>	IADC CODE _____	_____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>43</u>	SIZE <u>12.25</u>	<u>17.5</u>	PUMP RATE stks/min <u>65</u>	<u>65</u>
PV/YP <u>16/18</u>	JETS <u>3-13,1-12</u>	<u>3-18,1-11</u>	FLOW RATE gal/min <u>641</u>	_____
GELS <u>3/3</u>	DEPTH OUT _____	<u>1050</u>	PRESSURE psi _____	<u>2050</u>
pH <u>10.0</u>	ROT HRS. <u>5.9</u>	<u>.15</u>	PD SURF / DS psi _____	<u>90/465</u>
FILT/CAKE API _____	FOOTAGE <u>595</u>	<u>10</u>	ANN / BIT psi _____	<u>10/1485</u>
HP-HT _____	AVG ft/hr <u>101</u>	<u>60</u>	JET VELOCITY ft/sec _____	<u>412</u>
P _m <u>1.5</u>	GRADE <u>INC</u>	<u>2-2-1</u>	JET IMPACT lbs _____	<u>1340</u>
Pf/Mf <u>.4/1.3</u>	HOLE DEV. <u>.31</u>	_____	BIT HP _____	<u>555</u>
CHLORIDES ppm <u>17400</u>	COST/FT <u>326</u>	<u>NA</u>	HP RATIO / HP/IN2 <u>72% - .4.7/IN2</u>	_____
CALCIUM ppm <u>1560</u>	RPM <u>140</u>	<u>95</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>0/6.5/93.5</u>	WOB <u>0/10</u>	<u>10</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____	_____	_____	_____	_____

ANNULAR DATA

	LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u> DP-RISER	<u>177</u>	<u>.3644</u>	<u>42</u>	<u>211</u>	_____
<u>5 X 18.73</u> DP-CSG	<u>845</u>	<u>.3166</u>	<u>48</u>	<u>216</u>	_____
<u>5 X 12.25</u> DP-HOLE	<u>147</u>	<u>.1215</u>	<u>126</u>	<u>242</u>	_____
<u>8.0 X 12.25</u> DC-HOLE	<u>476</u>	<u>.0836</u>	<u>183</u>	<u>285</u>	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	_____	_____	_____
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>21</u>	<u>30</u>	<u>20</u>	_____
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	<u>20</u>	<u>27</u>	<u>18.73</u>	_____
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>	_____
LENGTH-ft	<u>442</u>	<u>727</u>	<u>476</u>	<u>177</u>	<u>100</u>	<u>812</u>	_____
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	<u>450</u>	<u>133</u>	_____

REMARKS AND RECOMMENDATIONS

MW 9.6 GPM 650 JETS 4-12'S 3000 PSI _____ ft/mi = _____ sec/std

CASING TESTED TO 2200 PSI FOR 30 MINUTES. RIH WITH BIT NO. 2. DRILLOUT CEMENT AND FLOAT/SHOE. DRILL 10' OF NEW HOLE.

CO. SPOT HIGH VIS PILL AT BOTTOM. DISPLACE HOLE WITH PHPA-POLY MUD SYSTEM. RUN LEAK OFF TEST = 14.3 PPG. POOH.

P/U NEW BIT 3 AND MWD TOOL. RIH. DRILL AHEAD THROUGH SAND AND CLAY.

ADT _____ J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 3100
OPERATION DRILLING
FOOTAGE 1455

NO. 6
DATE Sep 15 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>20</u>	MAX GAS (units) <u>56</u>	AT DEPTH (feet) <u>2340'</u>	SURVEY DATA <u>.47 DEG @ 2968'</u>
BACKGROUND CONNECTION TRIP <u>0</u>	TRIP <u>153</u>	FLOWLINE TEMP <u>37</u> degrees F	LITHOLOGY <u>30% SAND 50% CLAY 20% SILT</u>
			SAMPLE DEPTH <u>2970</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP <u>365</u>
			LAG OFF BOTTOM <u>4800</u>
			DRILL RATE ft/hr <u>80</u>
			CORRECTED 'D' EXP. <u>1.01</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>3</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>452</u> psi	<u>8.5</u> ppg	<u>1402</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>760</u> psi	<u>14.3</u> ppg	<u>2257</u> psi	<u>14.0</u> ppg	_____ psi	_____ ppg
ECD	<u>531</u> psi	<u>10.8</u> ppg	<u>1612</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>00:00 9/14/93</u>	BIT NO. <u>3</u>	<u>2</u>	PUMPS <u>1.</u>	<u>ID-1600</u>	<u>2.</u>	<u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	<u>SS33SGJ4</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>		
WEIGHT IN <u>9.7+</u>	IADC CODE _____		CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>		
FUNNEL VIS. <u>72</u>	SIZE <u>12.25</u>	<u>17.5</u>	PUMP RATE stks/min _____	<u>123</u>		
PV/YP <u>29/35</u>	JETS <u>3-13.1-12</u>	<u>3-18.1-11</u>	FLOW RATE gal/min _____	<u>605</u>		
GELS <u>4/5</u>	DEPTH OUT _____	<u>1050</u>	PRESSURE psi _____	<u>2050</u>		
pH <u>10.1</u>	ROT HRS. <u>21.1</u>	<u>.15</u>	PD SURF / DS psi _____	<u>90/605</u>		
FILT/CAKE API <u>3.2</u>	FOOTAGE <u>2050</u>	<u>10</u>	ANN / BIT psi _____	<u>25/1330</u>		
HP-HT _____	AVG ft/hr <u>97</u>	<u>60</u>	JET VELOCITY ft/sec _____	<u>389</u>		
P _m <u>1.3</u>	GRADE <u>INC</u>	<u>2-2-1</u>	JET IMPACT lbs _____	<u>1200</u>		
P _f /M _f <u>1.1/2.7</u>	HOLE DEV. <u>.47</u>		BIT HP _____	<u>470</u>		
CHLORIDES ppm <u>17300</u>	COST/FT <u>295</u>	<u>NA</u>	HP RATIO / HP/IN2 _____	<u>65% - 4.0/IN2</u>		
CALCIUM ppm <u>880</u>	RPM <u>130</u>	<u>95</u>	REDUCED 1 _____ psi at _____ stk/min			
OIL/WATER/SOLIDS <u>0/7/93</u>	WOB <u>20</u>	<u>10</u>	RATE 2 _____ psi at _____ stk/min			
DAILY/CUM. COST _____						

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>40</u>	<u>331</u>	
<u>5 X 18.73</u>	<u>DP-CSG</u>	<u>845</u>	<u>.3166</u>	<u>45</u>	<u>340</u>	
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>1602</u>	<u>.1215</u>	<u>119</u>	<u>377</u>	
<u>8.0 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>173</u>	<u>440</u>	

PIPE DATA

	DP	HWDP	DRILL STRING	DC	CASING: DEPTH	RISER	COND.	SURF.
OD-inches	<u>5.0</u>	<u>5.0</u>		<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>		<u>2.875</u>		<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>		<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>		<u>.0542</u>			<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>1897</u>	<u>727</u>		<u>476</u>		<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>		<u>147</u>			<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.6 GPM 650 JETS 4-12'S 3000 PSI _____ ft/mi = _____ sec/std

DRILL AHEAD WITH BIT NO. 3. DRILL TO 2336'. CO. SHORT TRIP TO SHOE. HOLE TRYING TO SWAB ON WAY OUT. PUMP AND BACK REAM FROM STAND NO. 6. MAX GAS FROM TRIP = 153 UNITS. DRILL AHEAD. # 1 PUMP DOWN FOR MOST OF DAY.

ADT _____ J. PATTON

sperry-sun **LOGGING SYSTEMS**
DRILLING SERVICES
 A Baroid Company

DEPTH 3705
 OPERATION POOH
 FOOTAGE 705

No. 7
 DATE Sep 16 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>10</u>	MAX GAS (units) <u>60</u>	AT DEPTH (feet) <u>3400'</u>	SURVEY DATA <u>..22 DEG @ 3676'</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>313</u>	FLOWLINE TEMP <u>37</u> degrees F	LITHOLOGY <u>10% SAND 80% CLAY 10% SILT</u>
			SAMPLE DEPTH <u>3700</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP <u>365</u>
			LAG OFF BOTTOM <u>4800</u>
			DRILL RATE ft/hr <u>45</u>
			CORRECTED "D" EXP. <u>.90</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>3</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>452</u> psi	<u>8.5</u> ppg	<u>1676</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>760</u> psi	<u>14.3</u> ppg	<u>2735</u> psi	<u>14.5</u> ppg	_____ psi	_____ ppg
ECD	<u>531</u> psi	<u>10.0</u> ppg	<u>1927</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>21:30 9/15/93</u>	BIT NO. <u>3</u>	<u>2</u>	PUMPS <u>1.</u>	ID-1600	<u>2.</u>	ID-1600
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	<u>SS33SGJ4</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>		
WEIGHT IN <u>9.9</u>	IADC CODE _____		CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>		
FUNNEL VIS. <u>82</u>	SIZE <u>12.25</u>	<u>17.5</u>	PUMP RATE stks/min <u>66</u>	<u>67</u>		
PV/YP <u>37/44</u>	JETS <u>3-13.1-12</u>	<u>3-18.1-11</u>	FLOW RATE gal/min <u>653</u>			
GELS <u>6/9</u>	DEPTH OUT <u>3705</u>	<u>1050</u>	PRESSURE psi <u>2700</u>			
pH <u>19.8</u>	ROT HRS. <u>28.0</u>	<u>.15</u>	PD SURF / DS psi <u>100/1020</u>			
FILT/CAKE API <u>2.2</u>	FOOTAGE <u>2655</u>	<u>10</u>	ANN / BIT psi <u>40/1540</u>			
HP-HT _____	AVG ft/hr <u>95</u>	<u>60</u>	JET VELOCITY ft/sec <u>420</u>			
P _m <u>1.2</u>	GRADE <u>INC</u>	<u>2-2-I</u>	JET IMPACT lbs <u>1390</u>			
Pf/Mf <u>.9/2.3</u>	HOLE DEV. <u>.22</u>		BIT HP <u>587</u>			
CHLORIDES ppm <u>17100</u>	COST/FT <u>297</u>	<u>NA</u>	HP RATIO / HP/IN2 <u>57% - .5.0/IN2</u>			
CALCIUM ppm <u>680</u>	RPM <u>140</u>	<u>95</u>	REDUCED 1 _____ psi at _____ stk/min			
OIL/WATER/SOLIDS <u>0/7/93</u>	WOB <u>15</u>	<u>10</u>	RATE 2 _____ psi at _____ stk/min			
DAILY/CUM. COST _____						

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>43</u>	<u>386</u>	
<u>5 X 18.73</u>	<u>DP-C&G</u>	<u>845</u>	<u>.3166</u>	<u>49</u>	<u>395</u>	
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>2207</u>	<u>.1215</u>	<u>128</u>	<u>440</u>	
<u>8.0 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>186</u>	<u>515</u>	

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	<u>21</u>	<u>309</u>	<u>1022</u>	
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>20</u>	<u>27</u>	<u>18.73</u>	
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>	
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>		<u>.113</u>	<u>.0478</u>	
LENGTH-ft	<u>2502</u>	<u>727</u>	<u>476</u>	<u>177</u>	<u>100</u>	<u>812</u>	
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>		<u>450</u>	<u>133</u>	

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 650 JETS 4-12'S 3000 PSI _____ ft/mi = _____ sec/std

DRILL AHEAD WITH BIT NO. 3. DRILL TO 3705'. CO. SHORT TRIP TO SHOE. HOLE TRYING TO SWAB ON WAY OUT. PUMP AND BACK REAM FROM STAND NO. 6. MAX GAS FROM TRIP = 313 UNITS. CIRCULATE AND CONDITION HOLE. POOH. EXCESS DRAG NOTED WHEN BHA REACHED THE 20' SHOE. HOLE AGAIN TRYING TO SWAB. OBSERVE WELL. POOH FOR E-LOGS.

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 3705
 OPERATION W.O.W.
 FOOTAGE 0

NO. 9
 DATE Sep 18 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>0</u>	AT DEPTH (feet) <u>3705</u>	SURVEY DATA <u>.22 DEG @ 3676'</u>
BACKGROUND CONNECTION TRIP <u>0</u>	FLOWLINE TEMP <u>41</u> degrees F	LITHOLOGY <u>10% SAND 80% CLAY 10% SILT</u>	SAMPLE DEPTH <u>3700</u>
TRIP <u>214</u>		TRIP CHLORIDES <u>NA</u>	DRILL RATE ft/hr <u>45</u>
		LAG DOWN DP <u>365</u>	CORRECTED 'D' EXP. <u>.90</u>
		LAG OFF BOTTOM <u>4800</u>	SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>3</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>452</u> psi	<u>8.5</u> ppg	<u>1676</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>760</u> psi	<u>14.3</u> ppg	<u>2735</u> psi	<u>14.5</u> ppg	_____ psi	_____ ppg
ECD	<u>531</u> psi	<u>10.0</u> ppg	<u>1927</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>22:00 9/17/93</u>	BIT NO. <u>3</u>	<u>2</u>	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	<u>SS33SGJ4</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.0</u>	IADC CODE _____	_____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>54</u>	SIZE <u>12.25</u>	<u>17.5</u>	PUMP RATE stks/min _____	_____
PV/YP <u>21/26</u>	JETS <u>3-13,1-12</u>	<u>3-18,1-11</u>	FLOW RATE gal/min _____	_____
GELS <u>3/4</u>	DEPTH OUT <u>3705</u>	<u>1050</u>	PRESSURE psi _____	<u>STATIC</u>
pH <u>9.5</u>	ROT HRS. <u>28.0</u>	<u>.15</u>	PD SURF / DS psi _____	<u>PAST 24 HRS.</u>
FILT/CAKE API <u>2.8</u>	FOOTAGE <u>2655</u>	<u>10</u>	ANN / BIT psi _____	_____
HP-HT _____	AVG ft/hr <u>95</u>	<u>60</u>	JET VELOCITY ft/sec _____	_____
P _m <u>.5</u>	GRADE <u>INC</u>	<u>2-2-1</u>	JET IMPACT lbs _____	_____
Pf/Mf <u>.5/1.3</u>	HOLE DEV. <u>.22</u>	_____	BIT HP _____	_____
CHLORIDES ppm <u>17000</u>	COST/FT <u>297</u>	<u>NA</u>	HP RATIO / HP/IN2 _____	_____
CALCIUM ppm <u>480</u>	RPM <u>140</u>	<u>95</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>0/8/92</u>	WOB <u>15</u>	<u>10</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	_____	_____	_____
<u>5 X 18.73</u>	<u>DP-CSG</u>	<u>845</u>	<u>.3166</u>	_____	_____	_____
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>2207</u>	<u>.1215</u>	_____	_____	_____
<u>8.0 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	<u>21</u>	<u>30</u>	<u>20</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>2502</u>	<u>727</u>	<u>476</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 650 JETS 4-12'S 3000 PSI _____ ft/mi = _____ sec/std

COMPLETE ELECTRIC LOGS. DISPLCE RISER WITH SEA WATER AND DISCONNECT FROM WELL BECAUSE OF ROUGH WEATHER.
 WAIT ON CONDITIONS TO IMPROVE.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 3705 (3375)
 OPERATION OPEN HOLE
 FOOTAGE 2325

No. 10
 DATE Sep 19 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>20</u>	MAX GAS (units) <u>35</u>	AT DEPTH (feet) <u>1680</u>	SURVEY DATA <u>.22 DEG @ 3676'</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>0</u>	FLOWLINE TEMP <u>45</u> degrees F	LITHOLOGY <u>10% SAND 80% CLAY 10% SILT</u>
			SAMPLE DEPTH <u>3700</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP <u>427</u>
			LAG OFF BOTTOM <u>8250</u>
			DRILL RATE ft/hr <u>200</u>
			CORRECTED 'D' EXP. <u>.85</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>_____</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>452</u> psi	<u>8.5</u> ppg	<u>1676</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>760</u> psi	<u>14.3</u> ppg	<u>2735</u> psi	<u>14.5</u> ppg	_____ psi	_____ ppg
ECD	<u>531</u> psi	<u>10.0</u> ppg	<u>1927</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>22:00 9/18/93</u>	BIT NO. <u>3</u>	RR3 (4)	PUMPS <u>1.</u>	ID-1600	2. ID-1600
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	FDTC/H.O.	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>	
WEIGHT IN <u>9.9</u>	IADC CODE _____		CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>	
FUNNEL VIS. <u>60</u>	SIZE <u>12.25</u>	<u>17.5</u>	PUMP RATE stks/min <u>111</u>	<u>110</u>	
PV/YP <u>29/34</u>	JETS <u>3-13.1-12</u>	TFA: <u>1.44</u>	FLOW RATE gal/min <u>1086</u>		
GELS <u>4/6</u>	DEPTH OUT <u>3705</u>	NA	PRESSURE psi <u>2500</u>		
pH <u>9.7</u>	ROT HRS. <u>28.0</u>	<u>11.3</u>	PD SURF / DS psi <u>125/1935</u>		
FILT/CAKE API <u>2.0</u>	FOOTAGE <u>2655</u>	<u>2325</u>	ANN / BIT psi <u>25/515</u>		
HP-HT _____	AVG ft/hr <u>95</u>	<u>205</u>	JET VELOCITY ft/sec <u>240</u>		
P _m <u>.5</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u>1335</u>		
Pf/Mf <u>.5/1.5</u>	SOLE DEV. <u>.22</u>		BIT HP <u>325</u>		
CHLORIDES ppm <u>17000</u>	COST/FT <u>297</u>	NA	HP RATIO / HP/IN2 <u>21% - 1.3/IN2</u>		
CALCIUM ppm <u>240</u>	RPM <u>140</u>	<u>145</u>	REDUCED 1 _____ psi at _____ stk/min		
OIL/WATER/SOLIDS <u>0/7.5/92.5</u>	WOB <u>15</u>	<u>10-20</u>	RATE 2 _____ psi at _____ stk/min		
DAILY/CUM. COST _____					

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>71</u>		
<u>5 X 18.73</u>	<u>DP-CSG</u>	<u>845</u>	<u>.3166</u>	<u>82</u>		
<u>5 X 17.5</u>	<u>DP-HOLE</u>	<u>2056</u>	<u>.2733</u>	<u>95</u>		
<u>8.0 X 17.5</u>	<u>DC-HOLE</u>	<u>297</u>	<u>.2354</u>	<u>111</u>		

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20</u>	<u>30</u>	<u>20</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>18.73</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>			<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>2351</u>	<u>727</u>	<u>297</u>		<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>			<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 900 JETS _____ ft/mi = _____ sec/std

LATCH RISER. RIH WITH 17.5' HOLE OPENER. OPENING HOLE TO 17.5'.

sperry-sun *LOGGING SYSTEMS*

DRILLING SERVICES
A Baroid Company

DEPTH 3705
OPERATION RUN 13 3/8'
FOOTAGE 0

No. 11
DATE Sep 20 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>0</u>	AT DEPTH (feet) <u>3705</u>	SURVEY DATA <u>.22 DEG @ 3676'</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>114</u>	FLOWLINE TEMP <u>45</u> degrees F	LITHOLOGY <u>10% SAND 80% CLAY 10% SILT</u>
			SAMPLE DEPTH <u>3700</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP <u>427</u>
			LAG OFF BOTTOM <u>8250</u>
			DRILL RATE ft/hr <u>200</u>
			CORRECTED 'D' EXP. <u>.85</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u> </u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>452</u> psi	<u>8.5</u> ppg	<u>1676</u> psi	<u>8.7</u> ppg	psi	ppg
FRACTURE PRESSURE	<u>760</u> psi	<u>14.3</u> ppg	<u>2735</u> psi	<u>14.5</u> ppg	psi	ppg
ECD	<u>531</u> psi	<u>10.0</u> ppg	<u>1927</u> psi	<u>10.0</u> ppg	psi	ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>22:00 9/19/93</u>	BIT NO. <u>3</u>	RR3 (4)	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	<u>FDTC/H.O.</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8+</u>	IADC CODE		CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>80</u>	SIZE <u>12.25</u>	<u>17.5</u>	PUMP RATE stks/min <u>111</u>	<u>110</u>
PV/YP <u>30/42</u>	JETS <u>3-13,1-12</u>	<u>TFA: 1.44</u>	FLOW RATE gal/min <u>1086</u>	
GELS <u>5/9</u>	DEPTH OUT <u>3705</u>	<u>3705</u>	PRESSURE psi <u>2500</u>	
pH <u>9.5</u>	ROT HRS. <u>28.0</u>	<u>13.3</u>	PD SURF / DS psi <u>125/1935</u>	
FILT/CAKE API <u>3.6</u>	FOOTAGE <u>2655</u>	<u>2655</u>	ANN / BIT psi <u>25/515</u>	
HP-HT	AVG ft/hr <u>95</u>	<u>200</u>	JET VELOCITY ft/sec <u>240</u>	
Pm <u>.6</u>	GRADE <u>INC</u>	<u>INC</u>	JET IMPACT lbs <u>1335</u>	
Pf/Mf <u>.5/2.5</u>	HOLE DEV. <u>.22</u>		BIT HP <u>325</u>	
CHLORIDES ppm <u>16800</u>	COST/FT <u>297</u>	<u>NA</u>	HP RATIO / HP/IN2 <u>21% - 1.3/IN2</u>	
CALCIUM ppm <u>100</u>	RPM <u>140</u>	<u>145</u>	REDUCED 1 <u> </u> psi at <u> </u> stk/min	
OIL/WATER/SOLIDS <u>0/7.5/92.5</u>	WOB <u>15</u>	<u>15</u>	RATE 2 <u> </u> psi at <u> </u> stk/min	
DAILY/CUM. COST				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
5 X 20	DP-RISER	<u>177</u>	<u>.3644</u>	<u>71</u>		
5 X 18.73	DP-CSG	<u>845</u>	<u>.3166</u>	<u>82</u>		
5 X 17.5	DP-HOLE	<u>2056</u>	<u>.2733</u>	<u>95</u>		
8.0 X 17.5	DC-HOLE	<u>297</u>	<u>.2354</u>	<u>111</u>		

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>			<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>2351</u>	<u>727</u>	<u>297</u>		<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>			<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 700 JETS 2-12,3-13'S ft/mi = sec/std

OPENING HOLE TO 17.5' TO 3705'. CIRCULATE OUT. PUMP HIGH VIS SWEEP. SHORT TRIP TO SHOE. PUMP OUT OF HOLE ON LAST THREE STANDS AT CASING SHOE. MAX GAS FROM SHORT TRIP = 114 UNITS. CIRCULATE AND CONDITION HOLE. POOH. RIG UP FOR RUNNING CASING. RUN 13 3/8' - 68 LB/FT CASING.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 3705
 OPERATION C. DRLG LINE
 FOOTAGE 0

No. 12
 DATE Sep 21 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>35</u>	AT DEPTH (feet) <u>3705</u>	SURVEY DATA <u>.22 DEG @ 3676'</u>
BACKGROUND CONNECTION <u>0</u>	TRIP <u>35</u>	FLOWLINE TEMP <u>45</u> degrees F	LITHOLOGY <u>10% SAND 80% CLAY 10% SILT</u>
			SAMPLE DEPTH <u>3700</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP <u>475</u>
			LAG OFF BOTTOM <u>4200</u>
			DRILL RATE ft/hr _____
			CORRECTED 'D' EXP. _____
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. _____

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1627</u> psi	<u>8.7</u> ppg	<u>1676</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	_____ psi	<u>NA</u> ppg	<u>2735</u> psi	<u>14.5</u> ppg	_____ psi	_____ ppg
ECD	_____ psi	_____ ppg	_____ psi	_____ ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>22:00 9/20/93</u>	BIT NO. <u>3</u>	<u>4</u>	PUMPS <u>1.</u>	<u>ID-1600</u>	<u>2.</u>	<u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	<u>DS40-H</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>		
WEIGHT IN <u>9.9</u>	IADC CODE _____	<u>PDC</u>	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>		
FUNNEL VIS. <u>62</u>	SIZE <u>12.25</u>	<u>12.25</u>	PUMP RATE stks/min _____			
PV/YP <u>22/21</u>	JETS <u>3-13,1-12</u>	<u>5-13'S</u>	FLOW RATE gal/min _____			
GELS <u>3/6</u>	DEPTH OUT <u>3705</u>		PRESSURE psi <u>STATIC</u>			
pH <u>9.9</u>	ROT HRS. <u>28.0</u>		PD SURF / DS psi _____			
FILT/CAKE API <u>2.4</u>	FOOTAGE <u>2655</u>		ANN / BIT psi _____			
HPHT _____	AVG ft/hr <u>95</u>		JET VELOCITY ft/sec _____			
Pm <u>.6</u>	GRADE <u>INC</u>		JET IMPACT lbs _____			
PF/Mf <u>.6/1.9</u>	HOLE DEV. <u>.22</u>		BIT HP _____			
CHLORIDES ppm <u>17000</u>	COST/FT <u>297</u>		HP RATIO / HP/IN2 _____			
CALCIUM ppm <u>320</u>	RPM <u>140</u>		REDUCED <u>1</u> _____ psi at _____ stk/min			
OIL/WATER/SOLIDS <u>0/7.5/92.5</u>	WOB <u>15</u>		RATE <u>2</u> _____ psi at _____ stk/min			
DAILY/CUM. COST _____						

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>			
<u>5 X 18.73</u>	<u>DP-CSG</u>		<u>.3166</u>			
<u>5 X 12.25</u>	<u>DP-HOLE</u>		<u>.1215</u>			
<u>8.0 X 12.25</u>	<u>DC-HOLE</u>		<u>.0836</u>			

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>			<u>.113</u>	<u>.0478</u>
LENGTH-ft					<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>			<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 700 JETS 2-12,3-13'S _____ ft/mi = _____ sec/std

LAND 13 3/8" CASING. SHOE DEPTH AT 3681'. CIRCULATE AND CONDITION HOLE BEHIND CASING. MAX GAS FROM BOTTOM = 35 UNITS.

PUMP AP. 388 BBL OF CEMENT AND DISPLACE WITH MUD. TEST BOP. SLIP AND CUT DRILL LINE.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 3705
 OPERATION W.O.W.
 FOOTAGE 0

NO. 13
 DATE Sep 22 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUYLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>0</u>	MAX GAS (units) <u>0</u>	AT DEPTH (feet) <u>3600</u>	SURVEY DATA <u>.22 DEG @ 3676'</u>
BACKGROUND CONNECTION TRIP <u>0</u>	FLOWLINE TEMP <u>60</u> degrees F	LITHOLOGY <u>10% SAND 80% CLAY 10% SILT</u>	SAMPLE DEPTH <u>3700</u>
TRIP CHLORIDES <u>NA</u>	LAG DOWN DP <u>475</u>	LAG OFF BOTTOM <u>4200</u>	DRILL RATE ft/hr <u>NA</u>
			CORRECTED "D" EXP. <u>NA</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>NA</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1627</u> psi	<u>8.7</u> ppg	<u>1676</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	_____ psi	<u>NA</u> ppg	<u>2735</u> psi	<u>14.5</u> ppg	_____ psi	_____ ppg
ECD	<u>1914</u> psi	<u>10.0</u> ppg	<u>1927</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>22:00 9/21/93</u>	BIT NO. <u>4</u>	5	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDSS</u>	<u>40-HF</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8</u>	IADC CODE _____	<u>PDC</u>	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>58</u>	SIZE <u>12.25</u>	<u>12.25</u>	PUMP RATE stks/min <u>72</u>	<u>73</u>
PV/YP <u>19/20</u>	JETS <u>3-13,1-12</u>	<u>5-13'S</u>	FLOW RATE gal/min <u>712</u>	_____
GELS <u>3/4</u>	DEPTH OUT <u>3705</u>	<u>3600</u>	PRESSURE psi _____	<u>2450</u>
pH <u>9.0</u>	ROT HRS. <u>28.0</u>	_____	PD SURF / DS psi _____	<u>100/1240</u>
FILT/CAKE API <u>3.4</u>	FOOTAGE <u>2655</u>	<u>0</u>	ANN / BIT psi _____	<u>20/1090</u>
HP-HT _____	AVG ft/hr <u>95</u>	_____	JET VELOCITY ft/sec _____	<u>352</u>
P _m <u>.6</u>	GRADE <u>INC</u>	_____	JET IMPACT lbs _____	<u>1273</u>
Pf/Mf <u>.25/1.5</u>	HOLE DEV. <u>.22</u>	_____	BIT HP _____	<u>450</u>
CHLORIDES ppm <u>17000</u>	COST/FT <u>297</u>	_____	HP RATIO / HP/IN2 _____	<u>45% - 3.8/IN2</u>
CALCIUM ppm <u>360</u>	RPM <u>140</u>	<u>50-120</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>0/7.2/92.8</u>	WOB <u>15</u>	<u>0-20</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____				

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>47</u>	<u>223</u>	_____
<u>5 X 12.415</u>	<u>DP-C&G</u>	<u>2947</u>	<u>.1255</u>	<u>135</u>	<u>278</u>	_____
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>-</u>	<u>.1215</u>	_____	_____	_____
<u>8 X 12.415</u>	_____	<u>476</u>	<u>.0876</u>	<u>194</u>	<u>327</u>	_____
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>-</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING			CASING:			
	DP	HWDP	DC	DEPTH	RISER	COND.	SURF.
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>2397</u>	<u>727</u>	<u>476</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 700 JETS 2-12,3-13'S _____ ft/mi = _____ sec/std

RIH WITH BIT NO. 4 - PDC TYPE. TEST CASING. ATTEMPT TO DRILL OUT FLOAT COLLAR AFTER TAGGING UP. BIT WOULD NOT DRILL.

POOH TO CHANGE BIT. DISPLACE RISER WITH SEA WATER AND DISCONNECT - WAIT ON WEATHER CONDITIONS TO IMPROVE.

ADT _____ J. PATTON

sperry-sun *LOGGING SYSTEMS*

DRILLING SERVICES
A Baroid Company

DEPTH 3705
OPERATION W.O.W.
FOOTAGE 0

No. 14
DATE Sep 23 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

BACKGROUND	AVG GAS (units) <u>0</u>	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>.22 DEG @ 3676'</u>	LITHOLOGY <u>10% SAND 80% CLAY 10% SILT</u>
CONNECTION	TRIP <u>10</u>	TRIP CHLORIDES <u>NA</u>	LAG DOWN DP <u>475</u>	DRILL RATE ft/hr <u>NA</u>	CORRECTED 'D' EXP. <u>NA</u>
TRIP	FLOWLINE TEMP <u>60</u> degrees F	LAG OFF BOTTOM <u>4200</u>	SHALE DENSITY g/cc <u>NA</u>	EWR Res. _____	

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1627</u> psi	<u>8.7</u> ppg	<u>1676</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	_____ psi	<u>NA</u> ppg	<u>2735</u> psi	<u>14.5</u> ppg	_____ psi	_____ ppg
ECD	<u>1914</u> psi	<u>10.0</u> ppg	<u>1927</u> psi	<u>10.0</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>22:00 9/22/93</u>	BIT NO. _____	PUMPS 1. <u>ID-1600</u> 2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>40-HF</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>9.7+</u>	IADC CODE <u>PDC</u>	CAPACITY gal/stk <u>4.92</u> <u>4.92</u>
FUNNEL VIS. <u>56</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____
PV/YP <u>18/20</u>	JETS <u>5-13'S</u>	FLOW RATE gal/min _____
GELS <u>3/4</u>	DEPTH OUT <u>3600</u>	PRESSURE psi <u>STATIC PAST</u>
pH <u>9.0</u>	ROT HRS. _____	PD SURF / DS psi <u>24 HRS</u>
FILT/CAKE API <u>3.4</u>	FOOTAGE <u>0</u>	ANN / BIT psi _____
HP-HT <u>8.0</u>	AVG ft/hr _____	JET VELOCITY ft/sec _____
Pm <u>.6</u>	GRADE _____	JET IMPACT lbs _____
Pf/Mf <u>.25/1.5</u>	HOLE DEV. _____	BIT HP _____
CHLORIDES ppm <u>17000</u>	COST/FT _____	HP RATIO / HP/IN2 _____
CALCIUM ppm <u>360</u>	RPM _____	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>0/7.2/92.8</u>	WOB _____	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	_____	_____	_____
<u>5 X 12.415</u>	<u>DP-CSG</u>	<u>2947</u>	<u>.1255</u>	_____	_____	_____
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>-</u>	<u>.1215</u>	_____	_____	_____
<u>8 X 12.415</u>	<u>-</u>	<u>476</u>	<u>.0876</u>	_____	_____	_____
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>-</u>	<u>.0836</u>	_____	_____	_____

PIPE DATA

	DRILL STRING				CASING: DEPTH	RISER	COND.	SURF.	
	DP	HWDP		DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	_____	<u>8.0</u>	_____	<u>21</u>	<u>309</u>	<u>1022</u>	<u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	_____	<u>2.875</u>	_____	<u>20</u>	<u>30</u>	<u>20</u>	<u>13 3/8</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	_____	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	_____	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>	<u>.0240</u>
LENGTH-ft	<u>2397</u>	<u>727</u>	_____	<u>476</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>	<u>3774</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	_____	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

WAIT ON WEATHER CONDITIONS TO IMPROVE.

ADT J. PATTON

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 4285
 OPERATION DRILL
 FOOTAGE 604

NO. 15
 DATE Sep 24 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>35</u>	MAX GAS (units) <u>303</u>	AT DEPTH (feet) <u>4058</u>	SURVEY DATA <u>.51 @ 4274'</u>
BACKGROUND CONNECTION TRIP <u>8</u>	FLOWLINE TEMP <u>80</u> degrees F	LITHOLOGY <u>50% CLAY 20% SLT 30 % SAND TR COAL</u>	SAMPLE DEPTH <u>3960</u>
TRIP CHLORIDES <u>NA</u>	LAG DOWN DP <u>540</u>	LAG OFF BOTTOM <u>4751</u>	DRILL RATE ft/hr <u>110</u>
			CORRECTED 'D' EXP. <u>1.16</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>3.09</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi	<u>8.7</u> ppg	<u>1863</u> psi	<u>8.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>2871</u> psi	<u>14.8</u> ppg	<u>2871</u> psi	<u>15.0</u> ppg	_____ psi	_____ ppg
ECD	<u>1933</u> psi	<u>10.1</u> ppg	<u>2272</u> psi	<u>10.2</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 23 SEP 93</u>	BIT NO. <u>6</u>	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>FDT</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8+</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>62</u>	SIZE <u>12.25</u>	PUMP RATE stks/min <u>68</u>	<u>67</u>
PV/YP <u>23/25</u>	JETS <u>3X13 1-12</u>	FLOW RATE gal/min <u>334</u>	<u>329</u>
GELS <u>3/5</u>	DEPTH OUT _____	PRESSURE psi <u>2775</u>	
pH <u>9.0</u>	ROT HRS. <u>5.9</u>	PD SURF / DS psi <u>83/1145</u>	
FILT/CAKE API <u>3.8/1</u>	FOOTAGE <u>604</u>	ANN / BIT psi <u>30/1617</u>	
HPHT <u>6.8</u>	AVG ft/hr <u>102</u>	JET VELOCITY ft/sec <u>426</u>	
P _m <u>.25</u>	GRADE _____	JET IMPACT lbs <u>1452</u>	
P _f /M _f <u>.15/2.9</u>	HOLE DEV. <u>.51</u>	BIT HP <u>628</u>	
CHLORIDES ppm <u>17000</u>	COST/FT _____	HP RATIO / HP/IN2 <u>7.8/in2</u>	
CALCIUM ppm <u>360</u>	RPM <u>135</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>0/8/92</u>	WOB <u>15/25</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____			

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>43</u>	<u>260</u>	<u>65</u>
<u>5 X 12.415</u>	<u>DP-CSG</u>	<u>3504</u>	<u>.1255</u>	<u>126</u>	<u>322</u>	<u>440</u>
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>128</u>	<u>.1215</u>	<u>130</u>	<u>324</u>	<u>16</u>
<u>8 X 12.415</u>						
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>189</u>	<u>381</u>	<u>40</u>

PIPE DATA

	DP	HWDP	DRILL STRING	DC	CASING: DEPTH	RISER	COND.	SURF.
OD-inches	<u>5.0</u>	<u>5.0</u>		<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>		<u>2.875</u>		<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>		<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>		<u>.0542</u>			<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>3082</u>	<u>727</u>		<u>476</u>		<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>		<u>147</u>			<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

WAIT ON WEATHER CONDITIONS TO IMPROVE. RIH WITH NB 4 AND MWD TOOL. TEST CASING TO 3000 psi. DRILL FLOAT COLLAR, SHOE AND 20' OF FORMATION. LEAKOFF TEST PERFORMED TO 14.8 ppg EQUIVALENT MUD WEIGHT. DRILL AHEAD THRU SAND/SILT TO 4285'.

ADT _____ D. WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 5475
 OPERATION DRILL
 FOOTAGE 890

No. 16
 DATE Sep 25 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>85</u>	MAX GAS (units) <u>324</u>	AT DEPTH (feet) <u>5470</u>	SURVEY DATA <u>.19 @ 5400</u>
BACKGROUND CONNECTION TRIP FLOWLINE TEMP <u>82</u> degrees F	LITHOLOGY <u>60% CLAY 20% SLT 20 % SAND</u>	SAMPLE DEPTH <u>5310</u>	DRILL RATE ft/hr <u>109</u>
	TRIP CHLORIDES <u>NA</u>	LAG DOWN DP <u>735</u>	CORRECTED 'D' EXP. <u>.78</u>
	LAG OFF BOTTOM <u>6140</u>	SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>4.00</u>

FORMATION PRESSURE DATA

CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi <u>8.7</u> ppg	<u>2533</u> psi <u>8.9</u> ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ ft
FRACTURE PRESSURE	<u>2871</u> psi <u>15</u> ppg	<u>4270</u> psi <u>15.0</u> ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ ft
ECD	<u>1971</u> psi <u>10.3</u> ppg	<u>2960</u> psi <u>10.4</u> ppg	_____ psi _____ ppg	_____ psi _____ ppg	_____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 24 SEP 93</u>	BIT NO. <u>7</u>	6	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	<u>FDT</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>9.8+</u>	IADC CODE _____	_____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>62</u>	SIZE <u>12.25</u>	<u>12.25</u>	PUMP RATE stks/min <u>70</u>	<u>70</u>
PV/YP <u>29/27</u>	JETS <u>TFA .751</u>	<u>3X13, 1-12</u>	FLOW RATE gal/min <u>344</u>	<u>344</u>
GELS <u>3/7</u>	DEPTH OUT <u>4585</u>	_____	PRESSURE psi _____	<u>2210</u>
pH <u>9.0</u>	ROT HRS. <u>9.0</u>	<u>9.1</u>	PD SURF / DS psi _____	<u>54/1431</u>
FILT/CAKE API <u>3.4/1</u>	FOOTAGE <u>891</u>	<u>880</u>	ANN / BIT psi <u>41/765</u>	_____
HP-HT <u>7.8</u>	AVG ft/hr <u>99</u>	<u>96</u>	JET VELOCITY ft/sec <u>293</u>	_____
P _m <u>.5</u>	GRADE _____	_____	JET IMPACT lbs <u>1034</u>	_____
Pf/Mf <u>.2/2.8</u>	HOLE DEV. <u>.19</u>	<u>.51</u>	BIT HP <u>307</u>	_____
CHLORIDES ppm <u>17000</u>	COST/FT _____	<u>379</u>	HP RATIO / HP/IN2 <u>15.9 hp/in2</u>	_____
CALCIUM ppm <u>240</u>	RPM <u>160</u>	<u>131</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>TR/7.5/92.5</u>	WOB <u>2/3</u>	<u>22</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____	_____	_____	_____	_____

ANNULAR DATA

	LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
5 X 20 DP-RISER	<u>177</u>	<u>.3644</u>	<u>45</u>	<u>262</u>	<u>65</u>
5 X 12.415 DP-CSG	<u>3504</u>	<u>.1255</u>	<u>131</u>	<u>333</u>	<u>583</u>
5 X 12.25 DP-HOLE	<u>1318</u>	<u>.1215</u>	<u>135</u>	<u>326</u>	<u>16</u>
8 X 12.415 _____	_____	_____	_____	_____	_____
8 X 12.25 DC-HOLE	<u>476</u>	<u>.0836</u>	<u>196</u>	<u>378</u>	<u>40</u>

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.
	DP	HWDP	DC				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	<u>21</u>	<u>30</u>	<u>20</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>4272</u>	<u>727</u>	<u>476</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>

REMARKS AND RECOMMENDATIONS

MW 9.8 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

DRILL AHEAD THRU CLY/SILT/SAND TO 4584'. POOH DUE TO SLOW PENETRATION RATES. HOLE PULLED TIGHT FROM 3937 TO SHOE. BACK REAM TO SHOE. RIH W/NB 7 (PDC) AND MWD TOOL. DRILL TO 5475'. ESTIMATED PORE PRESSURE RAISED TO 8.9 ppg AT 4600'.

ADT D. WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 6658
 OPERATION TRIP
 FOOTAGE 1183

NO. 17
 DATE Sep 26 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>60</u>	MAX GAS (units) <u>630</u>	AT DEPTH (feet) <u>6350</u>	SURVEY DATA <u>.78 @ 6628</u>
BACKGROUND CONNECTION TRIP <u>160</u>	<u>422</u>	<u>6563</u>	LITHOLOGY <u>70% CLAY 30% SLT</u>
FLOWLINE TEMP _____ degrees F			SAMPLE DEPTH <u>6658</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP <u>915</u>
			LAG OFF BOTTOM <u>7250</u>
			DRILL RATE ft/hr <u>60</u>
			CORRECTED 'D' EXP. <u>.81</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>4.00</u>

FORMATION PRESSURE DATA

	CASING	BOTTOM HOLE	OPEN HOLE
PORE PRESSURE	<u>1665</u> psi <u>8.7</u> ppg	<u>3185</u> psi <u>9.2</u> ppg	_____ psi _____ ppg _____ ft
FRACTURE PRESSURE	<u>2871</u> psi <u>15</u> ppg	<u>5366</u> psi <u>15.5</u> ppg	_____ psi _____ ppg _____ ft
ECD	<u>2067</u> psi <u>10.8</u> ppg	<u>3739</u> psi <u>10.8</u> ppg	_____ psi _____ ppg _____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 25 SEP 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u> 2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>10.4</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u> <u>4.92</u>
FUNNEL VIS. <u>64</u>	SIZE <u>12.25</u>	PUMP RATE stks/min <u>71</u> <u>71</u>
PV/YP <u>30/41</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min <u>349</u> <u>349</u>
GELS <u>4/8</u>	DEPTH OUT _____	PRESSURE psi _____ <u>2350</u>
pH <u>9.1</u>	ROT HRS. <u>23.2</u>	PD SURF / DS psi _____ <u>54/1653</u>
FILT/CAKE API <u>3.0/1</u>	FOOTAGE <u>2074</u>	ANN / BIT psi _____ <u>78/804</u>
HP-HT <u>6.6</u>	AVG ft/hr <u>89</u>	JET VELOCITY ft/sec _____ <u>293</u>
P _m <u>.5</u>	GRADE _____	JET IMPACT lbs _____ <u>1086</u>
Pf/Mf <u>.25/2.9</u>	HOLE DEV. <u>.78</u>	BIT HP _____ <u>323</u>
CHLORIDES ppm <u>17000</u>	COST/FT _____	HP RATIO / HP/IN2 _____ <u>16.8 hp/in2</u>
CALCIUM ppm <u>200</u>	RPM <u>155</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>0/10/90</u>	WOB <u>4</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>45</u>	<u>368</u>	<u>65</u>
<u>5 X 12.415</u>	<u>DP-C&G</u>	<u>3504</u>	<u>.1255</u>	<u>131</u>	<u>439</u>	<u>583</u>
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>2501</u>	<u>.1215</u>	<u>135</u>	<u>441</u>	<u>267</u>
<u>8 X 12.415</u>						
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>196</u>	<u>471</u>	<u>40</u>

PIPE DATA

	DRILL STRING			CASING:	RISER	COND.	SURF.
	DP	HWDP	DC	DEPTH			
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u> <u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20</u>	<u>27</u>	<u>18.73</u> <u>12.415</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>.3409</u> <u>.1498</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>			<u>.113</u>	<u>.0478</u> <u>.0240</u>
LENGTH-ft	<u>5455</u>	<u>727</u>	<u>476</u>		<u>177</u>	<u>100</u>	<u>812</u> <u>3774</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>			<u>450</u>	<u>133</u> <u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.2 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

DRILL TO 6373' LOOKING FOR CORE POINT. CBU. DRILL TO 6658'. CBU. SHORT TRIP TO SHOE TO CONDITION HOLE. HOLE PULLED TIGHT.

BACKREAM AND PUMP OUT TO SHOE. BIT APPARENTLY BALLING UP WITH CLAY. ESTIMATED PORE PRESSURE RAISED TO 9.2 ppg. CONDENSED RESISTIVITY PLOT INDICATES INCREASING PORE PRESSURE AT 5000'. MUD WEIGHT RAISED IN STAGES TO 10.4 ppg.

ADT D. WALTERS

sperry-sun **LOGGING SYSTEMS**

DRILLING SERVICES
A Baroid Company

DEPTH 7036
OPERATION W.O.W.
FOOTAGE 387

No. 18
DATE Sep 27 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>85</u>	MAX GAS (units) <u>220</u>	AT DEPTH (feet) <u>7036</u>	SURVEY DATA <u>.57 @ 6911</u>	LITHOLOGY <u>40% CLAY 60% SLT</u>	SAMPLE DEPTH <u>7036</u>	DRILL RATE ft/hr <u>60</u>
BACKGROUND CONNECTION <u>100</u>	TRIP <u>365</u>	FLOWLINE TEMP _____ degrees F	TRIP CHLORIDES <u>NA</u>	LAG DOWN DP <u>994</u>	LAG OFF BOTTOM <u>7810</u>	CORRECTED "D" EXP. <u>.81</u>
						SHALE DENSITY g/cc <u>NA</u>
						EWR Res. <u>4.00</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi	<u>8.7</u> ppg	<u>3366</u> psi	<u>9.2</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>2832</u> psi	<u>14.8</u> ppg	<u>5671</u> psi	<u>15.5</u> ppg	_____ psi	_____ ppg
ECD	<u>2048</u> psi	<u>10.7</u> ppg	<u>3914</u> psi	<u>10.7</u> ppg	_____ psi	_____ ppg

MUD DATA

TIME	<u>2300 26 SEP 93</u>
TYPE	<u>PHPA-SEA WATER</u>
WEIGHT IN	<u>10.5</u>
FUNNEL VIS.	<u>57</u>
PV/YP	<u>25/29</u>
GELS	<u>4/8</u>
pH	<u>9.2</u>
FILT/CAKE API	<u>2.8/1</u>
HP-HT	<u>6.6</u>
P _m	<u>.6</u>
Pf/Mf	<u>.3/2.0</u>
CHLORIDES ppm	<u>17000</u>
CALCIUM ppm	<u>320</u>
OIL/WATER/SOLIDS	<u>0/10/90</u>
DAILY/CUM. COST	_____

BIT DATA

BIT NO.	<u>7</u>
TYPE	<u>DS40HF</u>
IADC CODE	_____
SIZE	<u>12.25</u>
JETS	<u>TFA .751</u>
DEPTH OUT	_____
ROT HRS.	<u>28.8</u>
FOOTAGE	<u>2455</u>
AVG ft/hr	<u>85</u>
GRADE	_____
HOLE DEV.	<u>.57</u>
COST/FT	_____
RPM	<u>171</u>
WOB	<u>5</u>

HYDRAULIC DATA

PUMPS	1. <u>ID-1600</u>	2. <u>ID-1600</u>
SIZE inches	<u>6.5X12</u>	<u>6.5X12</u>
CAPACITY gal/stk	<u>4.92</u>	<u>4.92</u>
PUMP RATE stks/min	<u>71</u>	<u>71</u>
FLOW RATE gal/min	<u>349</u>	<u>349</u>
PRESSURE psi	<u>2650</u>	
PD SURF / DS psi	<u>54/1654</u>	
ANN / BIT psi	<u>56/812</u>	
JET VELOCITY ft/sec	<u>293</u>	
JET IMPACT lbs	<u>1096</u>	
BIT HP	<u>326</u>	
HP RATIO / HP/IN2	<u>19.2 hp/in2</u>	
REDUCED 1	_____ psi at _____	_____ stks/min
RATE 2	_____ psi at _____	_____ stks/min

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>45</u>	<u>280</u>	<u>65</u>
<u>5 X 12.415</u>	<u>DP-CSG</u>	<u>3504</u>	<u>.1255</u>	<u>131</u>	<u>344</u>	<u>583</u>
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>2879</u>	<u>.1215</u>	<u>135</u>	<u>346</u>	<u>206</u>
<u>8 X 12.415</u>						
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>196</u>	<u>377</u>	<u>40</u>

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	
	DP	HWDP	DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u>	<u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20</u>	<u>30</u>	<u>20</u>	<u>13 3/8</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>.3409</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>			<u>.113</u>	<u>.0478</u>	<u>.0240</u>
LENGTH-ft	<u>5842</u>	<u>727</u>	<u>476</u>		<u>177</u>	<u>100</u>	<u>812</u>	<u>3774</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>			<u>450</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.2 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

TRIP IN HOLE AFTER SHORT TRIP. TRIP GAS=365. DRILL AHEAD TO 7036' LOOKING FOR CORE POINT. WEATHER DETERIORATING. POOH TO SHOE AND HANG OFF. WAIT ON WEATHER. RAISED MW TO 10.5 ppg.

ADT D. WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 7518
 OPERATION DRILL
 FOOTAGE 482

NO. 19
 DATE Sep 28 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>47</u>	MAX GAS (units) <u>100</u>	AT DEPTH (feet) <u>7518</u>	SURVEY DATA <u>1.09 @ 7384</u>
BACKGROUND CONNECTION TRIP <u>75</u>	FLOWLINE TEMP <u>77</u> degrees F	LITHOLOGY <u>20% CLAY 70% SLT 10% SAND</u>	LAG DOWN DP <u>1042</u>
TRIP CHLORIDES <u>876</u>	LAG OFF BOTTOM <u>8333</u>	SAMPLE DEPTH <u>7330</u>	DRILL RATE ft/hr <u>187</u>
		TRIP CHLORIDES <u>NA</u>	CORRECTED 'D' EXP. <u>.80</u>
		LAG OFF BOTTOM <u>8333</u>	SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>4.00</u>

FORMATION PRESSURE DATA

	CASING	BOTTOM HOLE	OPEN HOLE
PORE PRESSURE	<u>1665</u> psi <u>8.7</u> ppg	<u>3675</u> psi <u>9.4</u> ppg	psi ppg ft
FRACTURE PRESSURE	<u>2832</u> psi <u>14.8</u> ppg	<u>5671</u> psi <u>15.5</u> ppg	psi ppg ft
ECD	<u>2208</u> psi <u>11.0</u> ppg	<u>4300</u> psi <u>11.0</u> ppg	psi ppg ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 27 SEP 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u> 2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>10.5</u>	IADC CODE	CAPACITY gal/stk <u>4.92</u> <u>4.92</u>
FUNNEL VIS. <u>60</u>	SIZE <u>12.25</u>	PUMP RATE stks/min <u>74</u> <u>71</u>
PV/YP <u>25/30</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min <u>364</u> <u>349</u>
GELS <u>3/8</u>	DEPTH OUT	PRESSURE psi <u>2670</u>
pH <u>9.2</u>	ROT HRS. <u>32.5</u>	PD SURF / DS psi <u>54/1847</u>
FILT/CAKE API <u>2.8/1</u>	FOOTAGE <u>2934</u>	ANN / BIT psi <u>64/881</u>
HP-HT <u>8.0</u>	AVG ft/hr <u>90</u>	JET VELOCITY ft/sec <u>306</u>
Pm <u>.6</u>	GRADE	JET IMPACT lbs <u>1191</u>
Pf/Mf <u>.3/2.0</u>	HOLE DEV. <u>1.08</u>	BIT HP <u>369</u>
CHLORIDES ppm <u>17000</u>	COST/FT	HP RATIO / HP/IN2 <u>19.2 hp/in2</u>
CALCIUM ppm <u>280</u>	RPM <u>170</u>	REDUCED 1 psi at stk/min
OIL/WATER/SOLIDS <u>0/10.5/89.5</u>	WOB <u>6</u>	RATE 2 psi at stk/min
DAILY/CUM. COST		

ANNULAR DATA

	LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u> DP-RISER	<u>177</u>	<u>.3644</u>	<u>47</u>	<u>290</u>	<u>65</u>
<u>5 X 12.415</u> DP-C&G	<u>3504</u>	<u>.1255</u>	<u>136</u>	<u>353</u>	<u>583</u>
<u>5 X 12.25</u> DP-HOLE	<u>3361</u>	<u>.1215</u>	<u>141</u>	<u>355</u>	<u>265</u>
<u>8 X 12.415</u>					
<u>8 X 12.25</u> DC-HOLE	<u>476</u>	<u>.0836</u>	<u>204</u>	<u>385</u>	<u>40</u>

PIPE DATA

	DRILL STRING			CASING: RISER	COND.	SURF.	
	DP	HWDP	DC	DEPTH			
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	<u>21</u>	<u>309</u>	<u>1022</u>	<u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	<u>20</u>	<u>30</u>	<u>18.73</u>	<u>12.415</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>		<u>.113</u>	<u>.0478</u>	<u>.0240</u>
LENGTH-ft	<u>6315</u>	<u>727</u>	<u>476</u>	<u>177</u>	<u>100</u>	<u>812</u>	<u>3774</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>		<u>450</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.4 GPM 650 JETS 2-12,2-13 ft/mi = sec/std

WAIT ON WEATHER. RUN BACK IN HOLE FROM SHOE. SHORT TRIP GAS-876. DRILL AHEAD THRU SILTSTONE/CLAY/SAND TO 7518'.
 CONDENSED RESISTIVITY PLOT INDICATES PORE PRESSURE INCREASING. RAISED ESTIMATED PORE PRESSURE TO 9.4 ppg.
 HOLE OCCASIONALLY PACKING OFF. CONTINUE DRILLING LOOKING FOR CORE POINT.

ADT D. WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 8000
 OPERATION E LOG
 FOOTAGE 482

NO. 20
 DATE Sep 29 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) <u>55</u>	MAX GAS (units) <u>100</u>	AT DEPTH (feet) <u>8000</u>	SURVEY DATA <u>2.18 @ 7951</u>	LITHOLOGY <u>20% CLAY 70% SLT 10% SAND</u>
BACKGROUND CONNECTION TRIP <u>75</u>	TRIP CHLORIDES <u>NA</u>	DRILL RATE ft/hr <u>111</u>	SAMPLE DEPTH <u>8000</u>	CORRECTED 'D' EXP. <u>.78</u>
FLOWLINE TEMP <u>79</u> degrees F	LAG DOWN DP <u>NA</u>	SHALE DENSITY g/cc <u>NA</u>	LAG OFF BOTTOM <u>NA</u>	EWR Res. <u>4.73</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi	<u>8.7</u> ppg	<u>4035</u> psi	<u>9.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>2832</u> psi	<u>14.8</u> ppg	<u>5671</u> psi	<u>15.5</u> ppg	_____ psi	_____ ppg
ECD	<u>2124</u> psi	<u>11.1</u> ppg	<u>4617</u> psi	<u>11.1</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 28 SEP 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.6</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>6060</u>	SIZE <u>12.25</u>	PUMP RATE stks/min <u>74</u>	<u>71</u>
PV/YP <u>31/43</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min <u>364</u>	<u>349</u>
GELS <u>4/9</u>	DEPTH OUT <u>8000</u>	PRESSURE psi <u>3100</u>	
pH <u>9.1</u>	ROT HRS. <u>36.5</u>	PD SURF / DS psi <u>58/2029</u>	
FILT/CAKE API <u>3.0/1</u>	FOOTAGE <u>2934</u>	ANN / BIT psi <u>99/898</u>	
HP-HT <u>7.6</u>	AVG ft/hr <u>90</u>	JET VELOCITY ft/sec <u>306</u>	
P _m <u>.6</u>	GRADE _____	JET IMPACT lbs <u>1213</u>	
P _f /M _f <u>.2/2.0</u>	HOLE DEV. <u>1.08</u>	BIT HP <u>376</u>	
CHLORIDES ppm <u>17000</u>	COST/FT <u>317</u>	HP RATIO / HP/IN2 <u>19.54 hp/in2</u>	
CALCIUM ppm <u>320</u>	RPM <u>172</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>0/11/89</u>	WOB <u>66.4</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____			

ANNULAR DATA

		LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>47</u>	<u>374</u>	<u>65</u>
<u>5 X 12.415</u>	<u>DP-CSG</u>	<u>3504</u>	<u>.1255</u>	<u>136</u>	<u>445</u>	<u>583</u>
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>3843</u>	<u>.1215</u>	<u>141</u>	<u>447</u>	<u>454</u>
<u>8 X 12.415</u>						
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>204</u>	<u>477</u>	<u>40</u>

PIPE DATA

	DRILL STRING			CASING: RISER COND. SURF.				
	DP	HWDP	DC	DEPTH				
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>		<u>21</u>	<u>309</u>	<u>1022</u>	<u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>		<u>20</u>	<u>27</u>	<u>18.73</u>	<u>12.415</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>		<u>.3887</u>	<u>.7085</u>	<u>.3409</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>			<u>.113</u>	<u>.0478</u>	<u>.0240</u>
LENGTH-ft	<u>6797</u>	<u>727</u>	<u>476</u>		<u>177</u>	<u>100</u>	<u>812</u>	<u>3774</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>			<u>450</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW <u>10.7</u> GPM <u>650</u> JETS <u>2-12,2-13</u> _____ ft/mi = _____ sec/std
DRILL AHEAD THRU SILTSTONE/CLAY/SAND TO 8000' -TD. SHORT TRIP TO SHOE. HOLE PULLED TIGHT FROM BOTTOM TO 6120'. RIH. SHORT TRIP
GAS = 525. CBU PUMPING SWEEPS TO CLEAN HOLE FOR LOGGING OPS. POOH. COMMENCE E LOGGING. CONDENSED RESISTIVITY PLOT
INCREASING PORE PRESSURE FROM 4700' TO 6100' AND 6800' TO 7800'. ESTIMATED PORE PRESSURE RAISED TO 9.7 ppg AT 7500'. MUD WEIGHT RAISED TO 10.7 ppg.
ADT <u>D. WALTERS</u>

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS
 A Baroid Company

DEPTH 8000
 OPERATION TRIP
 FOOTAGE _____

NO. 21
 DATE Sep 30 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) _____	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>2.18 @ 7951</u>
BACKGROUND CONNECTION TRIP _____	FLOWLINE TEMP _____ degrees F	LITHOLOGY <u>20% CLAY 70% SLT 10% SAND</u>	SAMPLE DEPTH <u>8000</u>
TRIP CHLORIDES <u>NA</u>	LAG DOWN DP _____	DRILL RATE ft/hr _____	CORRECTED 'D' EXP. <u>.78</u>
LAG OFF BOTTOM _____	LAG OFF BOTTOM _____	SHALE DENSITY g/cc <u>NA</u>	EWR Res. <u>4.73</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi	<u>8.7</u> ppg	<u>4035</u> psi	<u>9.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>2832</u> psi	<u>14.8</u> ppg	<u>5671</u> psi	<u>15.5</u> ppg	_____ psi	_____ ppg
ECD	<u>2124</u> psi	<u>11.1</u> ppg	<u>4617</u> psi	<u>11.1</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 29 SEP 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u> 2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>10.7</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u> <u>4.92</u>
FUNNEL VIS. <u>62</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____
PV/YP <u>30/42</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min _____
GELS <u>7/16</u>	DEPTH OUT <u>8000</u>	PRESSURE psi <u>STATIC</u>
pH <u>9.0</u>	ROT HRS. <u>36.5</u>	PD SURF / DS psi _____
FILT/CAKE API <u>3.0/1</u>	FOOTAGE <u>2934</u>	ANN / BIT psi _____
HP-HT <u>7.8</u>	AVG ft/hr <u>90</u>	JET VELOCITY ft/sec _____
Pm <u>.4</u>	GRADE _____	JET IMPACT lbs _____
Pf/Mf <u>.15/1.9</u>	HOLE DEV. <u>1.08</u>	BIT HP _____
CHLORIDES ppm <u>17000</u>	COST/FT <u>317</u>	HP RATIO / HP/IN2 _____
CALCIUM ppm <u>360</u>	RPM <u>172</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>0/11.5/88.5</u>	WOB <u>66.4</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

	LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBL/STK
<u>5 X 20 DP-RISER</u>	<u>177</u>	<u>.3644</u>	<u>47</u>	<u>374</u>	<u>65</u>
<u>5 X 12.415 DP-CSG</u>	<u>3504</u>	<u>.1255</u>	<u>136</u>	<u>445</u>	<u>583</u>
<u>5 X 12.25 DP-HOLE</u>	<u>3843</u>	<u>.1215</u>	<u>141</u>	<u>447</u>	<u>454</u>
<u>8 X 12.415</u>	_____	_____	_____	_____	_____
<u>8 X 12.25 DC-HOLE</u>	<u>476</u>	<u>.0836</u>	<u>204</u>	<u>477</u>	<u>40</u>

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	
	DP	HWDP	DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	<u>21</u>	<u>309</u>	<u>1022</u>	<u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>20</u>	<u>30</u>	<u>18.73</u>	<u>13 3/8</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>	<u>.1498</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>	<u>.0240</u>
LENGTH-ft	<u>6797</u>	<u>727</u>	<u>476</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>	<u>3774</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.7 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

LOGGING TOOL WOULD NOT PENETRATE PAST CASING SHOE. RIH TO 2350'. WASH AND REAM CASING FROM 2350 TO 3760'. MAX GAS=80.

POOH FOR LOGGING RUN. LOGGING TOOL WOULD NOT GO TO BOTTOM. RIH. WASH AND REAM FROM 6500' TO 6782'. RUN TO BOTTOM. CBU

TRIP GAS=181. POOH. BACKREAM FROM 6400' TO 6120'. CBU AT SHOE. POOH.

ADT D. WALTERS

sperry-sun *LOGGING SYSTEMS*

DRILLING SERVICES
A Baroid Company

DEPTH 8000
OPERATION E LOG
FOOTAGE _____

NO. 23
DATE Oct 2 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY
MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) _____	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>2.18 @ 7951</u>
BACKGROUND _____	CONNECTION _____	TRIP _____	LITHOLOGY <u>20% CLAY 70% SLT 10% SAND</u>
FLOWLINE TEMP _____ degrees F	DRILL RATE ft/hr _____	CORRECTED 'D' EXP. <u>.78</u>	SAMPLE DEPTH <u>8000</u>
	TRIP CHLORIDES <u>NA</u>	SHALE DENSITY g/cc <u>NA</u>	LAG DOWN DP _____
	LAG OFF BOTTOM _____	EWR Res. <u>4.73</u>	

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi	<u>8.7</u> ppg	<u>4035</u> psi	<u>9.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>2832</u> psi	<u>14.8</u> ppg	<u>5671</u> psi	<u>15.5</u> ppg	_____ psi	_____ ppg
ECD	<u>2124</u> psi	<u>11.1</u> ppg	<u>4617</u> psi	<u>11.1</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 1 OCT 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u> 2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u> <u>6.5X12</u>
WEIGHT IN <u>10.7</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u> <u>4.92</u>
FUNNEL VIS. <u>81</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____
PV/YP <u>25/33</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min _____
GELS <u>4/9</u>	DEPTH OUT <u>8000</u>	PRESSURE psi <u>STATIC</u>
pH <u>9.0</u>	ROT HRS. <u>36.5</u>	PD SURF / DS psi _____
FILT/CAKE API <u>2.6/1</u>	FOOTAGE <u>2934</u>	ANN / BIT psi _____
HP-HT <u>8.2</u>	AVG ft/hr <u>90</u>	JET VELOCITY ft/sec _____
Pm <u>.3</u>	GRADE _____	JET IMPACT lbs _____
Pf/Mf <u>.15/1.7</u>	HOLE DEV. <u>1.08</u>	BIT HP _____
CHLORIDES ppm <u>17800</u>	COST/FT <u>317</u>	HP RATIO / HP/IN2 _____
CALCIUM ppm <u>320</u>	RPM <u>172</u>	REDUCED 1 _____ psi at _____ stk/min
OIL/WATER/SOLIDS <u>0/11.5/88.5</u>	WOB <u>66.4</u>	RATE 2 _____ psi at _____ stk/min
DAILY/CUM. COST _____		

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLs/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	_____	_____	<u>65</u>
<u>5 X 12.415</u>	<u>DP-CSG</u>	<u>3504</u>	<u>.1255</u>	_____	_____	<u>583</u>
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>3843</u>	<u>.1215</u>	_____	_____	<u>454</u>
<u>8 X 12.415</u>	_____	_____	_____	_____	_____	_____
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	<u>40</u>

PIPE DATA

	DRILL STRING			CASING: DEPTH	RISER	COND.	SURF.	
	DP	HWDP	DC					
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	<u>21</u>	<u>309</u>	<u>1022</u>	<u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>20</u>	<u>30</u>	<u>20</u>	<u>13 3/8</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>18.73</u>	<u>12.415</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	_____	_____	<u>.3409</u>	<u>.1498</u>	<u>.1498</u>
LENGTH-ft	<u>6797</u>	<u>727</u>	<u>476</u>	_____	<u>177</u>	<u>.113</u>	<u>.0478</u>	<u>.0240</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	_____	<u>100</u>	<u>812</u>	<u>3774</u>
						<u>450</u>	<u>133</u>	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.7 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

WAIT ON WEATHER. LATCH UP. CONTINUE E LOGGING.

ADT D. WALTERS

sperry-sun
DRILLING SERVICES LOGGING SYSTEMS

A Baroid Company

DEPTH 8000
 OPERATION E LOG
 FOOTAGE _____

No. 24
 DATE Oct 3 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) _____	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>2.18 @ 7951</u>
BACKGROUND CONNECTION TRIP _____	FLOWLINE TEMP _____ degrees F	LITHOLOGY <u>20% CLAY 70% SLT 10% SAND</u>	SAMPLE DEPTH <u>8000</u>
		TRIP CHLORIDES <u>NA</u>	DRILL RATE ft/hr _____
		LAG DOWN DP _____	CORRECTED 'D' EXP. <u>.78</u>
		LAG OFF BOTTOM _____	SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>4.73</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi	<u>8.7</u> ppg	<u>4035</u> psi	<u>9.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>2832</u> psi	<u>14.8</u> ppg	<u>5671</u> psi	<u>15.5</u> ppg	_____ psi	_____ ppg
ECD	<u>2124</u> psi	<u>11.1</u> ppg	<u>4617</u> psi	<u>11.1</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 2 OCT 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.5</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>59</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____	
PV/YP <u>20/24</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min _____	
GELS <u>3/6</u>	DEPTH OUT <u>8000</u>	PRESSURE psi _____	STATIC
pH <u>9.1</u>	ROT HRS. <u>36.5</u>	PD SURF / DS psi _____	
FILT/CAKE API <u>3.2/1</u>	FOOTAGE <u>2934</u>	ANN / BIT psi _____	
HP-HT <u>8.2</u>	AVG ft/hr <u>90</u>	JET VELOCITY ft/sec _____	
P _m <u>.3</u>	GRADE _____	JET IMPACT lbs _____	
P _f /M _f <u>.15/1.6</u>	HOLE DEV. <u>1.08</u>	BIT HP _____	
CHLORIDES ppm <u>18000</u>	COST/FT <u>317</u>	HP RATIO / HP/IN2 _____	
CALCIUM ppm <u>320</u>	RPM <u>172</u>	REDUCED 1 _____ psi at _____ stk/min	
OIL/WATER/SOLIDS <u>0/10.5/89.5</u>	WOB <u>66.4</u>	RATE 2 _____ psi at _____ stk/min	
DAILY/CUM. COST _____			

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
<u>5 X 20</u>	<u>DP-RISER</u>	<u>177</u>	<u>.3644</u>	_____	_____	<u>65</u>
<u>5 X 12.415</u>	<u>DP-CSG</u>	<u>3504</u>	<u>.1255</u>	_____	_____	<u>583</u>
<u>5 X 12.25</u>	<u>DP-HOLE</u>	<u>3843</u>	<u>.1215</u>	_____	_____	<u>454</u>
<u>8 X 12.415</u>		_____	_____	_____	_____	_____
<u>8 X 12.25</u>	<u>DC-HOLE</u>	<u>476</u>	<u>.0836</u>	_____	_____	<u>40</u>

PIPE DATA

	DRILL STRING			CASING:			
	DP	HWDP	DC	DEPTH	RISER	COND.	SURF.
OD-inches	<u>5.0</u>	<u>5.0</u>	<u>8.0</u>	_____	_____	_____	<u>3681</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	<u>2.875</u>	_____	<u>21</u>	<u>30</u>	<u>13 3/8</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	<u>.0080</u>	_____	<u>20</u>	<u>27</u>	<u>18.73</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	<u>.0542</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
LENGTH-ft	<u>6797</u>	<u>727</u>	<u>476</u>	_____	_____	<u>.113</u>	<u>.0478</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	<u>147</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>
						<u>450</u>	<u>133</u>
							<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.7 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

WAIT ON WEATHER. LATCH UP. CONTINUE E LOGGING. SUSPEND E LOGGING. HANG OFF. LATCH UP. CONTINUE E LOGGING. TIH FOR CLEANOUT RUN.

ADT _____ D. WALTERS

sperry-sun *LOGGING SYSTEMS*
 DRILLING SERVICES

A Baroid Company

DEPTH 8000
 OPERATION E LOG
 FOOTAGE _____

No. 25
 DATE Oct 4 93
 TIME 04 00

APPLIED DRILLING TECHNOLOGY
 MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units) _____	MAX GAS (units) _____	AT DEPTH (feet) _____	SURVEY DATA <u>2.18 @ 7951</u>
BACKGROUND _____	CONNECTION _____	TRIP _____	LITHOLOGY <u>20% CLAY 70% SLT 10% SAND</u>
FLOWLINE TEMP _____ degrees F	TRIP <u>517</u>	8000	SAMPLE DEPTH <u>8000</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP _____
			LAG OFF BOTTOM _____
			DRILL RATE ft/hr _____
			CORRECTED 'D' EXP. <u>.78</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>4.73</u>

FORMATION PRESSURE DATA

	CASING			BOTTOM HOLE			OPEN HOLE		
PORE PRESSURE	<u>1665</u>	psi	<u>8.7</u>	ppg	<u>4035</u>	psi	<u>9.7</u>	ppg	_____ psi _____ ppg _____ ft
FRACTURE PRESSURE	<u>2832</u>	psi	<u>14.8</u>	ppg	<u>5671</u>	psi	<u>15.5</u>	ppg	_____ psi _____ ppg _____ ft
ECD	<u>2124</u>	psi	<u>11.1</u>	ppg	<u>4817</u>	psi	<u>11.1</u>	ppg	_____ psi _____ ppg _____ ft

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 3 OCT 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.5</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>61</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____	_____
PV/YP <u>19/24</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min _____	_____
GELS <u>3/6</u>	DEPTH OUT <u>8000</u>	PRESSURE psi _____	<u>STATIC</u>
pH <u>9.1</u>	ROT HRS. <u>36.5</u>	PD SURF / DS psi _____	_____
FILT/CAKE API <u>3.2/1</u>	FOOTAGE <u>2934</u>	ANN / BIT psi _____	_____
HP-HT <u>8.2</u>	AVG ft/hr <u>90</u>	JET VELOCITY ft/sec _____	_____
P _m <u>.3</u>	GRADE _____	JET IMPACT lbs _____	_____
Pf/Mf <u>.15/1.5</u>	HOLE DEV. <u>1.08</u>	BIT HP _____	_____
CHLORIDES ppm <u>18000</u>	COST/FT <u>317</u>	HP RATIO / HP/IN2 _____	_____
CALCIUM ppm <u>360</u>	RPM <u>172</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>0/10.5/89.5</u>	WOB <u>66.4</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____			

ANNULAR DATA

	LENGTH - FT.	VOLUME BBL/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLs
5 X 20 DP-RISER	<u>177</u>	<u>.3644</u>	_____	_____	<u>65</u>
5 X 12.415 DP-CSG	<u>3504</u>	<u>.1255</u>	_____	_____	<u>583</u>
5 X 12.25 DP-HOLE	<u>3843</u>	<u>.1215</u>	_____	_____	<u>454</u>
8 X 12.415 _____	_____	_____	_____	_____	_____
8 X 12.25 DC-HOLE	<u>476</u>	<u>.0836</u>	_____	_____	<u>40</u>

PIPE DATA

	DRILL STRING				CASING: DEPTH	RISER	COND.	SURF.
OD-inches	DP <u>5.0</u>	HWDP <u>5.0</u>	_____	DC <u>8.0</u>	_____	<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	_____	<u>2.875</u>	_____	<u>20</u>	<u>27</u>	<u>18.73</u>
CAP-bbls/ft	<u>.0178</u>	<u>.0087</u>	_____	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbls/ft	<u>.0072</u>	<u>.0181</u>	_____	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>6797</u>	<u>727</u>	_____	<u>476</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	_____	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>
								<u>3681</u>
								<u>13 3/8</u>
								<u>12.415</u>
								<u>.1498</u>
								<u>.0240</u>
								<u>3774</u>
								<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.7 GPM 650 JETS 2-12,2-13 ft/mi = _____ sec/std

RIH FOR CLEAN OUT RUN. PUMP SWEEP. CBU. TRIP GAS=517. POOH. E LOG

ADT D. WALTERS

sperry-sun DRILLING SERVICES **LOGGING SYSTEMS**

A Baroid Company

DEPTH 8000
OPERATION E LOG
FOOTAGE _____

NO. 26
DATE Oct 5 93
TIME 04 00

APPLIED DRILLING TECHNOLOGY MORNING REPORT

OPERATOR <u>ARCO ALASKA, INC.</u>	WELL NAME <u>KUVLUM #3</u>	FIELD/BLOCK <u>NR 6-4 BLK 673</u>
CONTRACTOR <u>CANMAR</u>	RIG NAME <u>KULLUK</u>	AREA <u>BEAUFORT SEA</u>
START DATE <u>Sep 9 93</u>	LOC. <u>OFFSHORE</u>	STATE <u>ALASKA</u>

LOGGING DATA

AVG GAS (units)	MAX GAS (units)	AT DEPTH (feet)	SURVEY DATA <u>2.18 @ 7951</u>
BACKGROUND CONNECTION TRIP			LITHOLOGY <u>20% CLAY 70% SLT 10% SAND</u>
FLOWLINE TEMP _____ degrees F			SAMPLE DEPTH <u>8000</u>
			TRIP CHLORIDES <u>NA</u>
			LAG DOWN DP _____
			LAG OFF BOTTOM _____
			DRILL RATE ft/hr _____
			CORRECTED 'D' EXP. <u>.78</u>
			SHALE DENSITY g/cc <u>NA</u>
			EWR Res. <u>4.73</u>

FORMATION PRESSURE DATA

	CASING		BOTTOM HOLE		OPEN HOLE	
PORE PRESSURE	<u>1665</u> psi	<u>8.7</u> ppg	<u>4035</u> psi	<u>9.7</u> ppg	_____ psi	_____ ppg
FRACTURE PRESSURE	<u>2832</u> psi	<u>14.8</u> ppg	<u>5671</u> psi	<u>15.5</u> ppg	_____ psi	_____ ppg
ECD	<u>2124</u> psi	<u>11.1</u> ppg	<u>4617</u> psi	<u>11.1</u> ppg	_____ psi	_____ ppg

MUD DATA

BIT DATA

HYDRAULIC DATA

TIME <u>2300 3 OCT 93</u>	BIT NO. <u>7</u>	PUMPS 1. <u>ID-1600</u>	2. <u>ID-1600</u>
TYPE <u>PHPA-SEA WATER</u>	TYPE <u>DS40HF</u>	SIZE inches <u>6.5X12</u>	<u>6.5X12</u>
WEIGHT IN <u>10.5</u>	IADC CODE _____	CAPACITY gal/stk <u>4.92</u>	<u>4.92</u>
FUNNEL VIS. <u>61</u>	SIZE <u>12.25</u>	PUMP RATE stks/min _____	_____
PV/YP <u>19/24</u>	JETS <u>TFA .751</u>	FLOW RATE gal/min _____	_____
GELS <u>3/6</u>	DEPTH OUT <u>8000</u>	PRESSURE psi _____	<u>STATIC</u>
pH <u>9.1</u>	ROT HRS. <u>36.5</u>	PD SURF / DS psi _____	_____
FILT/CAKE API <u>3.2/1</u>	FOOTAGE <u>2934</u>	ANN / BIT psi _____	_____
HP-HT <u>8.2</u>	AVG ft/hr <u>90</u>	JET VELOCITY ft/sec _____	_____
P _m <u>.3</u>	GRADE <u>E-2-i</u>	JET IMPACT lbs _____	_____
P _f /M _f <u>.15/1.5</u>	HOLE DEV. <u>1.08</u>	BIT HP _____	_____
CHLORIDES ppm <u>18000</u>	COST/FT <u>317</u>	HP RATIO / HP/IN2 _____	_____
CALCIUM ppm <u>360</u>	RPM <u>172</u>	REDUCED 1 _____ psi at _____ stk/min	_____
OIL/WATER/SOLIDS <u>0/10.5/89.5</u>	WOB <u>66.4</u>	RATE 2 _____ psi at _____ stk/min	_____
DAILY/CUM. COST _____			

ANNULAR DATA

		LENGTH - FT.	VOLUME BBLS/FT.	VELOCITY FT/MIN	CRIT-VEL FT/MIN	ANN-VOL BBLS
5 X 20	DP-RISER	<u>177</u>	<u>.3644</u>	_____	_____	<u>65</u>
5 X 12.415	DP-CSG	<u>3504</u>	<u>.1255</u>	_____	_____	<u>583</u>
5 X 12.25	DP-HOLE	<u>3843</u>	<u>.1215</u>	_____	_____	<u>454</u>
8 X 12.415		_____	_____	_____	_____	_____
8 X 12.25	DC-HOLE	<u>476</u>	<u>.0836</u>	_____	_____	<u>40</u>

PIPE DATA

	DP	HWDP	DRILL STRING	DC	CASING: DEPTH	RISER	COND.	SURF.
OD-inches	<u>5.0</u>	<u>5.0</u>	_____	<u>8.0</u>	_____	<u>21</u>	<u>309</u>	<u>1022</u>
ID-inches	<u>4.276</u>	<u>3.0</u>	_____	<u>2.875</u>	_____	<u>20</u>	<u>30</u>	<u>20</u>
CAP-bbbls/ft	<u>.0178</u>	<u>.0087</u>	_____	<u>.0080</u>	_____	<u>.3887</u>	<u>.7085</u>	<u>.3409</u>
DISP-bbbls/ft	<u>.0072</u>	<u>.0181</u>	_____	<u>.0542</u>	_____	_____	<u>.113</u>	<u>.0478</u>
LENGTH-ft	<u>6797</u>	<u>727</u>	_____	<u>476</u>	_____	<u>177</u>	<u>100</u>	<u>812</u>
WEIGHT-lbs/ft	<u>19.5</u>	<u>49</u>	_____	<u>147</u>	_____	_____	<u>450</u>	<u>133</u>
			_____	_____	_____	_____	_____	<u>3681</u>
			_____	_____	_____	_____	_____	<u>13 3/8</u>
			_____	_____	_____	_____	_____	<u>12.415</u>
			_____	_____	_____	_____	_____	<u>.1498</u>
			_____	_____	_____	_____	_____	<u>.0240</u>
			_____	_____	_____	_____	_____	<u>3774</u>
			_____	_____	_____	_____	_____	<u>68</u>

REMARKS AND RECOMMENDATIONS

MW 10.7 GPM 650 JETS 2-12,2-13 _____ ft/mi = _____ sec/std

COMPLETE E LOGGING. P&A.

ADT D. WALTERS